

# Surface Water Interim Remedial Measure Engineering Report

Chicago Pneumatic Tool Company Frankfort, New York

October 1994

BLASLAND, BOUCK & LEE, INC. ENGINEERS & SCIENTISTS

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surface water at the Site. The first investigation was initiated in 1985 by Recra Research, Inc., under contract to the NYSDEC, to complete a Phase I Investigation and to propose a Phase II Work Plan for the Chicago Pneumatic Site. The Phase I Investigation identified surface and subsurface issues at the Site; however, no air, water, or soil samples were obtained.

In 1986, the United States Environmental Protection Agency (USEPA) contracted NUS Corporation (NUS) to prepare a Potential Hazardous Waste Site Inspection Report. Seven surface water, ten sediment, and two soil samples were obtained by NUS as part of their investigation. NUS's report identified four potential areas of concern (AOCs): the debris landfill area; the three former oil separation ponds; the drainage ditches; and the chip chute area.

In January 1988, BB&L was contracted to conduct an Environmental Assessment to further characterize the constituents identified at the Chicago Pneumatic Site during the 1986 USEPA investigation. The Environmental Assessment activities included conducting an aerial photograph review, a magnetometer survey, the installation of monitoring wells and surface water, ground-water, soil and sediment sampling. The Environmental Assessment was conducted in several phases between 1988 and 1991. The scope of work and results of the activities were detailed in the following two reports prepared by BB&L and submitted to the NYSDEC: "Summary of Site Activities and Quality Assurance Project Plan (QAPP)", dated June 1990, and "Site Investigation Report", dated July 1990.

Based on the results of information collected during these previous site investigations, a Consent Order was issued in July 1993. Among the work activities covered by the Consent Order was preparation of an RI/FS Work Plan. Based on review of data generated during the Environmental Assessment and the scoping efforts, the following five AOCs were investigated during the RI:

- 1. The former debris landfill area;
- 2. The former separation ponds (including the east lot);
- 3. The former chip chute area and drainage ditches;



- 4. The foundry and beneath the west parking lot; and
- 5. The clay drainage pipe and off-site drainage ditch.

A conceptual site model was developed in the RI/FS Work Plan (BB&L, 1993) and included identification of existing data gaps associated with characterization of the AOCs, assessment of background conditions, a hydrogeologic characterization to address non-site related constituents, and an assessment of ground-water and surface water (i.e., drainage ditches) migration pathways. A Risk Assessment addressed exposure pathways and receptors associated with the drainage ditches. RI activities were conducted between November 1993 and April 1994 and a RI Report was issued in July 1994.

One of the recommendations of the RI Report was to complete an IRM to address VOCs discharging from a clay pipe to a surface water ditch along Bleecker Street and the oil skimmer pond overflow to SPDES Outfall 003. This surface water IRM Engineering Report addresses this recommendation of the RI Report.

### 3.0 - Existing Site Data



#### 3.1 General

This section includes a discussion of the information and data that were used to develop the basis of design of the surface water IRM. This information included discharge monitoring data for Outfall 003, sampling results from the RI, and data from the four streams that contribute flow to Outfall 003. As shown on Figure 3, the surface water drainage ditches at the Site include the southern drainage ditch, the chip chute drainage ditch, the eastern drainage ditch, and the drainage ditch parallel to Bleecker Street. Both the southern drainage ditch (which receives drainage from the debris landfill area and the former separation ponds), and the chip chute drainage ditch discharge to the oil skimmer pond. The oil skimmer pond overflow discharges through Outfall 003, which in turn, discharges to the eastern drainage ditch. The eastern drainage ditch converges into the Bleecker Street drainage ditch. The clay pipe discharges to Bleecker Street drainage ditch downstream of the convergence with the eastern drainage ditch.

