

GEOTECHNICAL INVESTIGATION REPORT

FOR

Liberty Towers-Site A and Site B Richmond Terrace Staten Island, Richmond County, New York

PREPARED FOR:

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1.0 INTRODUCTION

We have completed our geotechnical investigation of the subsurface conditions as they pertain to establishing site preparation procedures and foundation design criteria for the proposed construction to be located at along Richmond Terrace and Stuyvesant Place in Staten Island, NY. Survey drawings indicate that the site comprises two parcels, both less than 1 acre in size. An approximate 50' wide utility right of way bisects the two parcels. Our investigation incorporated both of the parcels into one site, bordered by Stuyvesant Place and Richmond Terrace to the East, Richmond Terrace and residential structures to the north, two approximately 20-story residential building towers to the west, and Hamilton Avenue to the south. The majority of the site slopes from the southwest at elevation 84' (msl) to the northeast at elevation 40' (msl). Figure 1 presents a topographic map depicting the site.

Site observations revealed that the site is mainly undeveloped, heavily vegetated, and contains aged concrete walls and possible former walkways and stairways along the northeastern parts of the site; new concrete foundations in the northernmost part of the site, and several piles of debris, including construction debris. Some portions of the site could not be accessed by the drill rig due to excessive grades. It appears that the site was formerly occupied by previously demolished structures.

The design plans indicate that proposed construction will consist of two residential towers, Tower A and Tower B, each approximately 20 stories high, additional midrise building areas and 2 to 3 levels of below grade parking throughout the entire building footprint. It appears that an excavation support system will be required to reach the proposed subgrade elevation for the entire perimeter of the proposed buildings. Some underpinning of adjacent structures may also be required during construction. We are currently designing a shoring and bracing and underpinning system for this project; the design will be submitted under a separate cover. The design plans also indicate that the footing elevations for the tower portions of the buildings will be approximately 27.5' msl in Tower A, and approximately 20' msl in Tower B, footing elevation for the remaining area in Tower A will be approximately 32.5' msl, and footing elevation in the remaining portion of Tower B will be approximately 34' msl.

It is our understanding that column loads will be as high as approximately 2,000 kips at some of the column locations. Rock cores collected at the site indicate rock with an end bearing capacity of either 20 tons per foot (tsf) or 8 tsf, depending on the condition of the rock. The footing schedule should be dependent on the condition of rock; and identification of the weaker rock areas can be made at the time of excavation.

Bedrock underlying the site has been identified as Serpentinite rock. Serpentinite is known to contain naturally occurring asbestiform minerals, to which occupational exposure is regulated by OSHA.

2.0 FIELD AND LABORATORY INVESTIGATIONS

Our engineering study included a site reconnaissance, a review of published geological information of the area, a review of geotechnical investigations completed by Santoro, P. E. in October 2006 and January 2007, a review of the preliminary design drawings, and a field investigation consisting of the drilling of nine (9) drilled borings; four (4) of which included rock cores.

SESI borings were completed to depths of 18.0 to 48.5 feet below existing grade, using a track mounted drill rig at the locations shown on Figure 2. All borings were backfilled upon completion. Individual boring logs, which describe the materials encountered, are presented in Appendix A. A key to soil terminology is also included in Appendix A. The locations of the borings completed by Santoro are also included on Figure 2, and the boring logs of borings completed by Santoro are included in Appendix B.

Soil samples suitable for identification purposes were extracted from the borings at various intervals in accordance with the procedures of the Standard Penetration Test (SPT) (ASTM D1586). For this test, a standard split spoon (2-inches outside diameter, 1 and three eighths inches inside diameter) is driven into the soil by a 140-pound weight falling 30 inches. The number of blows required for driving the sampler through four 6-inch intervals is recorded. After discounting the initial six inches of penetration due to possible disturbance of the material resulting from the drilling operation, the number of blows required to drive the sampler the second and third 6-inch intervals is recorded and referred to as the standard penetration number or N-value. It is also commonly called the blow count.

All fieldwork was performed under the full-time direct technical observation of a geotechnical engineer/technician from SESI Consulting Engineers, PC. Our representative maintained continuous logs of the explorations as work proceeded and supervised the soil sampling operations so as to develop the required subsurface information.

All soil samples extracted in the field were brought to our office where they were further examined in our soil mechanics laboratory.

Laboratory classification testing consisted of two (2) unconfined compression tests on specimens from two rock cores. The results of the compression tests are presented on the individual boring logs and in the text below.

3.0 GENERALIZED SUBSURFACE CONDITIONS

3.1 Geology

Geologically, the site soils are mapped as younger glacial ground moraine; or glacial till. This soil is chiefly an unsorted mixture of clay, silt, sand, gravel and boulders. Soils at the site were found to contain predominately sand sized particles, with silt, occasional bounders, and little gravel. Underlying the soils is Serpentinite bedrock, which is classified as massive or schistose, thoroughly sheared and broken by innumerable intersection zones of weak, friable and slippery material of low strength. Rock joints are common and closely spaced, and generally exhibit random orientation and little structural significance. This type of rock is said to have very low compressive strength.

In addition, Serpentinite is known to contain naturally occurring asbestiform minerals, to which occupational exposure is regulated by OSHA.

3.2 General Subsurface Conditions

All SESI and Santoro borings were completed in the proposed building area footprints. Fill was encountered at each boring location, and all SESI borings were terminated at the depth of bedrock, or in the bedrock. Generally, three soil Strata were encountered, as described below:

<u>Stratum 1:</u> FILL: A fill layer consisting primarily of brown silty sand, little gravel, little silt and widely varying amounts of boulders, brick, wood and other small amounts of debris was encountered over the site. Our borings indicate the depth of the fill varies from approximately 5' to approximately 15' below grade, at the locations investigated.

The fill is in a medium to medium dense condition; however, it is not suitable for support of building foundations in its current condition. Uncontrolled fill has no allowable bearing capacity because of its unknown overall quality and density.

In addition to the fill encountered in the borings, there were several piles of existing fill on the site that were not investigated.

<u>Stratum 2</u>: SAND: Beneath the fill layer, a red-brown to olive brown silty sand with little gravel layer was encountered. Some cobbles and fractured weathered rock were also evident in this layer, in particular, the occurrence of fractured rock increased with depth. The depth of this stratum ranges from 5 feet to greater than 45 feet below grade. This stratum is in a dense to very dense condition, with an allowable bearing capacity of approximately 3.0 tons/per square foot (tsf).

Stratum 3: Weathered rock and Serpentinite bedrock was encountered between approximately 17 feet and 45 feet below grade. A weathered rock layer was located

above the bedrock elevation, the thickness the weathered zone ranged from 1' to 5' thick. Bedrock elevations, based on the topographic information on the plans range from approximately 35' msl near the intersection of Hamilton Avenue and Stuyvesant Place to approximately 14' msl near the northeastern boundary of Tower A. Bedrock elevations are indicated next to the corresponding boring location on Figure 2, "Boring Location Plan".

Cores were collected in approximately 5-foot runs, using a double barrel NX core sampler drilled with a track mounted drill rig. Recovery rates and Rock Quality Designations (RQD) were established for each rock core obtained. The Rock Quality Designation, which is an indication of the soundness of the rock, is determined by the cumulative length of rock core pieces in excess of 4 inches divided by the total length of rock cored. In general, the RQD values ranged from 0% to 88%. A complete rock description is included on the boring logs including recovery and RQD values. The chart below shows the relationship between RQD values and rock quality. Unconfined compression testing was completed on two rock pieces from the cores, the results of which were 5,580 psi and 5,770 psi. The unconfined compression test results are included in Appendix C.

RELATIONSHIP OF RQL	O AND ROCK QUALITY
ROCK QUALITY DESIGNATION (RQD)	DESCRIPTION OF ROCK QUALITY
0-25	VERY POOR
25-50	POOR
50-75	FAIR
75-90	GOOD
90-100	EXCELLENT

The rock is medium to fine grained, greenish gray Serpentinite. The condition and RQD and therefore the quality of the rock, varied across the site. Cores were collected in borings SB-1, SB-2, SB-5, and SB-7.

Cores collected from borings SB-1, SB-5 and SB-7 contain rock that is very strong to strong, hard, unweathered to slightly weathered, and moderately fractured. SB-1 was located towards the rear of Tower B, SB-7 was located towards the rear of Tower A and SB-5 was located towards the front of Tower A.

Cores collected from SB-2 contain rock that is very weak, soft, highly weathered and extremely fractured. The rock quality did not increase with depth. SB-2 was located towards the front of Tower B.

A summary of the rock core characteristics and rock bearing capacity is presented below:

Boring Number	Average Recovery	Average RQD %	Rock Quality	Unconfined Compressive	Bearing Capacity
	%			Test Result (psi)	(Tsf)
SB-1	98	73	Fair – Good		20
SB-2	50	8.5	Very Poor	5,580	8
SB-5	100	59	Fair	5,770	20
SB-7	92.5	49.5	Fair		20

<u>Groundwater:</u> Groundwater was encountered only in boring SB-5 at 28' below grade at the time of boring. Groundwater can sometimes be slow to infiltrate borings and can be highly seasonally variable; therefore, some groundwater infiltration should be expected during construction, especially during periods of wet weather. In addition, groundwater on the site may be tidally influenced, due to the proximity of The Narrows.

4.0 EVALUATION AND RECOMMENDATIONS

4.1 General

Fill was encountered at all boring locations, and as stated above, uncontrolled fill has no allowable bearing capacity. Based on the topographic information, it appears that the proposed building footing elevations are below the maximum depth of the fill; however, it is possible that there are areas on the site where the fill extends below the proposed footing depth. Footings and other structural building elements should not be allowed to bear on the fill in its present state of compaction.

The mainly sand soil layer beneath the fill has an allowable bearing capacity of 3.0 tsf, and the rock layer beneath the fill has allowable bearing capacities of 8 tsf or 20 tsf, depending on the condition of the rock. Based on the topographic information provided, some of the proposed building footing elevations are above the top of rock and some are at or below the top of rock.

4.2 Site and Building Area Preparation Procedures

In general, the building area preparation procedures should consist of installing the perimeter excavation support system in order to support the surrounding streets, existing structures and existing utilities, and overburden soils. Once the perimeter excavation support system is in place, the mass excavation of the site may commence. This operation will involve excavation of the existing fill and sand soils and loading this material into trucks for removal from the site.

The plans indicate that the majority of the soil within the building footprints will need to be excavated to the elevation of bedrock to reach foundation subgrade elevation; however, for any foundation footings that will be placed on soil, the footing subgrade should be proof-rolled with a large vibratory roller prior to the placement of concrete. The proofrolling operation should consist of making 4 complete coverages of the area. Any soft areas disclosed should be excavated to stable material and backfilled in compacted lifts to achieve 95 percent of Modified Proctor Density (ASTM D 1557).

Any fill required should be placed in maximum 12-inch thick lifts, with each layer compacted to the required density using a large vibratory roller (minimum 10-ton static drum weight). Building area fills should be compacted to a minimum of 92 percent and an average of 95 percent of the maximum Modified Proctor Density (ASTM D 1557).

Areas that will not have any foundations or other structural loads may be compacted to a minimum of 90 percent of the maximum Modified Proctor Density (ASTM D 1557).

