

This Appendix presents two hydrologic and hydraulic analysis tools that can be used to size stormwater management practices (SMPs). The first is the TR-55 (NRCS, 1986) “short-cut” sizing technique, used to size practices designed for extended detention, slightly modified to incorporate the small flows necessary to provide channel protection. The second is a method used to determine the peak flow from water quality storm events. (This is often important when the water quality storm is diverted to a water quality practice, with other larger events bypassed).

### B.1 Storage Volume Estimation

This section presents a modified version of the TR-55 short cut sizing approach. The method was modified by Harrington (1987), for applications where the peak discharge is very small compared with the uncontrolled discharge. This often occurs in the 1-year, 24-hour detention sizing.

Using TR-55 guidance (NRCS, 1986), the unit peak discharge ( $q_u$ ) can be determined based on the the Curve Number and Time of Concentration. Knowing  $q_u$  and  $T$  (extended detention time),  $q_o/q_i$  (peak outflow discharge/peak inflow discharge) can be estimated from Figure B.1.

Figure B.2 can also be used to estimate  $V_s/V_r$ . For a Type II or Type III rainfall distribution,  $V_s/V_r$  can also be calculated using the following equation:

$$V_s/V_r = 0.682 - 1.43 (q_o/q_i) + 1.64 (q_o/q_i)^2 - 0.804 (q_o/q_i)^3 \quad (2.1.16)$$

Where:

- $V_s$  = required storage volume (acre-feet)
- $V_r$  = runoff volume (acre-feet)
- $q_o$  = peak outflow discharge (cfs)
- $q_i$  = peak inflow discharge (cfs)

The required storage volume can then be calculated by:

$$V_s = \frac{(V_s/V_r)(Q_d)(A)}{12} \quad (2.1.17)$$

Where:  $V_s$  and  $V_r$  are defined above

$Q_d$  = the post-developed runoff for the design storm (inches)

$A$  = total drainage area (acres)

While the TR-55 short-cut method reports to incorporate multiple stage structures, experience has shown that an additional 10-15% storage is required when multiple levels of extended detention are provided.

Figure B.1 Detention Time vs. Discharge Ratios (Source: MDE, 2000)

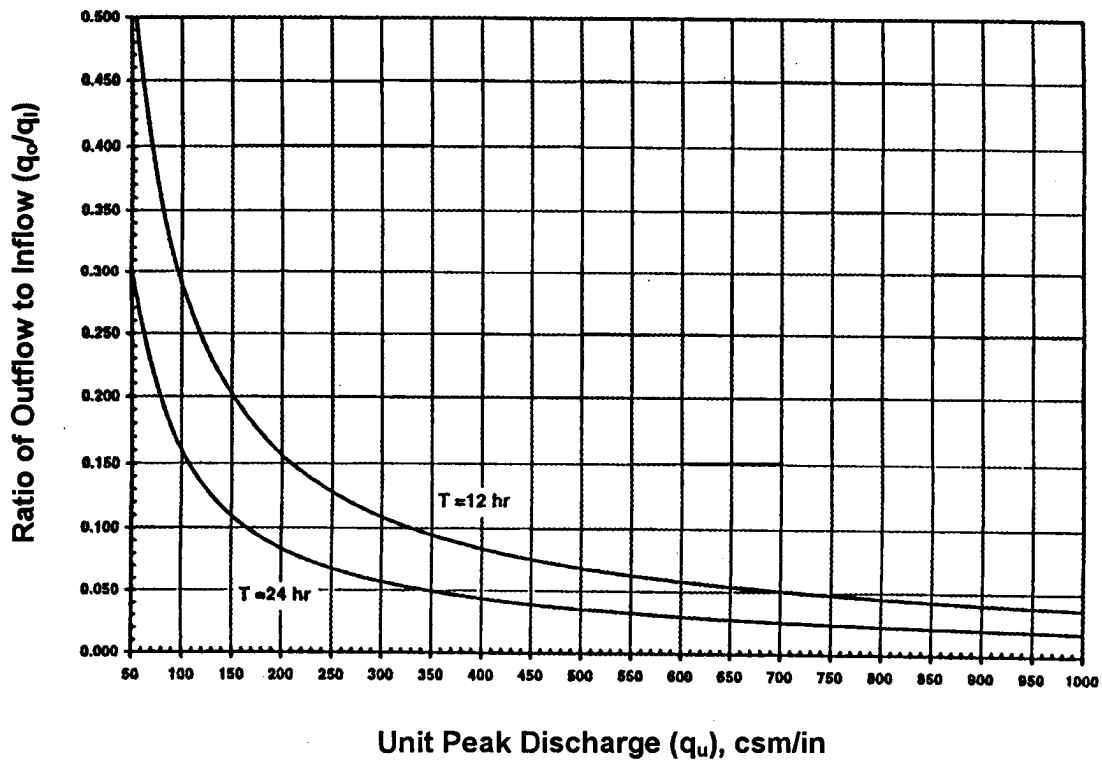
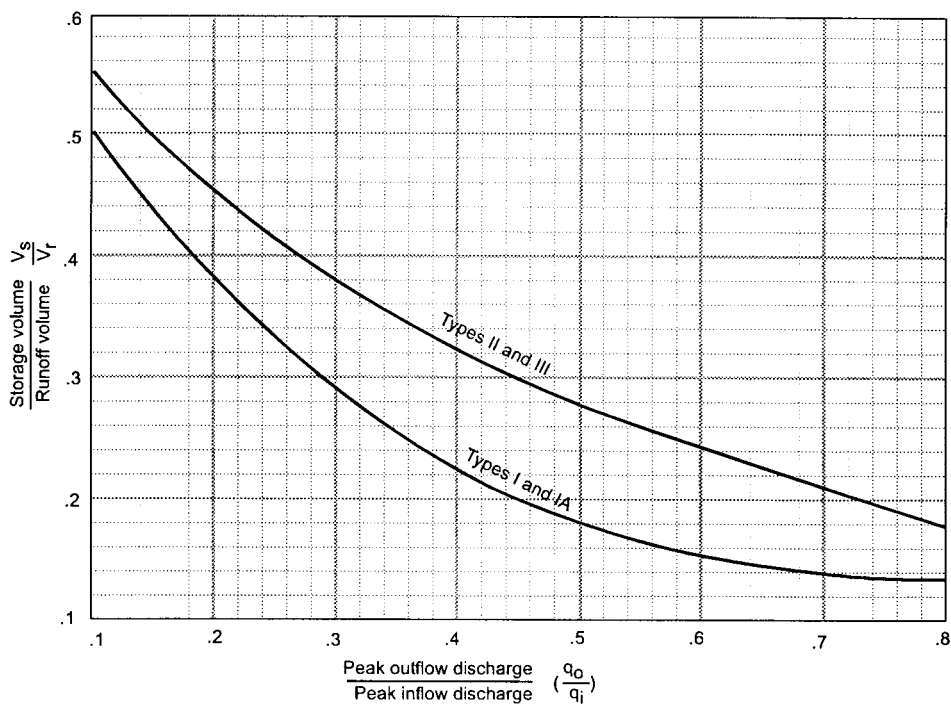