#### 3.2 Discharge Monitoring Data - Outfall 003

Discharge monitoring data collected by Chicago Pneumatics from Outfall 003 was evaluated between the period of January 1993 through June 1994. This monitoring data included bi-monthly flow measurements and analytical results for those parameters required by the existing SPDES permit. The following VOCs of concern were sampled and analyzed as part of these monitoring requirements:

- Trichloroethehe;
- cis-1,2-Dichloroethene;
- trans-1,2-Dickloroethene; and
- Vinyl chloride.



A summary of flows and concentrations recorded at Outfall 003 for the period evaluated is provided in Table 1. The average flow during the period evaluated was approximately 23 gallons per minute (gpm). The six highest recorded flow events for this period were 37 gpm in April 1994, 42 gpm in March 1994, 55 gpm in May 1993, 60 gpm in May 1994, 100 gpm in April 1993, and 300 gpm in November 1993. However, a total of 30 out of 36 flows were below 20 gpm, and six flows were less than 1 gpm.

In evaluating this data, several observations were made. Trichloroethene and cis-1,2-Dichloroethene were present in the highest concentrations in comparison to the other parameters with detected at concentrations of 1.1 and 2.2 milligrams per liter (mg/l), respectively. The highest concentrations of VOCs at Outfall 003 occurred during colder months while the lowest concentrations of VOCs occur during warmer months. There was no relationship observed between flow and concentration of VOCs. Higher flows (i.e., greater than 20 gpm) at Outfall 003 did not occur simultaneously with peak concentrations of VOCs. While high flows tended to occur during the months of March through May due to spring run-off, highest concentrations of VOCs tended to occur during the colder months of November through March. The highest flow of 300 gpm, which occurred during November 1993, is thought to be due to a wet weather sampling event.

#### 3.3 Remedial Investigation Sampling Results

RI activities included sampling and chemical characterization of surface water. VOCs were detected in the surface water samples obtained from the southern drainage ditch; the chip chute drainage ditch; the eastern drainage ditch; and the clay pipe discharge. A summary of these results is provided below:

			Conce	ntration (mg/l)
Loca	tion	Flow Rate (gpm)	Trichloroethene	Total 1,2-Dichloroethene
Southern Drainag	e Ditch	Stagnant	< 0.005	0.037
Chip Chute Drain	age Ditch	Stagnant	5.1	2.2
Eastern Drainage	Ditch	7	0.027	0.013



Loca	tion	Flow Rate (gpm)		ntration (mg/l)  Total 1,2-Dichloroethene
Clay Pipe Discha	rge	2	7.6	0.5

#### 3.4 Streams that Contribute Flow to Outfall 003

Four streams contribute flow to Outfall 003, including:

- Oil skimmer pond overflow;
- Manufacturing building roof leaders;
- Building fibor drains from warehouse to east of manufacturing building; and
- Exterior warehouse loading dock trench drain.

On April 1 and April 8, 1994, Chicago Pneumatic measured flow and sampled these four streams that contribute flow to Outfall 003. The results of these activities are provided on Table 2. As can be seen by the results, the oil skimmer pond overflow was the only source of VOCs to Outfall 003. Trichloroethene and cis-1,2-Dichloroethene were present in the highest concentrations on the April 8, 1994 sampling event at 0.12 and 0.065 mg/l, respectively. During the April 1 and April 8, 1994 sampling events, the flow contribution of the oil skimmer pond overflow relative to other streams that contributed flow to Outfall 003 was 12 percent and 16 percent, respectively.

Since the warehouse at the Chicago Pneumatic facility is relatively new (constructed in the 1970s) and no known sources of VOCs have been found at that location, there is no reason to expect the presence of such compounds in either the floor drains or exterior dock drain as was demonstrated by the April 1994 sampling events. The discharge main connecting the building roof leaders runs directly under the southeast side of the facility where ground water and geoprobe samples have detected concentrations of VOCs in the soil and ground water. However, based upon BB&L's inspection of Chicago Pneumatic manufacturing building plumbing and facility drawings, the roof leader discharge main is buried above the ground water level.