Offsite borrow material, if required, should have a maximum particle size of 6 inches and the maximum amount of fines (percentage passing a No. 200 mesh sieve) should be 15% to help facilitate construction during wet weather. The "fines" should be non-plastic. The granular fill should be compacted using a heavy vibratory roller (Dynapac CA-15 or equivalent) to achieve the same density requirements as above.

Backfill in confined areas such as utility trenches and foundations within load bearing or paved areas should be placed in maximum 8-inch thick layers and compacted to a minimum of 92 percent and average of 95 percent density as described above.

It appears that the majority of the onsite soils will be satisfactory for use as structural fill. Wetting or drying of the fill material should be accomplished as necessary to achieve the required density. The subgrade should be graded to drain and tight-rolled at the end of the day, if wet weather is anticipated.

If stormwater seepage is encountered during construction, gravel filled sumps with pumps should be installed below the subgrade elevation to allow for dewatering of the excavation. We recommend that the building be constructed with drainage sumps placed at the lowest levels to allow for permanent dewatering. The need for an underslab drainage system should be evaluated during construction.

4.3 Foundation Design Criteria

Footings may be placed on the natural inorganic soil, bedrock, or the controlled compacted fill. As stated above, footings and other structural building elements should not be allowed to bear on the fill in its present state of compaction. Footings bearing on the natural inorganic soil or controlled compacted fill shall be designed for a maximum net allowable bearing pressure of 3.0 tsf (6,000 psf). Footings bearing on the bedrock shall be designed for a maximum net allowable bearing pressure of 8 tsf (16,000 psf) for highly weathered rock or 20 tsf (40,000 psf) for slightly to unweathered rock. The condition of the rock will need to be determined in the field by a geotechnical engineer during the controlled inspections required by the NYCDOB.

Regardless of the loads, the minimum plan dimension of isolated footings should be 36 inches and the minimum width of continuous footings should be 20 inches. Exterior footings and those footings potentially exposed to frost action should be founded a minimum of 3.0 feet below adjacent exterior grade.

All other temporary excavations greater than 4 feet in depth should have the sides sloped back to a maximum slope of 1.5 horizontal to 1 vertical or be appropriately sheeted and braced in accordance with all applicable codes. Flatter side slopes will be required if the excavation extends below groundwater.

Because groundwater seepage will likely be encountered in some of the footing excavations, over-excavation may be required along with placement of a minimum of 6 to 12 inches of ³/₄ inch clean crushed stone. Any groundwater seepage should be directed to a sump for pumping.

The floor slab should be designed using a subgrade modulus of 175 pci, assuming that 6 inches of dense graded aggregate is placed beneath the slab.

All retaining walls, including foundation walls, should be provided with positive drainage behind the walls to preclude hydrostatic pressures from developing.

After satisfactory completion of the outlined building area preparation procedures, footings and floor slabs founded on the compacted structural fill/natural soils should have post-construction total settlements of less than 1-inch and maximum differential settlements in a 30 foot span of less than ½ inch.

A summary of recommended soil design parameters is included in Table 1.

Seismic Design

The site soils and highly weathered bedrock have been classified as Site Class S_1 for seismic design purposes in accordance with the Building Code of the City of New

York, 2008 (NYC Code). The unweathered to slightly weathered bedrock on the site has been classified as Site Class S_0 for seismic design purposes.

The Reference Standards, (RS-9-6) of the NYC Code require that the soil profile be evaluated for the potential for liquefaction in the event of a seismic occurrence. The Reference Standard identifies liquefaction potential relating to the blow counts obtained during the sampling operation. The blow counts obtained during the sampling operation indicated that the soils would be classified as "liquefaction unlikely", or Category C.

4.4 Footings on Rock

Because of the variation in the condition of the rock encountered on site, the footing schedule will have to vary to compensate for the rock that is highly weathered. Footings on sound unweathered to slightly weathered rock may be designed for a maximum net allowable bearing pressure of 20 tsf (40,000 psf). For the building columns with large loads, ie 2,000 kip, conventional shallow footings should prove to be the most economical. Footings on highly weathered rock may be designed for a maximum net allowable bearing pressure of 8 tsf (16,000 psf). Column footings with large loads over the highly weathered rock can be designed as a mat foundation, or alternatively, drilled shafts can be used.

A mat foundation over the highly weathered rock should be designed for a maximum allowable net bearing pressure of 8 tsf with an allowance for localized bearing overstress of 25% due to static, live and dead loads. Additional bearing stress resulting from wind and seismic loads should not be included with the static analysis. In addition, a modulus of subgrade reaction of 160 tons/c.f. may be used for design of the mat foundation.

Drilled shafts may consist of multiple smaller diameter shafts with a cap, or one large drilled element. The following design parameters can be used for the highly weathered rock.

End Bearing Capacity: 8 tsf.

Ultimate bond stress-Rock/concrete bond-50 psi.

Exposed surfaces of highly weathered rock may rapidly degrade, leading to a further reduction in allowable bearing capacity. To avoid this, it is advisable to install a thin concrete mud mat over exposed surfaces of the highly weathered rock after the overburden soils are excavated.

<u>Bedrock Footings:</u> The load capacity of the bedrock is dependent on the quality of rock. The occurrence of weathered and unweathered rock will likely be somewhat variable across the site. It is necessary that a geotechnical engineer from our office be on site during excavation to make the determination of the condition of the rock and the required footing schedule at most of the column footing locations.

4.5 Environmental Consideration of Serpentinite Rock

As stated above, bedrock underlying the site has been identified as Serpentinite rock. Serpentinite is known to contain naturally occurring asbestiform minerals, to which occupational exposure is regulated by OSHA.

Asbestos becomes hazardous when it is physically disturbed and released into the air as a potential airborne contaminant. Physical disturbance of naturally occurring asbestos minerals can be generated by natural weathering and erosion of steep serpentinite rock slopes or by excavation, drilling, blasting, chipping, or crushing of asbestos containing rock.

To confirm the presence of asbestos in the rock at the site, laboratory analyses on rock samples should be performed by a certified asbestos laboratory following applicable USEPA methodologies. If the rock is found to contain asbestos, special handling procedures should be developed in a written site specific Health and Safety Plan, and/or Material Handling Plan.

Mitigation procedures for construction sites with known asbestos minerals generally consist of wetting the excavated rock for dust control, personal and community air monitoring, and controlled disposal of asbestos containing rock.

4.6 Temporary Earth Support

In order to attain the elevation of the proposed lower parking level, an earth retention system will be required to support the soils surrounding the excavation. A retention system consisting of soldier beams with timber lagging is the most common form of earth retention and generally the least expensive. Timber lagging is installed to the soldier beam through direct bearing of the timber on the beam or attached mechanically to the piles as the mass excavation proceeds. Over-excavation for the installation of the lagging should be limited to four feet and all excavated areas should have all lagging installed at the completion of each work shift. Additional bracing to the system in the form of tiebacks or raker beams will be required due to the depth of the proposed excavations. The tiebacks are installed by rotary or augerdrilling techniques, drilled through the earth retention wall line into the retained soil behind the wall at specified elevations as the mass excavation proceeds. A steel tendon is then inserted into the drilled hole and injected with grout under pressure. After allowing the grout to harden, the steel tendon is stressed to a specific tension and locked into the soldier beam to restrain it from moving. Temporary easements for the tiebacks that encroach on the neighbors' property will be required

The raker beam support provides the necessary support with steel beams supported at the base of the excavation and propped along the sidewalls of the system. In this system the raker beams are left in place until the walls are backfilled and the structure is self-supporting. Penetrations through the building walls and floors will require closure once the rakers are removed.

Alternately, the mass excavation may be supported through the use of a soil nail system. This system involves drilling steel rods into the slope to be supported, in a predescribed pattern to a design length based on the height of the excavation. These steel rods are grouted in place and covered with a reinforced shotcrete face.

The final selection of the type of support to be employed on this project is beyond the scope of the investigation; however, we are currently designing a system for shoring and bracing and underpinning for the project, and will submit the design under a separate cover.

4.7 Lateral Earth Pressures

It is recommended that walls subject to unbalanced earth pressures be designed for the following minimum lateral soil pressures (calculated on the basis of an equivalent fluid pressure in pounds per foot)

Active Case =	36 pcf
At-Rest Case =	56 pcf

The active case would apply to wing walls such as in loading docks where deflection of the wall would be permissible. The at-rest condition exists for those walls that are restrained at both the top and bottom of the wall such as the pit walls within an elevator pit or basement/foundation walls. Walls subject to surcharge loads must be designed for an additional uniform lateral pressure over the entire height of the wall equal to 0.3 times the surcharge loading. All retaining walls, including foundation walls, should be provided with positive drainage behind the walls to preclude hydrostatic pressures from developing.

5.0 TESTING REQUIREMENTS

During the placement of all structural fill, visual observations and density tests should be performed to determine the adequacy of the fill. Density testing should be done in accordance with the following minimum frequency requirements:

Building Areas: Minimum of 4 tests per 12-inch lift; spacing not to exceed 100 feet between test locations.

<u>Parking/Roadway Areas:</u> Minimum of 3 tests per 12-inch lift; spacing not to exceed 100 feet between test locations.

<u>Retaining Wall(s)</u>: Minimum of 4 tests per 12-inch lift; spacing not to exceed 50 feet between test locations.

Minimum density requirements are outlined in the previous sections of this report.

6.0 UTILITY LINES

The site soils will provide suitable support for utility lines. Cobbles greater than 4 inches in diameter should be removed from the utility line subgrade or a minimum 4-inch thick sand layer placed beneath the utility lines.

Backfill material placed around utility lines to 6 inches above the utility lines should have a maximum particle size of 1.5 inches. Backfill of utility trenches that fall within load-bearing areas should be placed in maximum 8-inch thick lifts and compacted to a minimum of 92 percent and average of 95 percent of Modified Proctor Density (ASTM D-1557).

7.0 PAVEMENT AREAS

The cut soils may be used as fill in paved areas; however, as previously discussed, if these soils possess a high percentage of silt/clay, they cannot be worked or compacted when wet. In order to reuse these soils, they may need to be spread out to let dry or treated with lime/cement to reduce the moisture content and make them workable.

The compaction criteria for fills in parking and roadway areas may consist of 92 percent (ASTM D-1557), except in the uppermost 2 feet where 95 percent should be achieved to provide for good pavement support. Visual observations and in-place field density tests should be made to determine the adequacy of the compaction.

8.0 INSPECTION

The recommendations presented in the previous sections of this report are based on the assumption that the site preparation procedures will be done under engineering inspection by a representative of this office. SESI should inspect the proofrolling operations, the placement of the compacted fill and the bottom of the footing excavations prior to the placement of concrete and/or stone, and prior to form or steel reinforcement for column footings. Visual observations and in-place density testing should be done throughout fill construction and column footing excavations to determine that the work is done in accordance with our recommendations.

We should review the grading plan and foundation plan, when completed, to determine if any revisions to our recommendations are necessary.

9.0 LIMITATIONS

The subsurface investigation performed identifies the subsurface conditions only at the locations of the test holes and at the depths where the samples were taken. SESI Consulting Engineers, PC, reviews the published geologic data and the field and laboratory data and uses their professional judgment and experience to render an opinion on the subsurface conditions throughout the site. Since the actual subsurface conditions may differ, we recommend that SESI be retained to provide construction inspection in order to minimize the risks associated with unanticipated conditions.