Figure B.2 Approximate Detention Basin Routing For Rainfall Types I, IA, II, and III (Source: NRCS, 1986)



## B.2 Water Quality Peak Flow Calculation

The peak rate of discharge for the water quality design storm is needed for the sizing of diversion structures for off-line practices such as sand filters. An arbitrary storm would need to be chosen using the Rational method, and conventional SCS methods have been found to underestimate the volume and rate of runoff for rainfall events less than 2". This discrepancy in estimating runoff and discharge rates can lead to situations where a significant amount of runoff by-passes the filtering treatment practice due to an inadequately sized diversion structure and leads to the design of undersized bypass channels.

The following procedure can be used to estimate peak discharges for small storm events. It relies on the Water Quality Volume and the simplified peak flow estimating method above. A brief description of the calculation procedure is presented below.

Using the water quality volume ( $WQ_V$ ), a corresponding Curve Number (CN) is computed utilizing the following equation:

$$CN = 1000/[10 + 5P + 10Q - 10(Q^2 + 1.25 QP)^{1/2}]$$

Where

P = rainfall, in inches (use the 90% rainfall event from Figure 4.1 for the Water Quality Storm)

Q = runoff volume, in inches

Once a CN is computed, the time of concentration ( $t_c$ ) is computed using guidance provided in TR-55.

Using the computed CN,  $t_c$  and drainage area (A), in acres; the peak discharge ( $Q_p$ ) for the water quality storm event is computed (either Type II or Type III in the State of New York).

Read initial abstraction ( $I_a$ ), compute  $I_a/P$

Read the unit peak discharge ( $q_u$ ) for appropriate  $t_c$

Using the water quality volume ( $WQ_V$ ), compute the peak discharge ( $Q_p$ )

$$Q_p = q_u * A * WQ_V$$

where  $Q_p$  = the peak discharge, in cfs

$q_u$  = the unit peak discharge, in cfs/mi<sup>2</sup>/inch

A = drainage area, in square miles

$WQ_V$  = Water Quality Volume, in watershed inches

## References

- Harrington, B.W. 1987. Design Procedures for Stormwater Management Extended Detention Structures. Report to Water Resources Administration. Maryland Department of Natural Resources. Annapolis, MD.
- Maryland Department of the Environment (MDE). 2000. Maryland Stormwater Design Manual. Baltimore, MD.
- Natural Resources Conservation Service (NRCS). 1986. Urban Hydrology for Small Watersheds. Technical Release No. 55. USDA. Washington D.C.

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# Appendix C

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