Infiltration of ground water containing VOCs into the discharge main would therefore not be expected as was demonstrated by the April 1994 sampling events.

In order to better understand the sources of flow contributing to Outfall 003 during wet-weather conditions, the Rational Method was employed. The following assumptions were made in applying the Rational Method:

- Drainage area for the oil skimmer pond (which includes the drainage ditches) is approximately 60,000 square feet (assumes drainage ditches collect runoff from an area 50 feet wide);
- Drainage area for the roof drains is approximately 90,000 square feet (200 feet by 450 feet area of the roof);
- Run-off coefficient for the oil skimmer pond drainage area is 0.15 (generally unpaved area);
- Run-off coefficient for the roof drain drainage area is 0.85 (all impervious surfaces); and
- Run-off from warehouse floor drains and loading dock trench drains are insignificant.

Given these assumptions, the total flow to Outfall 003 during wet-weather conditions was calculated to be 89 percent run-off from the roof drains drainage area and 11 percent run-off from the oil skimmer pond drainage area.

# 4.0 - Interim Remedial Measure Basis of Design



#### 4.1 General

The basis of design for the IRM is based upon the existing site data discussed in Section 3.0. The basis of design for the IRM considers the following three design and operating conditions:

- 1. High flow operating condition;
- 2. Normal operating condition; and
- 3. Long-term average operations.

The design of the air stripper system is governed by flow rate, concentration of the influent and target effluent concentrations. The high flow operating condition represents the maximum design condition while the normal operating condition represents typical design conditions. Both the high flow and normal operating conditions are used as a basis for sizing the air stripper and to evaluate the short-term (hourly) potential air emission impacts. The long-term average operations is used to evaluate the long-term (annual) potential air emission impacts. The basis of design for each of these three conditions is provided on Table 3. Further details regarding the development of flow rates and VOC influent concentrations at each operating condition are described below. The target for treatment of VOCs in the effluent is 0.01 mg/l. These limits are established based on the NYSDEC's Best Available Technology Economically Achievable (BAT) guidance.

#### 4.2 Operating Conditions

#### 4.2.1 High Flow Operating Condition

This subsection summarizes the basis of design for the high flow operating condition at the oil skimmer pond overflow and clay pipe discharge. The basis of design of the treatment system for the



high flow operating condition is equal to the sum of the oil skimmer pond overflow and clay pipe discharge flows or 150 gpm.

The basis of design for the high flow operating condition at the oil skimmer pond overflow is 130 gpm.

This 130 gpm is extremely conservative considering:

- This flow rate is greater than all but one (300 gpm in November 1993) of the 36 flow measurements at Outfall 003 from January 1993 to June 1994;
- Based upon the Rational Method calculations which demonstrate that the percentage of flow from
  the oil skimmer pond overflow is only 11 percent of the wet-weather flow at Outfall 003, the oil
  skimmer pond flow would have only been approximately 33 gpm during the 300 gpm flow event
  measured at Outfall 003 in November 1993; and
- The 130 gpm flow rate would accommodate a rainfall event of approximately 1.4 inch per hour which is equivalent to just under a ten-year, one-hour frequency storm.

The basis of design for the high flow operating condition at the clay pipe discharge is 20 gpm. This flow rate is 10 times the estimated flow measured in November 1993 during RI sampling activities.

The basis of design with respect to VOCs for the high flow operating condition is based on the highest historical sampling results as described in Section 3.0. For the oil skimmer pond overflow, the data obtained at Outfall 003 from January 1993 to June 1994 was utilized since these sampling results had higher concentrations and covered a greater time period than those obtained from the oil skimmer pond overflow in April 1994. To be conservative, twice the highest observed concentrations from the six sampling events at a flow rate greater than 20 gpm were utilized. For the clay pipe discharge, the sampling results obtained during the November 1993 RI sampling event were utilized. The basis of



design for the treatment system influent concentrations are the flow weighted concentrations from the oil skimmer pond overflow and clay pipe discharge.