10.0 DISCLAIMER

This Report was prepared by SESI for the sole and exclusive use of Truisi Suk Design. Nothing under the Professional Services Agreement between SESI and its client, Truisi Suk Design shall be constructed to give any rights or benefits to anyone other than Client and SESI, and all duties and responsibilities undertaken pursuant to the Agreement will be for the sole and exclusive benefit of Client and SESI and not for the benefit of any other party. This Report has been prepared and issued subject to the express condition that same is not to be disseminated to anyone other than Client, without the advance written consent of SESI (which SESI, in its sole discretion, is free to grant or withhold). Use of the Report by any other person is unauthorized and such use is at the sole risk of the user.

TABLE 1 SUMMARY OF SOIL DESIGN PARAMETERS

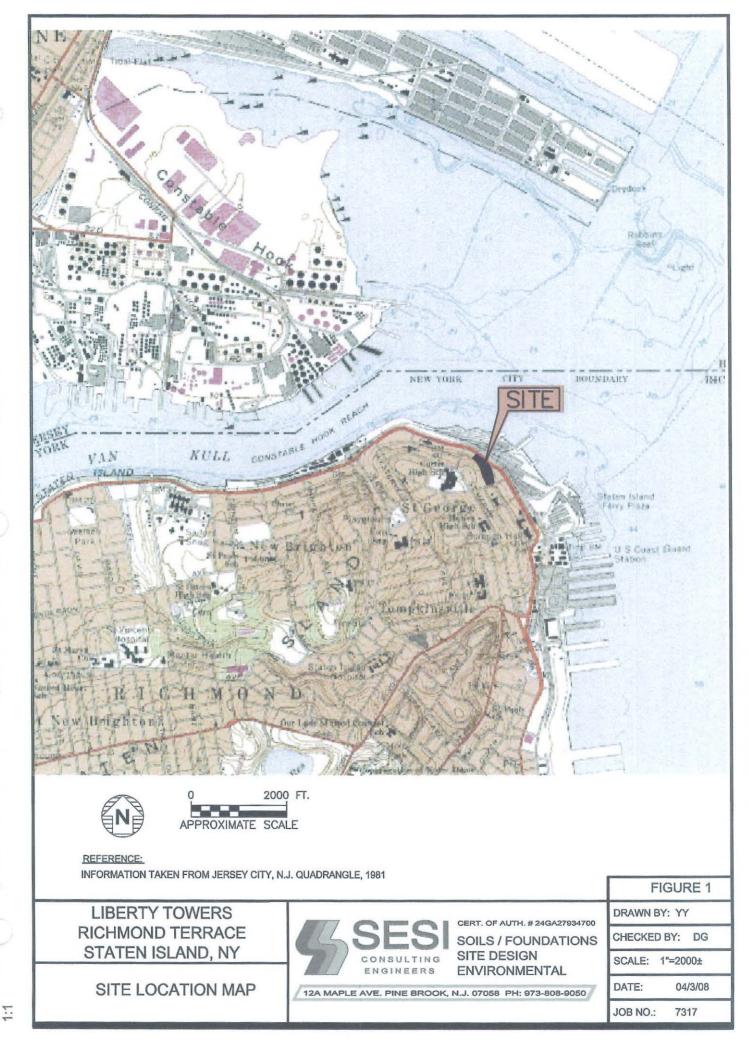
1.	PARAMETER Allowable Bearing Capacity (net)	VALUE
1.	Natural Soil/Compacted Fill Rock – sound, un-weathered	6,000 psf
	to slightly weathered Rock – highly weathered	20 tsf 8 tsf
2.	Total Unit Weight (Onsite/Imported Soil)	125 pcf
3.	Angle of Internal Friction - Backfill against Structures	32 degrees
4.	Earth Pressure Coefficient (See Note 1) Active Earth Pressure (Ka) Earth Pressure @ Rest (Ko) Passive Earth Pressure (Kp)	0.31 0.50 3.25
5.	Coefficient of Sliding (concrete over soil)	0.40
6.	Subgrade Modulus for Floor Slab Design (Granular Fill)	175pci
7.	Slopes (Above Groundwater) Maximum Cut Slope in Soil Maximum Fill Slope in Soil	2.5H:1V 2.5H:1V
8.	Footing Depth for Frost Protection	3.0 ft
9.	Seismic Design Criteria- Site Class	S_1

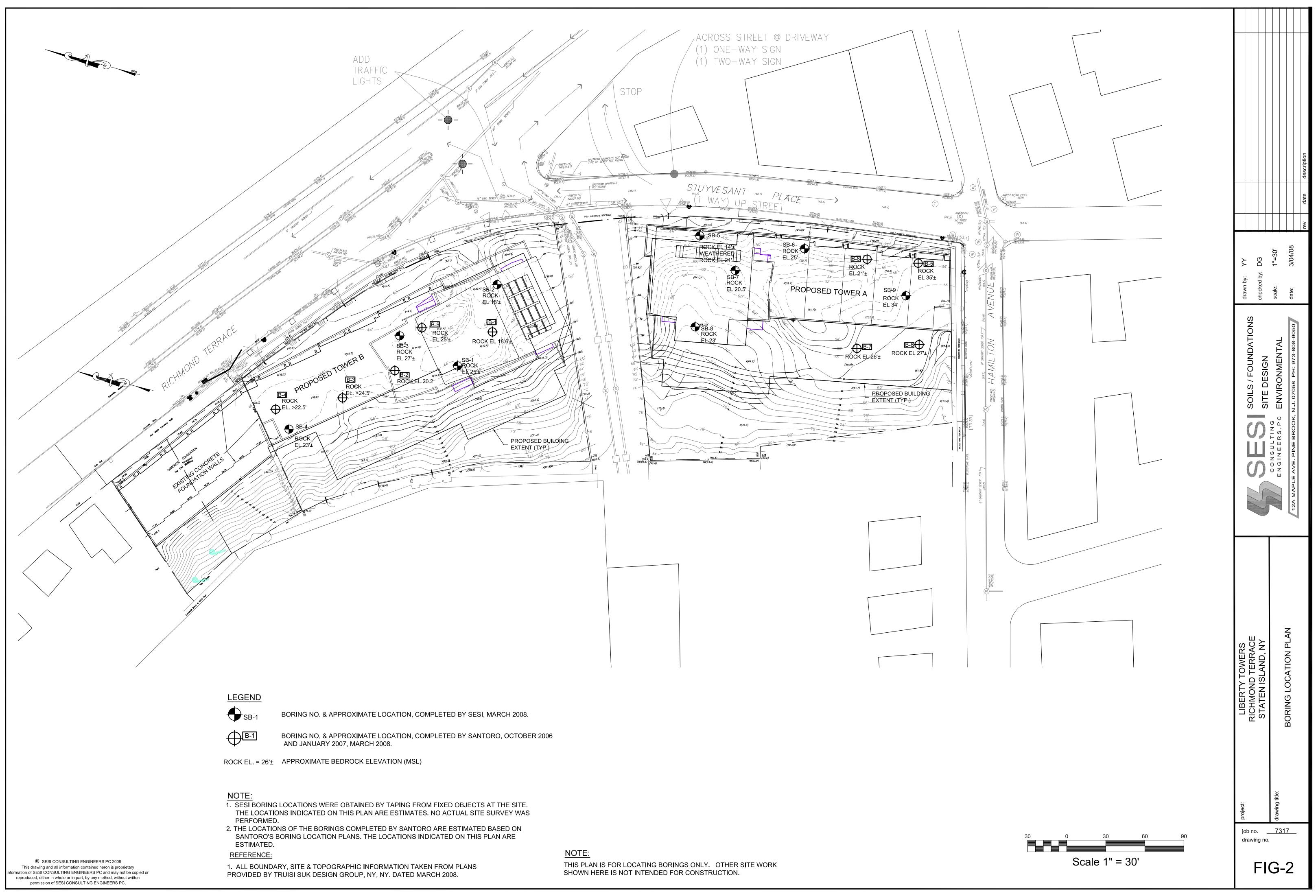
Notes:

A drainage medium should be installed along all retaining walls to avoid hydrostatic pressures from developing.

Compaction equipment used within $5\pm$ feet permanent walls should not weigh more than 5,000 pounds.

FIGURES





APPENDIX A

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6	777 C				PF	OJECT	NAME:	Liberty	Tower	s BORING NO. SB-	-1						
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Ť	SS	S-2	5	7	. 4	6	11	12	15	FILL: Brown fine SAND, trace of Gravel, trace of Silt,							
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	SS	S-3	10	12	28	27	29	30	12	Brown fine SAND, some Silt, trace of Gravel, Boulders							
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20		ļ		<u> </u>	<u> </u>		 			(4-65)							
		Run-1	20	25	3	min				Core Run-1, 20' - 25'; REC = 100%; RQD = 88%	and the second						
					5	min	<u> </u>			Serpentinite, gray, massive, very strong, hard, medium to fine							
		<u> </u>		<u> </u>	5	min			ļ	grained, unweathered, slightly fractured, randomly oriented							
1000			<u> </u>	├───	4	min				joints, some highly angled							
25				1	5	min	İ	1		(3-65)							
		Run-2	25	30	3	min	ĺ			Core Run-2, 25'-30', REC = 100%; RQD = 61%	and the balance of th						
					5	min				Serpentinite, gray, massive, very strong, hard, medium to fine							
294650000					4	min		1		grained, unweathered, slightly fractured, randomly oriented							
]	4	min				joints, some highly angled	119407/// Made /						
30)		ļ	<u> </u>	4	min		ļ	ļ	(3-65)	and the second secon						
		Run-3	30	35	4	min	<u> </u>	<u> </u>		Core Run-3, 30'-35'; REC = 93 %; RQD = 70%	TAN DAMAGAMATAN						
			<u> </u>	<u> </u>	6	min	ļ	<u> -</u>	ļ	Serpentinite, gray, massive, very strong, hard, medium to fine							
		<u> </u>	<u> </u>	<u> </u>	5	min	<u> </u>		<u> </u>	grained, unweathered, slightly fractured, randomly oriented joints, some highly angled							
0.		<u> </u>	┢────		5	min				(3-65)							
35	<u>}</u>		┣───	┼───	7	min				***	**************************************						
	·····	1	┢━━━				 		<u> </u>	Boring Complete @ 35'							
		<u>}</u>	 	<u> </u>	1	<u> </u>		-	┢━━━	•	(1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.						
-		<u> </u>	<u>}</u>	<u> </u>	<u> </u>		<u> </u>			- ⁻	Print - 1970 - 1971 - 1970						
40	,	1	 	 	†	<u> </u>		1	1								
L	، من تش الي <u>من من من المحمد /u>								. <u>.</u>		و معدم معد من معالم م ا						
Non	ninal I.D. of	Hole			in	The sub	surface i	informati	on show	hereon was obtained for the design and estimating purposes for our client							
<u></u>	ninal I.D. of	and the second	Sample	r	t and the second se	1				users only that they may have access to the same information available							
	ght/type of I									od faith, but it is not intended as a substitute for investigations, interpretation)118						
ei	ght/type of I	Hammer or	n Split Ba	arrel		140 lb or judgment of such authorized users. Information on the logs should not be relied upon without the geotechnical											
Dro	o of Hamme	or on Drive	Pipe		l in	in engineers recommendations contained in the report from which these logs were extracted.											
Cor	e Size				in] P	p: Pocke	t Penetro:	meter; W	OH: Weight of Hammer; WOR: Weight of Rod							

Approximate Change in Strata: ______ Inferred Change in Strata:

Soil descriptions represent a field identification after D. M. Burmister unless otherwise noted.

											the second s	во	BORING NO.				SB-2
ACCOUNTS ON THE			onsult	ING			LOC	ATION:	Staten	Island	, NY		3 NO.				7317
	<u> </u>		SNGINEE				4 mm			GROUND ELEVATION: 3/7/2008 GROUNDWATER TABLE DEPTH : NE							13.0' ±
			eneral Bori	ngs			TE STA			10 March 10				3		NE Date	
	JEPTH	CTOR: G		DEP	тн	DATE	COMPL	EIED:	3/10/	2008		ate _{N/A}		24 Hr.	N/A	Juale	
and the second	(ft)	METHOD	SAMPLE	FROM	то	E	3lows or	n Spoon		REC SOIL DESCRIPTION AND STRATIFICATION						ON	SYMBOL
10100	0		No.	(ft)	(ft)	0/6	6/12	12/18	18/24	(in)							
-		SS	S-1	0	2	24	29	31	34	10	FILL: Brown SILT	T, some f	ine Sa	nd, trace	Gravel,	Asphalt	
											(11-65)						
Property listen																	
	5				غدا الأل _{ال} ي وي جمي حدمه							~ ~	145705				
Distant		SS	<u>S-2</u>	5	7	9	12	16	16	15	FILL: Yellow brow (11-65)	wn fine S	AND,	some S1	II, trace (Jravel	
										l <u></u>							
and the second																	······································
	10																
		SS	S-3	10	12	17	25	35	24	18	Gray brown coarse	se to fine	SANI	D, some S	Silt, trace	Gravel,	
A DESCRIPTION OF A DESC											Boulders						and the second
										ļ	(7-65)						
	45																
	15	SS	Q 4	1.0							Brown medium to fine SAND, some Silt, trace Gravel,						
		- 33	S-4	15		80/4				12	Boulders	mic 3Ai	ND, 50	nne ont,	uace ora		
				<u> </u>							(7-65)						annoninensegnet ^{en} t
								·····									
	20																
-Carpendar - Bar)	SS	S-5	20	22	32	33	36	33	10	Gray brown mediu		e SAN	D, some	Gravel,	some Silt	
	North Contraction of								<u> </u>	Į	with fractured Roc (7-65)	СК					
				<u> </u>													
	25	ss	S-6	25	27	50/2"				2	Brown medium	n to fine S	Sand s	ome Gra	vel. some	Silt with	
			Run-1	25	30	3	min		}	<u> </u>		fracture					
			1		<u> </u>	2	min		<u> </u>		Core Run-1, 25'-3	30'; RE(C = 33	%; RQI) = 0%:		
						4	min				Serpentinite, light						0
			<u> </u>			2	min		ļ	<u> </u>	fine grained, highl	ly weath	ered, e	xtremely	fractured	1	
	30	[L	L	4	min	L	<u> </u>	<u> </u>	(4-65)				0.0		
			Run-2	30	35	2	min		ļ	<u> </u>	Core Run-2, 30' -	- 35'; RI	C = 8	v.y%; R	QD = 26	10	
		, , , , , , , , , , , , , , , , , , ,	1		<u> </u>	3	min min		رور جهان ال		Serpentinite, light						o 🔤
			1		<u> </u>	3	min			<u> </u>	fine grained, highl	ly weath	ered, e	xtremely	fractured	1	
	35		1		1	4	min		†	1	- (4-65)						
			Run-3	35	40	2	min			<u> </u>	Core Run-3, 35' -	- 40'; RI	EC = 4	1%; RQ	D = 8.39	%	
						2	min				Comontinite links				aale aafe	modium	
			<u>3</u> min								Serpentinite, light green, massive, very weak, soft, medium to fine grained, highly weathered, extremely fractured						
	<i></i>		<u> </u>	<u> </u>		4 ·	min	Į	ļ	ļ	(4-65)						
	40			[3	min		<u> </u>								

		the second s	
	Nominal I.D. of Hole	in	The subsurface information shown hereon was obtained for the design and estimating purposes for our client.
	Nominal I.D. of Split Barrel Sampler	1¾ in	It is made available to authorized users only that they may have access to the same information available
مسح	Weight/type of Hammer on Drive Pipe	300 lb	to our client. It is presented in good faith, but it is not intended as a substitute for investigations, interpretations
	sight/type of Hammer on Split Barrel	140 lb	or judgment of such authorized users. Information on the logs should not be relied upon without the geotechnical
~	Drop of Hammer on Drive Pipe	in	engineers recommendations contained in the report from which these logs were extracted.
	Core Size	in	Pp: Pocket Penetrometer; WOH: Weight of Hammer; WOR: Weight of Rod
			-

Approximate Change in Strata: ______ Inferred Change in Strata:

Soil descriptions represent a field identification after D. M. Burmister unless otherwise noted.

FIGURE 4

MTT CECI PROJ								NAME:	Mea	Meadowlands Hospital Addition BORING NO. SE					
		TO Car	n Berneren V	28			LOC	ATION:		Se	ecaucus, NJ	JOB NO.	73	00	
			INGINE	ा म् स् ह मि क्षे							21044/1	GROUND ELEVATION:	43.	<u>)' ±</u>	
	BORIN	IG BY: G	eneral Bori	ngs		DATE	STARTI	ED	3/7/2	2008	GROU	GROUNDWATER TABLE DEPTH: NE			
	-	CTOR: G	P			DATE	COMPL	ETED	3/10/	2008	0 Hr. NE Date	N/A 24 Hr. N/A	Date N/A		
	фертн		SAMPLE	DEF	РТН 		Blows o	n Spoor	,	REC					
	(ft)	METHOD	No.	FROM	то						SOIL DESCRI	PTION AND STRATIFICATIO	N	SYMBOL	
				(ft)	(ft)	0/6		12/18	18/24	(in)					
			Run-4	40	45	3	min				Core Run-4, 40' - 45';	REC = 46%; RQD =0%			
						3	min				Serpentinite, light green	n, massive, very weak, soft, m	edium to		
						2 2	min min					athered, extreemly fractured			
	45					2	min				(4-65)				
					<u> </u>		11114					سے ایک			
				<u> </u>							Bor	ring Complete @ 45'			
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	Contraction of the local division of the loc	the second second second second second second second second second second second second second second second s	Split Barrel	Samnle								re access to the same information		14.	
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"" And the second	the second second second second second second second second second second second second second second second s		lammer or	· · · · · · · · · · · · · · · · · · ·			-1	to our client. It is presented in good faith, but it is not intended as a substitute for investigations, interpretations or judgment of such authorized users. Information on the logs should not be relied upon without the geotechnical							
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	Core S					Contraction of the local division of the loc	in Pp: Pocket Penetrometer; WOH: Weight of Hammer; WOR: Weight of Rod								
	<u></u>						~					ange in Strata:			

Soil descriptions represent a field identification after D. M. Burmister unless otherwise noted.

	4 L C				PF			Liberty			BORING NO.				SB-	3
		ONSULT	TING			LOC	ATION:	Staten	Island		JOB NO.				731	**************************************
		ÉMGINEE									GROUNE				45.0'	¥
Serence and the second		eneral Bori	ings				ARTED:	3/2/2			IDWATER			NE	AND INCOMENCE	
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(ft)	METHOD	SAMPLE	FROM	то		Blows o	n Spoor	1	REC	SOIL DESCRI				111		SYMBOL
0	INC INCO	No.	(ft)	(ft)	0/6	6/12	12/18	18/24	(in)				hiloAnd	X14		51101806
<u> </u>	SS	S-1	0	2	7	12	14	22	10	FILL: Olive brown SIL	T some S	and little	e Gravel		┿	
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egy and the second second second second second second second second second second second second second second s	[<u> </u>	ļ			<u> </u>	Į		(7-65)						r ta The Carl Section State Section
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15		0.4	<u> </u>			- 10				Red brown clayey SILT						
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rich and a second			<u> </u>	···						Weathered Rock @ 17^{\prime} (4-65)						FEATURE CONTRACTOR VALUE
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Service and and a service of the ser		Split Barre	Sample	<u>۲</u>	Contraction of the second second second second second second second second second second second second second s	-1				users only that they may have						
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Core		стеророк (1994) - 44 - 44 - 44 - 44 - 44 - 44 - 44		20Cm301+609+001	ir	-	engineers recommendations contained in the report from which these logs were extracted. Pp: Pocket Penetrometer; WOH: Weight of Hammer; WOR: Weight of Rod									
						Approx	timate Ch	nange in S	Strata: _	Inferred Ch	ange in Stra	nta:				
Soil de	escriptions	represent a	field ider	utification	after D.	M. Buri	nister un		wise no	ted.						

I	17	77 C				PF	OJECT	NAME:	Liberty	Tower	s BORING NO. SB-	4							
		77) %	26.5				LOC	ATION:	Staten	Island	NY JOB NO. 731	7							
	<i></i>		ENGINEE	ING IRS							GROUND ELEVATION: 48.0'	±							
	BORIN	G BY: G	eneral Bori	ngs		DA	TE ST	ARTED:	3/7/2	2008	GROUNDWATER TABLE DEPTH : NE								
		CTOR: G	P			DATE	COMP	LETED:	3/7/2008		O Hr. NE Date N/A 24 Hr. N/A Date N/A								
²	DEPTH		SAMPLE	DEF	~		Blows o	n Spoor	,]	REC									
	(ft)	METHOD	No.	FROM	то						SOIL DESCRIPTION AND STRATIFICATION	SYMBOL							
	0	~~~		(ft)	(ft)	0/6		12/18	18/24	(in)									
		SS	<u>S-1</u>	0	2	6	16	8	15	15	FILL: Gray fine SAND, some Silt, trace Gravel (11-65)								
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	5		1								4								
		SS	S-2	5	• 7	10	12	15	15	20	FILL: Brown fine SAND, some Silt, trace Gravel								
											(11-65)								
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		SS	S-3	10	12	12	14	15	17	20	FILL: Brown fine SAND, some Silt, trace Gravel								
					ļ			ļ		L	(11-65)								
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	15		<u> </u>		┣───														
		SS	S-4	15	17	50	26	37	51	15	Olive brown coarse to fine SAND, trace Gravel, trace Silt								
					<u> </u>						(7-65)	*******							
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لسرر	_20				ļ					ļ		ulliki: famou ara-ara							
Sec. Company) I	SS	S5	20	22	38	100/5"			<u> </u>	Brown fine SAND, some Silt, trace Gravel with Rock								
4,004	Í							 -		<u> </u>	(7-65)	9 2 446.0							
										<u> </u>	Wasthand Book	1474-1. H.L.T. HILF							
	25		· .				· •			<u> </u>	Weathered Rock (4-65)								
		SS	S-6	25	27	50/0"					Rock (3-65)	a filia da katala da se ta se se se se se se se se se se se se se							
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											Hollow stem auger refusal on Rock @ 26.5'								
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	30							ļ		ļ	Boring Complete @ 26.5'	111207000000000000000000000000000000000							
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		al I.D. of	**********	Den st			14 C				hereon was obtained for the design and estimating purposes for our client.	•							
			Split Barre		······································	1					users only that they may have access to the same information available								
{	-Carrielanin		-lammer or -lammer or				to our client. It is presented in good faith, but it is not intended as a substitute for investigations, interpretations or judgment of such authorized users. Information on the logs should not be relied upon without the geotechnical												
The second	-		r on Drive			1	or judgment of such authorized users. Information on the logs should not be relied upon without the geotechnical engineers recommendations contained in the report from which these logs were extracted.												
	Core S					in		Pp: Pocket Penetrometer; WOH: Weight of Hammer; WOR: Weight of Rod											
			1			-ft	-				Inferred Change in Strata:								

Soil descriptions represent a field identification after D. M. Burmister unless otherwise noted.

	M	7.7. 5				PR	PROJECT NAME: I			and the second se		BORING NO.	SB-	5
			on sult	N G			LOC	ATION:	Staten	Island	, NY	JOB NO.	731	7
		CHOICE -	INCINE								1	- Particular	3.0' :	±
J	COLUMN STREET,		eneral Bori	ings		And the second se		ARTED:	Ser. Commenter	2008		NDWATER TABLE DEPTH: 28		
		CTOR: G	P			DATE	COMP	LETED:	3/10/	2008	O Hr. 28' Date	3/10/08 24 Hr. N/A Date	N/A	
1	DEPTH		SAMPLE	DEF			Blows o	n Spoor	n	REC				
	(ft) 0	METHOD	No.	FROM	TO	0/0	0/10	4040	10/04	(1)	SOIL DESCRI	PTION AND STRATIFICATION		SYMBOL
		· 00		(ft)	(ft)	0/6		12/18	18/24	(in)		ـــــــــــــــــــــــــــــــــــــ		
		SS	S-1	0			7	16	21	10	TOP SOIL (4")	SAND, some Silt, trace Gravel with	-	
CHARACTER CONTRACTOR				and a second second second second second second second second second second second second second second second		-				7 _{1 1} بر با السام المسام (1	Brick pieces	SAIND, Some Sin, uace Graver with		
				[(11-65)			
	5													
		SS	S-2	5	7	10	11	14	15	18	Gray CLAY	(9-65)		
and the second se		00	0.2		<u> </u>	- 10				10	Brown fine SAND, son		-	
one-could have				<u> </u>			<u> </u>				(7-65)		t	
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		SS	S-3	10	12	5	8	26	30	18	Red brown fine SAND,	and Silt, trace Gravel with Boulders	T	
											(7-65)		Ī	
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							And the second s							
	15						100000		[
		SS	S-4	15	17	10	25	39	38	15	Red brown fine SAND,	some Silt, trace of Gravel (7-65)		
				[Į				Ļ	ļ				
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-	20			<u> </u>				<u> </u>	<u> </u>		-			
	2	SS	<u>S-5</u>	20	22	75	45	30	51	20	Red brown fine SAND,	, trace Gravel, trace Silt with fracture	d	
				Ļ		L			<u> </u>	ļ	rock			
					ļ			<u> </u>	<u></u>	<u> </u>	_(7-65)		-	
	25				<u> </u>				┢		-			
	20	SS	S-6	25	27	98	100		<u> </u>	 	Weathered Rock			
			3-0		2/	20	100	<u> </u>	┢────		(4-65)			
				<u>}</u>			<u> </u>	1	<u> </u>				ŀ	
				┢╼╼╼╸				<u> </u>	<u> </u>	<u> </u>	n:		- Jana	
	30				†			┼───	<u> </u>	<u></u>			-	100 for the second second second second second second second second second second second second second second s
		SS	S-7	30	32	80/3"				<u> </u>	- Weathered Rock			
				1	İ		(j.	<u> </u>		-[(4-65)			
			RUN-1	32	37	3	min	[REC = 100%; RQD = 50%	1	-RAWERS / real land / lowerbur
						7	min				Serpentinite, light gree	n, massive, strong, hard, medium		
	35					8	min					ered, moderately fractured, coated ro	1gh	
				L		7	min				joints		-	
					1	6	min](3-65)		a generation of the	
			RUN-2	37	42	7	min		<u> </u>	ļ	Core Run-2, 37' - 42';	REC = 100%; RQD = 68.3%	terre and	
				Į	-	5	min	<u> </u>	<u> </u>	ļ		n, massive, strong, hard, medium	ļ	Stort Climate and an and
	40			L		7	min		<u> </u>	<u> </u>	grained, slightly weath	ered, moderately fractured		
			C##			1	3							
	A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR	al I.D. of I			,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		1					e design and estimating purposes for our o		-
	10 to 10 to	A - 0100 10-00	Split Barrel			2	1					e access to the same information available		
1	the second second		lammer or			1	1			-		ed as a substitute for investigations, interpr		
and the second second	a' international and a second		lammer or		arrel	1	1					s should not be relied upon without the get	otech	nical
	Suppress of the second	10441	r on Drive	Pipe	· · · · · · · · · · · · · · · · · · ·		1					ch these logs were extracted.		
	Core S	SIZO				l in	8 .				/OH: Weight of Hammer; W	-		
	0.41.3			Cald 11								ange in Strata:		
	Soll de	scriptions	represent a	mend iden	uncation	atter D.	M. Burn	nister uni	less other	wise not	ea.	-		

FIGURE 7

H	7 _ s				۲۱			Liberty			·		BORING NO.	SB-5	
		ONSULT	havad ^{ar} ∰ 'tNG			LOC	CATION:	Staten	Island				JOB NO.	7317	
<i>160</i> ,		ENGINES	ខេត អ		<u></u>								GROUND ELEVATION:	46.0' :	±
		eneral Bori	ings		¢	START	and the second second second second second second second second second second second second second second second		2008	<u> </u>				28'	RIWALSHIP
STOLEN BURGE	CTOR: C	<u>аР</u>			DATE	COMPL	ETED	3/10/	2008	0 Hr.	28'	Date	3/10/08 24 Hr. N/A	Date N/A	
∍́ЕРТН (ft)	METHOD	SAMPLE No.	DEF FROM	тн то		Blows o	n Spoor	۱	REC		SOIL	DESCRI	PTION AND STRATIFICATION	s	SYMB [®]
40	ļ	ļ	(ft)	(ft)	0/6	1	12/18	18/24	(іл)	ļ		******			
		Run-2	37	42	5	min	<u> </u>						n, massive, strong, hard, mediu		
	·				7	min	<u> </u>			grained	1, slighti	y weath	ered, moderately fractured (3	-05)	
		<u> </u>										Bo	ring Complete @ 42'		
45				_	<u> </u>	<u> </u>	<u> </u>						0	1	
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Nominal I.D. of Split Barrel Sampler 1% in It is made available to authorized users only that they may have access to the same information available Weight/type of Hammer on Drive Pipe 300 lb to our client. It is presented in good faith, but it is not intended as a substitute for investigations, interpretations eight/type of Hammer on Split Barrel 140 lb or judgment of such authorized users. Information on the logs should not be relied upon without the geotechnical Drop of Hammer on Drive Pipe in engineers recommendations contained in the report from which these logs were extracted. Core Size in

Pp: Pocket Penetrometer; WOH: Weight of Hammer; WOR: Weight of Rod

Inferred Change in Strata: Approximate Change in Strata: _

Soil descriptions represent a field identification after D. M. Burmister unless otherwise noted.

FIGURE 7b

Control of the local division of the local d	Æ	7.Z C				PF		Contraction of the second second	Liberty		the second second second second second second second second second second second second second second second se	BORING NO.		<u>B-6</u>
	66	<u> </u>	onsult	N G	·		LOC	ATION:	Staten	Island	, NY	JOB NO.	7	317
			INGINE									GROUND ELEVATION:	50).0' ±
	BORIN	GBY: G	eneral Bori	ngs		DA	ATE ST/	ARTED:	3/11/	2008	GROUN	NDWATER TABLE DEPTH :	NE	
ĺ	SPE	CTOR: G	ìP		·	DATE	COMP	LETED:	3/11/	2008	0 Hr. NE Date	N/A 24 Hr. N/A	Date N	Λ I
1	EPTH		O ANDI E	DEF	тн			n Spoor		REC				
	(ft)	METHOD	SAMPLE No.	FROM	то			in opoor	1	nec.	SOIL DESCRI	PTION AND STRATIFICATIO	N	SYMBOL
5775-FURD	0		110.	(ft)	(ft)	0/6	6/12	12/18	18/24	(in)	g			
	2.N2	SS	S-1	0	2	1	6	7	8	20	6" Topsoil		NOVITA-ILLING	-
						774						D, some Silt, trace Gravel		
							·····				(11-65)			
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ord Alexandra	5													
		SS	S-2	5	7	8	8	12	15		EII I · Drown fing SAN	D, little Silt, trace Gravel		
		- 00	5-2		<u> </u>	<u> </u>	0	12	51	24	(11-65)	(D, male Shi, date Chavel		
						*****					(11-05)			-
								<u> </u>			-			-
- Contraction	40		ļ								-			
Constraints	10	~~				<u> </u>	<u> </u>	<u> </u>	 				-	
anna ann ann ann ann ann ann ann ann an		SS	S-3	10	12	. 9	24	21	36	24	Brown fine SAND, son	ne Silt, little Gravel		
NOWICK			l	Ļ		ļ	<u> </u>	<u> </u>	<u> </u>	<u> </u>	(7-65)			Curtorbanumierorowa
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		SS	<u>S-4</u>	15	17	23	50/1"	<u> </u>	<u> </u>	1				
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J	20			L				<u> </u>	<u> </u>	<u> </u>				
- marter	2	SS	S-5	20	22	34	34	38	53	10	Gray fine SAND, some	e Silt, little Gravel		
-4/64	and the second se							<u> </u>			(7-65)			
			<u> </u>]			<u> </u>		weathered rock			
					ļ			<u>l</u>	ļ.,		(4-65)			
	25			L					<u>[</u>					
		SS	S-6	25	27	50	50/0"		<u> </u>		Rock		(3-65)	
									L					- †
											Split spor	on refusal on Rock @ 25.5'		
				<u> </u>					[
	30										Bor	ing Complete @ 25.5'	_	
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	Nomin	al I.D. of	Hole			l in	The sut	osurface i	nformatio	on show	n hereon was obtained for th	he design and estimating purpose	s for our clie	ent.
	6.14h	C-7844401-8144	Split Barrel	Sample	F	-g	-7					ve access to the same information		
			lammer or			1						ed as a substitute for investigation		ations
Ś		oreal and a second second second second second second second second second second second second second second s	lammer or		10.0	· · · · · · · · · · · · · · · · · · ·	-					s should not be relied upon witho	-	
No. of	and the second second second second second second second second second second second second second second second		r on Drive			1	74					ch these logs were extracted.	8000	
	Core S			1. .		in	1				OH: Weight of Hammer; W	=		
I												ange in Strata:		
	Soil de	scriptions	represent a t	field iden	tification	after D.								

	T	726				PF	The second second second second second second second second second second second second second second second s	'NAME:		NAME OF TAXABLE PARTY.		BORING NO.	<u>SB-7</u>	
		W) 🐂					LOC	ATION:	Staten	Island	, NY	JOB NO.	7317	7
			ONSULT INGINEI									GROUND ELEVATION: 5	9.0' ±	
	BORIN	G BY: G	eneral Bori	ngs		D/	ATE ST	ARTED:	3/11/	2008	GROU	NDWATER TABLE DEPTH: NE		
(ISPE	CTOR: G	P		·	DATE	COMP	LETED:	3/12/	2008	0 Hr. NE Date	24 Hr. N/A Date	N/A	
·	ານ໌EPTH			ĎEF	тн					DEO				
	(ft)	METHOD	SAMPLE No.	FROM	то		Blows o	n Spoor	1	REC	SOIL DESCRI	PTION AND STRATIFICATION	s	YM8OL
	0		110.	(ft)	(ft)	0/6	6/12	12/18	18/24	(in)				Table
	1)	SS	S-1	0	2	3	5	6	9	16	6" Topsoil	, ₂₀₁₀ , and a second se	T	
								1			af "	SAND and Silt, little Gravel		
		CHARLES FROM THE DESCRIPTION OF THE						<u> </u>			(11-65)		at the take	
											1			
	5]						
and a state of the		SS	S-2	5	7	13	8	7	21	-14	FILL: Gray coarse to fi	ine SAND, some Silt, little Gravel		*******
Internet					<u></u>			ĺ			with Wood		5000	
								<u> </u>			(11-65)			
			·			*	<u> </u>	<u> </u>		<u> </u>	1		-	
	10									ļ				
, in the second s		SS	S-3	10	12	10	10	10	10	10	Red brown fine SAND	, some Silt, trace of Gravel		
											(7-65)			
								1	<u> </u>		•			
				<u> </u>			<u> </u>	1	<u> </u>		-			
	15			İ				1	1					
		SS	S-4	15	17	35	44	50	28	5				
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	20		6				(101100)							***
		SS	S+5	· 20	22	64	69	44	42	10	Red brown medium to	fine SAND, little Gravel, little Silt		
~~~~			Ì		1		<u> </u>		1		with Cobbles			
					· · · · · · · · · · · · · · · · · · ·	1940-4012-000			1	1	(7-65)			
	****							1					Ĺ	
	25						<u> </u>							
		SS	S-6	25	25.6	85	50/1			2				
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	1000	SS	S-7	30	30.5	77	95			0	No Recovery			
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	Concentration	Ļ	ļ			<u> </u>	<u></u>	Ļ						20000000000000000000000000000000000000
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	35						<u> </u>					,		
		SS	S-8	35	35.3	50/3				3		o fine SAND, little Gravel, trace Silt		
				<u> </u>							with Rock		-100	20207-02-0011-0-0-07
				Ļ		<u> </u>					(7-65)			
	1111100					ļ			L	<u> </u>		<u></u>		The second second second second second second second second second second second second second second second s
	40		Run - 1	38.5	43.5	L					Core Run-1, 38.5' - 4	3.5'; REC = 87%; RQD = 50%	Como Como	
						~~~~								
	Nomin	al I.D. of	Hole			ir	The sul	bsurface i	nformati	on show:	n hereon was obtained for the	he design and estimating purposes for our	client.	
	Nomin	al I.D. of	Split Barre	Sample	er	1% ir	It is ma	de availa	ble to aut	horized	users only that they may ha	ve access to the same information available	>	
/	Weigh	t/type of H	lammer or	n Drive F	Pipe	300 lk	to our o	lient. It	is present	ied in go	od faith, but it is not intende	ed as a substitute for investigations, interp	etation	18
a la character a la	√eigh	nt/type of H	lammer or	n Split Ba	arrel	140 lk	or judg	ment of s	uch auth	orized us	sers. Information on the log	s should not be relied upon without the ge	otechn	ical
	Drop o	of Hamme	r on Drive	Pipe		ir	engine	ers recom	mendatio	ons conta	ained in the report from whi	ch these logs were extracted.		
	Core S	Size				ir) F	p: Pocke	t Penetro	meter; W	VOH: Weight of Hammer; V	VOR: Weight of Rod		
							Approx	cimate Cł	ange in S	Strata: _	Inferred Ch	ange in Strata:		
	Soil de	scriptions	represent a	field iden	tification	after D.	M. Buri	mister un	less other	wise not	ted.			

(1)		S llama (5					Liberty Staten			<u>SB-</u> 731
		ONSULT	1 N G			LUL	ATION:	Juaten	ารเสทน		73 59.0
		eneral Bori				START		0/14	/2008		59.0
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J <u>OF L</u> VEPTH			DEF	тн		CONFL	EICU	0/12/	2000	Date 3/10/08 24111. IVA Date	
(ft)	METHOD	SAMPLE No.	FROM	то		Blows c			REC	SOIL DESCRIPTION AND STRATIFICATION	
40			(ft)	(ft)	0/6	6/12	12/18	18/24	(in)		_
					4	min	L			Serpentinite, light green, massive, very strong, hard, mediun	.
			L		6	min	ļ	ļ	ļ	to fine grained, slightly weathered, moderately fractured	
	*****		<u> </u>		6	min	<u> </u>			-(3-65)	
4.5		Run-2	43.5	48.5	4	min	<u> </u>				lumber of sole
45		ļ	<u> </u>		6	min				Core Run-2, 43.5' - 48.5'; REC = 98%; RQD = 48.3%	_
					9	min	<u> </u>	<u> </u>		Serpentinite, light green, massive, very strong, hard, medium	
			<u> </u>	ļ	4	min			<u> </u>	to fine grained, slightly weathered, moderately fractured (3-65)	
					7	min	<u> </u>				
50						<u> </u>				Poring Complete @ 48 5 FEET	
50				ļ		<u> </u>				Boring Complete @ 48.5 FEET	_
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Nomin	al I.D. of	Hole		////	;.	The	nourfood	informati	on chose	n hereon was obtained for the design and estimating purposes for our	110-
		Split Barre	Sample	>r		-				users only that they may have access to the same information available	
		Jammer or								bod faith, but it is not intended as a substitute for investigations, interpr	
		Hammer or						-		sers. Information on the logs should not be relied upon without the ge	
- Alter		r on Drive		41101						ained in the report from which these logs were extracted.	
Core					i					VOH: Weight of Hammer; WOR: Weight of Rod	
										Inferred Change in Strata:	

FIGURE 9b

	177	77 C				PF			IE: Liberty Towers			BORING NO. SB-8		-8	
and by the second			N Lange St				LOC	ATION:	Staten	island,	NY	JOB NO. 7317			
			ONSULT NGINES	ING RS								GROUND ELEVATION: 70.0' ±			
	BORIN	IG BY: G	eneral Bori	ngs		D	ATE ST/	ARTED:	3/12/	2008	i	NDWATER TABLE DEPTH: NE			
	7000	CTOR: G		- Сторини и с	and the second second		COMP		3/12/		0hr NE Date	24 Hr. N/A Date	N/A		
	DEPTH		T. T. Market	DEP	Ϋ́́ΤΗ		***************************************						I		
	(ft)	METHOD	SAMPLE	FROM	то		Blows o	n Spoor	L I	REC	SOIL DESCRI	PTION AND STRATIFICATION		SYMBOL	
	0		No.	(ft)	(ft)	0/6	6/12	12/18	18/24	(in)			urrupher.		
			· · ·		<u>`</u>						6" Topsoil	010 <u>0.1 </u>			
						<u> </u>					4 ~	dium to fine SAND, some Silt, with	reformen		
											Wood, Brick		undinnassa		
											(11-65)		-		
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Pp: Pocket Penetrometer; WOH: Weight of Hammer; WOR: Weight of Rod

Approximate Change in Strata: ____ Inferred Change in Strata:

Soil descriptions represent a field identification after D. M. Burmister unless otherwise noted.

Core Size

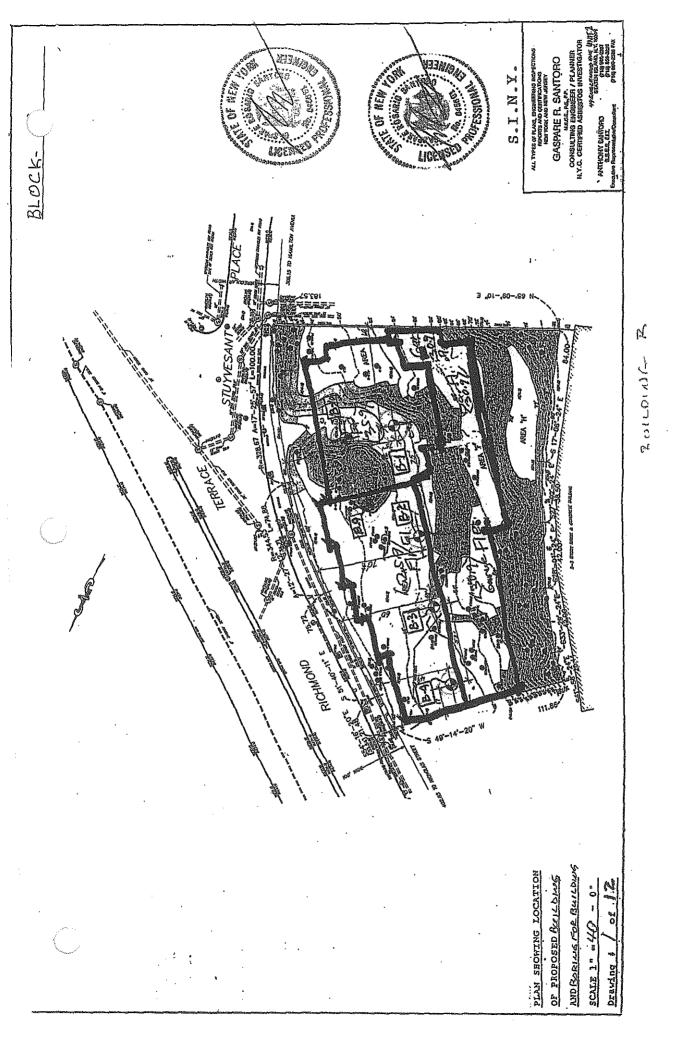
FIGURE 10b

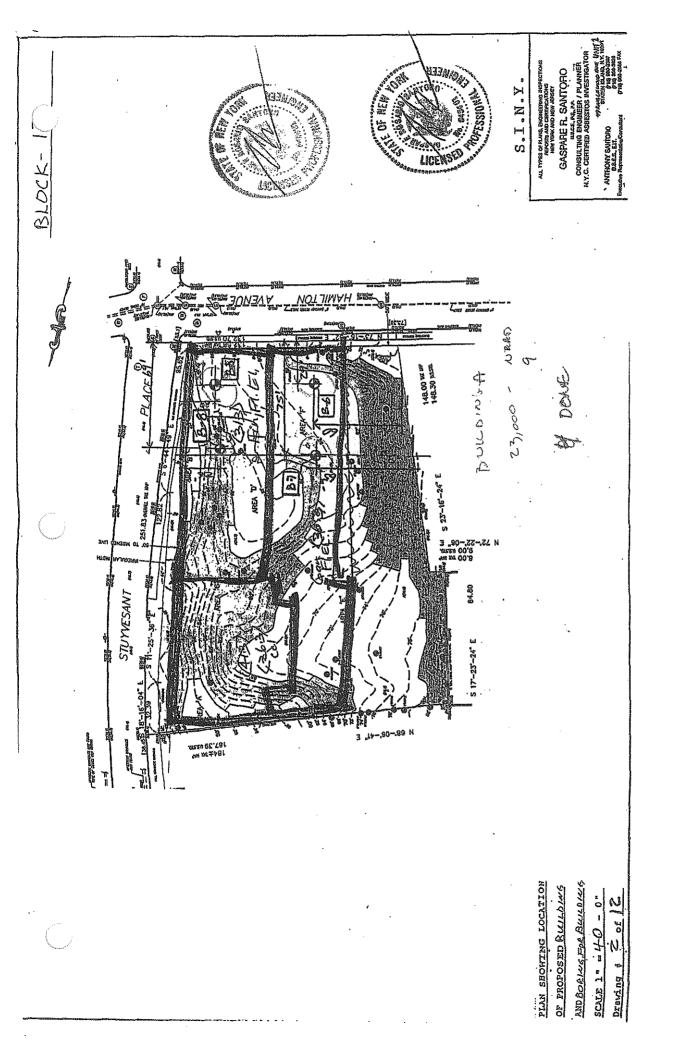
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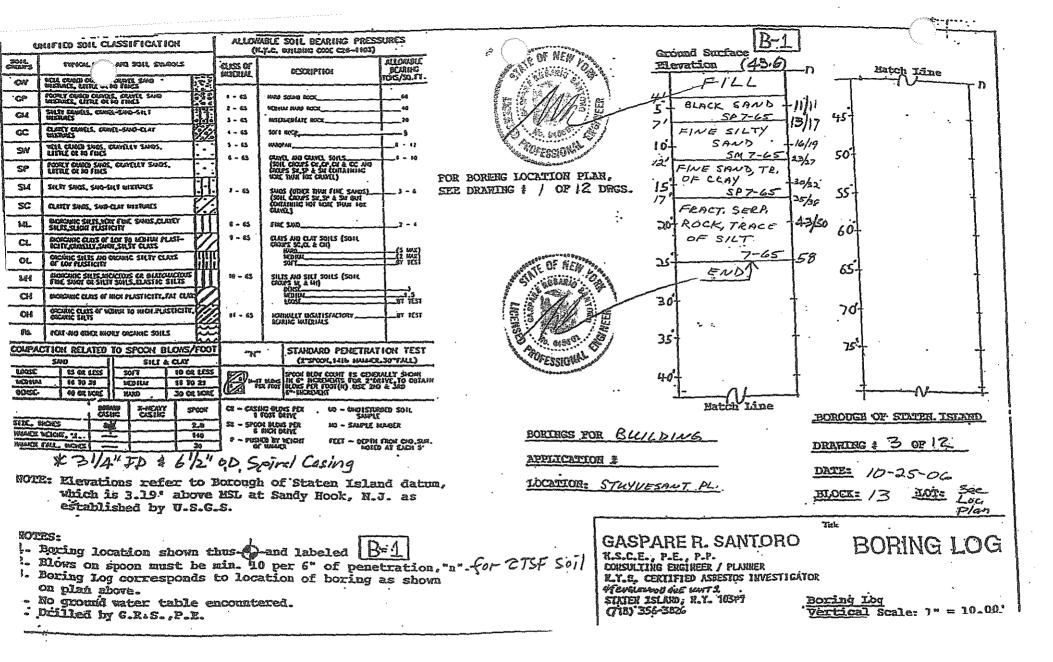
FIGURE 11

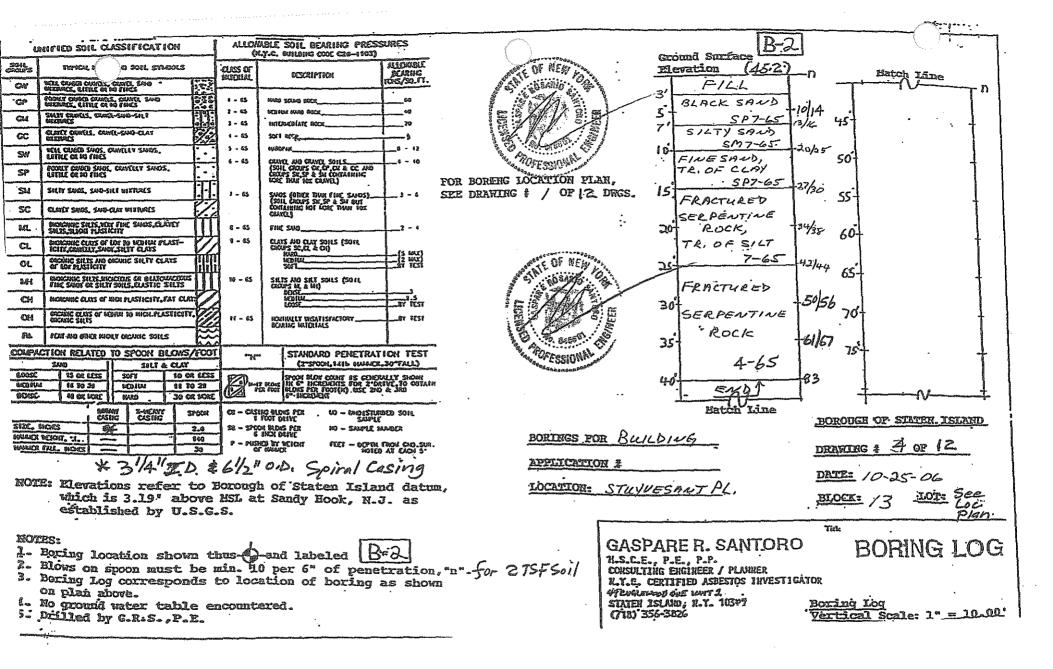
APPENDIX B

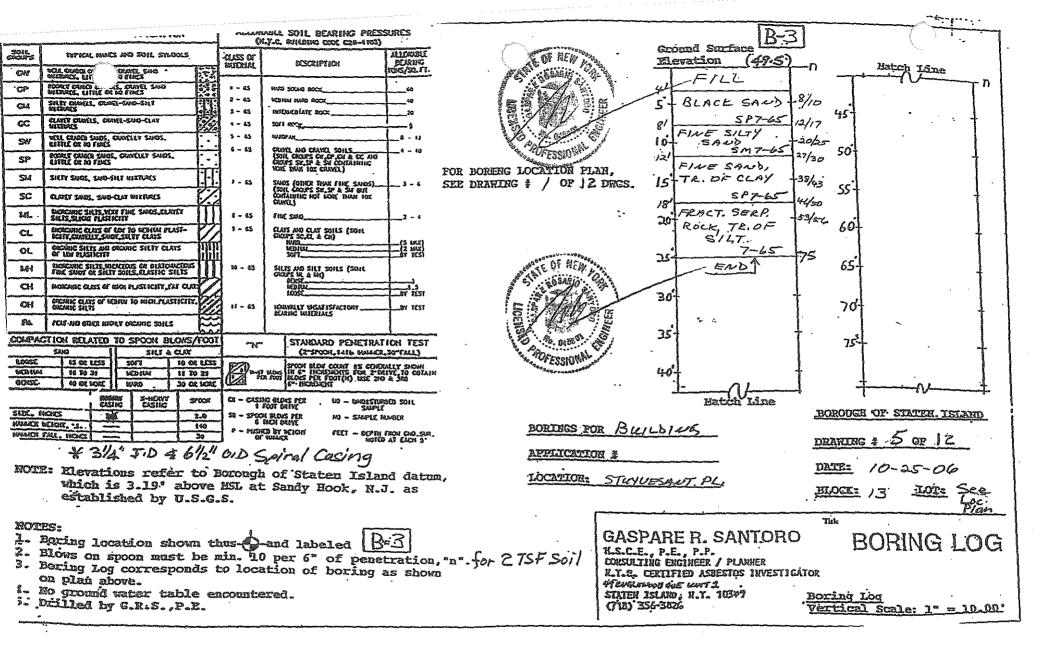
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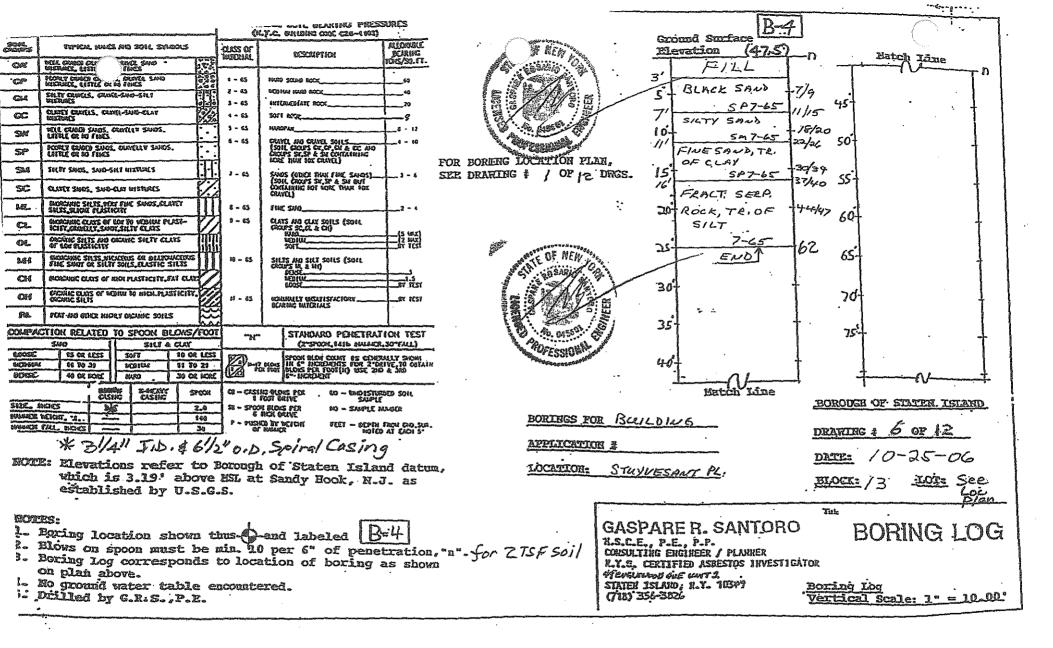


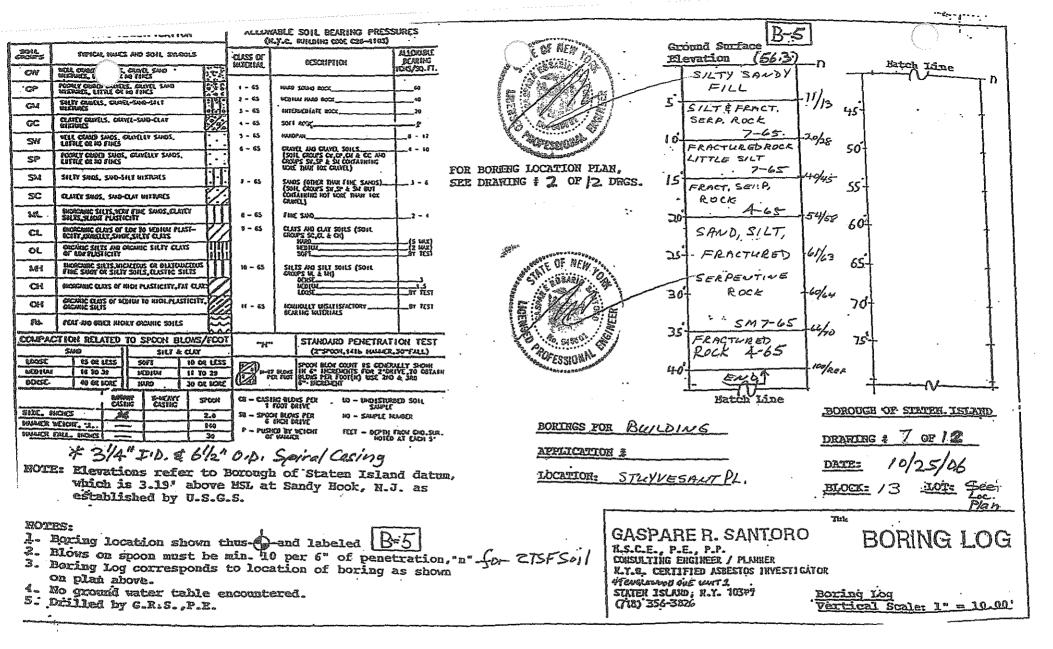


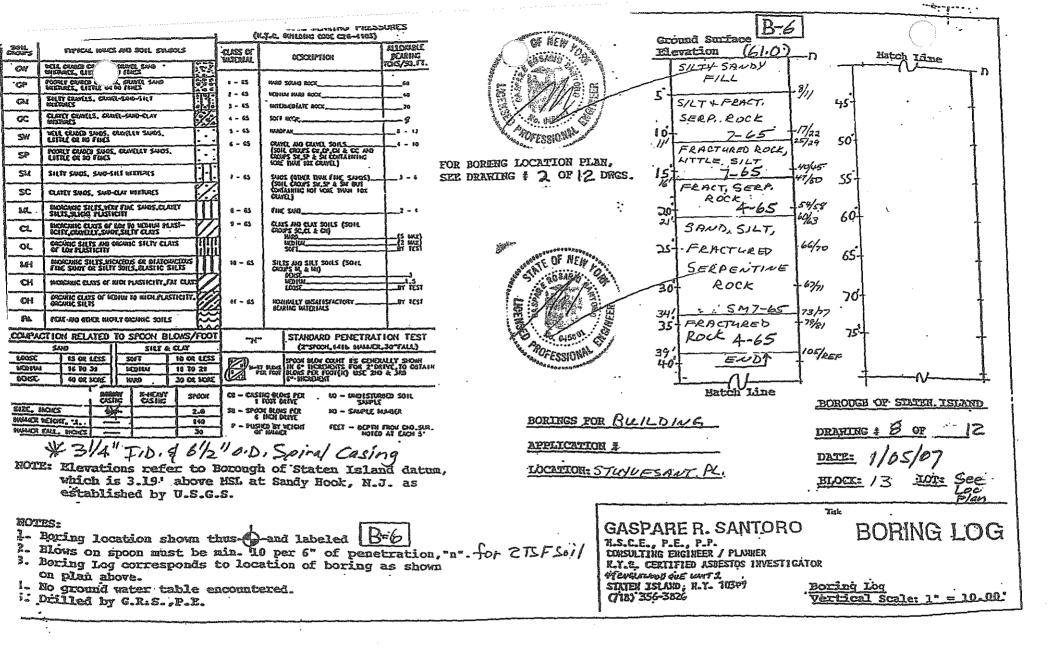


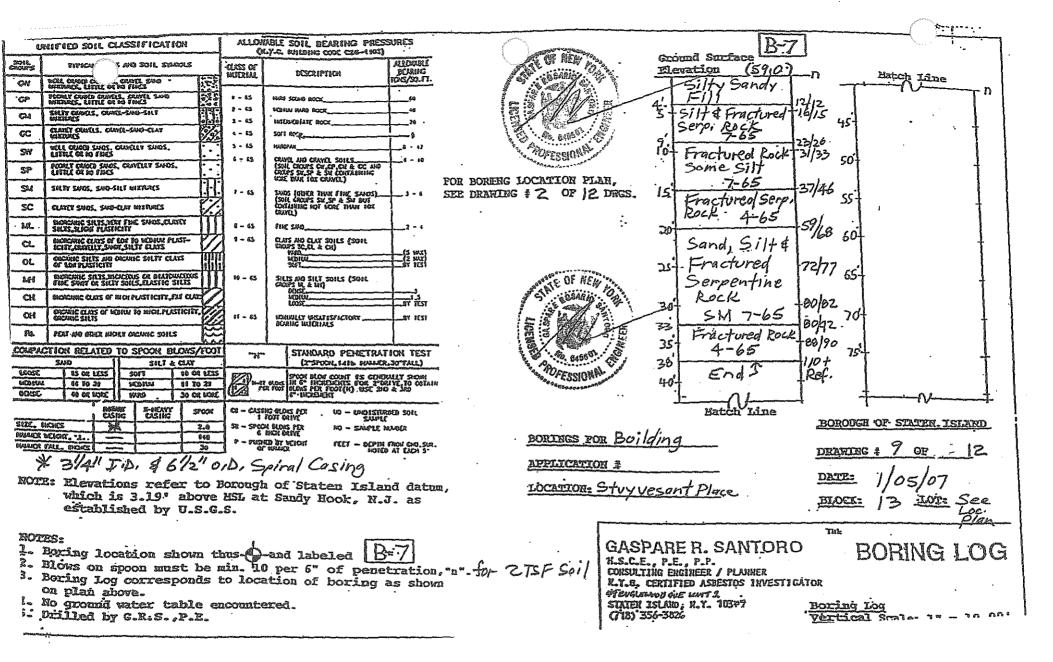


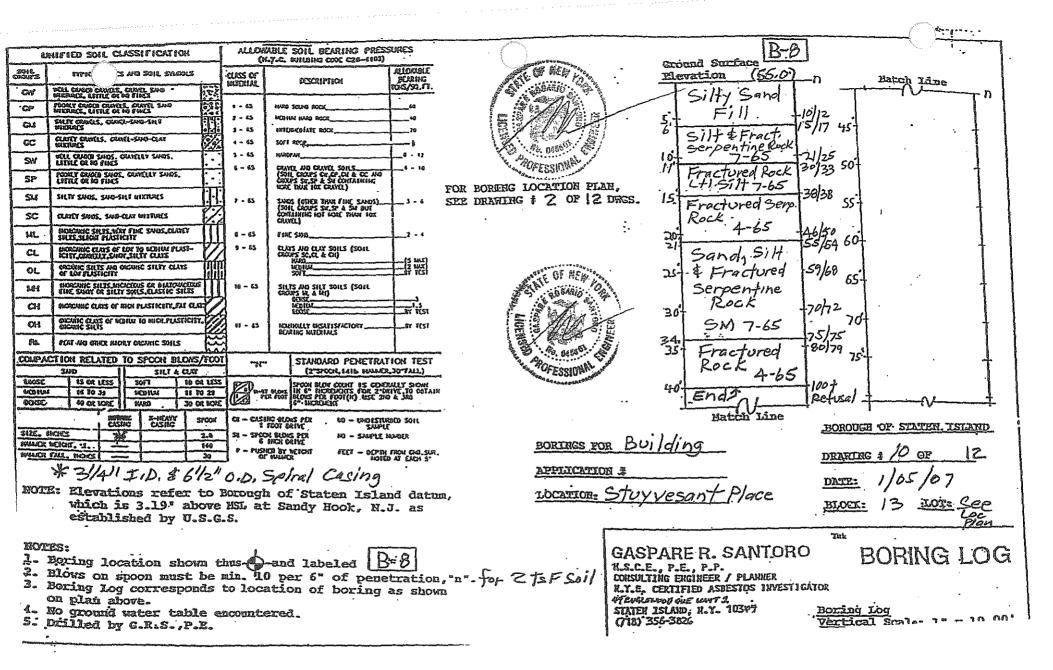


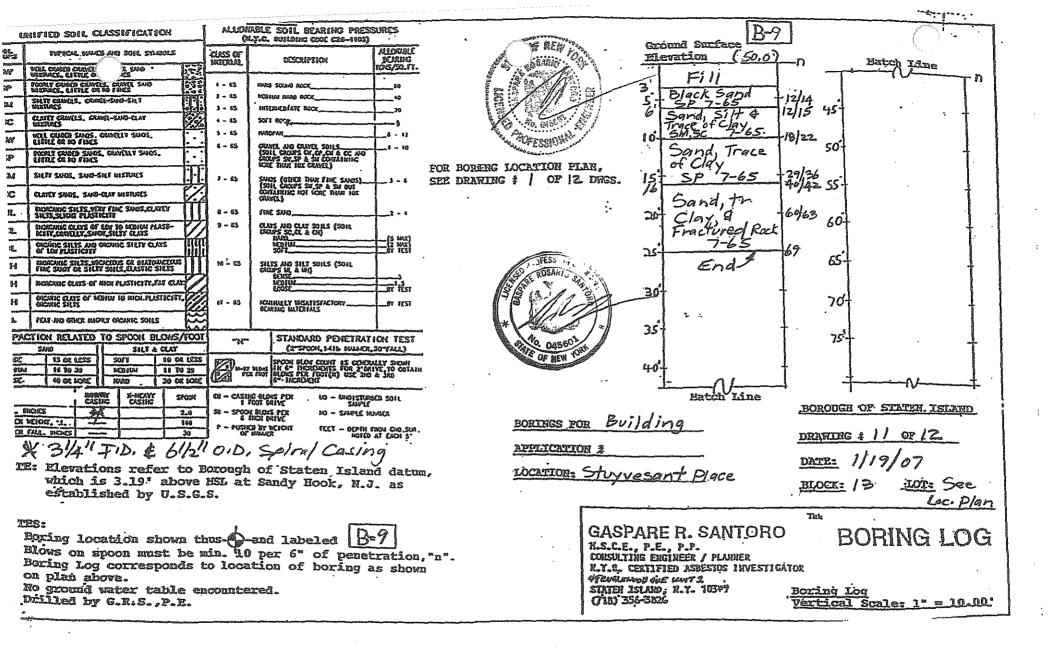












APPENDIX C

С ()



Porcello Engineering, Inc.

PO Box 728, Pine Brook, New Jersey 07058

Phone: (973) 882-8377 Fax: (973) 882-8478

UNCONFINED COMPRESSION TEST OF ROCK CORE SAMPLE

CLIENT: SESI Consulting Engineers 12A Maple Avenue Pine Brook, NJ 07058-9742 DATE:

3/13/2008

PROJECT: Liberty Towers Staten Island, N.Y.

LOCATION of PLACEMENT:

Test #1a, SB-2, R-2 30-35 (2"x4") Test #2a, SB-5, R-1 385 -435 (2"x4")

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Cylinder ID	Condition of Sample	Cylinder Size (in. x in.)	Area of Cylinder (sq. in.)	Total Load (Ibs.)	Compressive Strength (psi)
1a 1b	good good	2" x 4" 2" x 4"	3.14 3.14	17,500 18,100	5,580 - 5,770