#### 4.2.2 Normal Operating Condition

The basis of design flow rate for the normal operating condition at both the oil skimmer pond overflow and the clay pipe discharge is equal to ½ the high flow operating condition. The basis of design with respect to VOC concentrations at the oil skimmer pond overflow is assumed to be twice the highest historical sampling results observed for flow events of less than 20 gpm at Outfall 003 (i.e., during the thirty sampling events). This basis of design will allow the system to accommodate variations in VOC influent concentrations while still remaining extremely conservative. The basis of design with respect to VOC concentrations for the clay pipe discharge is assumed to be twice the concentrations measured during the November 1993 RI sampling event. Similar to the high flow operating condition, the flow weighted concentrations from the two sources were utilized to calculate the treatment system basis of design influent conditions.

#### 4.2.3 Long-Term Average Operations

The flow and influent concentrations for the long-term average operations will be used for air permitting purposes only. To be conservative, the basis of design for the oil skimmer pond overflow is based upon the average flow and influent concentration for VOCs measured at Outfall 003 observed during the January 1993 to June 1994 monitoring period. The basis of design for the clay pipe discharge is equal to the flow rate and VOC concentrations observed during the November 1993 RI sampling event. Again, the flow weighted concentrations from the oil skimmer pond overflow and clay pipe discharge were utilized to calculate the long-term average treatment system basis of design concentrations.



#### 4.3 Treatment System Design

The surface water IRM treatment system design is described below. A process flow diagram showing treatment system components is included as Figure 2. The major treatment system components are shown on the partial site plan included as Figure 3 and are summarized on Table 4. Additional details on the IRM treatment system are found on the Contract Drawings that are bound separately from this Engineering Report.

#### 4.3.1 Process Description

The IRM treatment system and all equipment controls will be located in the southeast corner of the manufacturing building and will consist of a low-profile air stripper. The low-profile air stripper will treat influent pumped from two manholes which will collect water from the oil skimmer pond overflow and clay pipe discharge. From the low-profile air stripper, treated water will discharge by gravity to the surface water drainage ditch upstream of Outfall 003 on the southeast corner of the Chicago Pneumatics' property. The area around the low-profile air stripper will be contained by a 6-inch curb and will drain into a trench drain/sump. A sump pump will transfer any collected water to the inlet of the low-profile air stripper.

The low-profile air stripper will be designed to treat the high flow and normal operating conditions provided on Table 3. Off-gas from the low-profile air stripper will be discharged to atmosphere through a 26 foot high, 12-inch diameter discharge stack.

An 8-inch diameter pipe will be installed to allow the oil skimmer pond to overflow by gravity into a manhole designated as Pumping Manhole No. 1. The existing oil skimmer overflow pipes leading to Outfall 003 will be removed. Two submersible pumps will be installed in the manhole and will operate on a lead/lag/alternate sequence via level controls. Each of the two pumps will be capable



of pumping the normal operating flow of 65 gpm and will meet the high flow operating conditions of 130 gpm with both pumps running. During normal operating conditions (i.e., 65 gpm), the manhole pumps provide 100% installed backup capacity.

Water from the clay pipe will flow by gravity via an 8-inch diameter pipe into a manhole designated as Manhole No. 2 located just south of Bleecker Street on the north side of the Chicago Pneumatic property. Two submersible pumps will be installed in the manhole and will operate on a lead/lag/alternate sequence via level controls. Each of the two pumps will be capable of pumping the normal operating flow of 10 gpm and will meet the high flow operating condition of 20 gpm with both pumps running. During normal operating conditions (i.e., 10 gpm), the manhole pumps provide 100% installed backup capacity.

#### 4.3.2 Operating Alarms

The IRM treatment system will have an alarm system which will activate an auto-dialer and notify the Chicago Pneumatic Security Office (manned continuously) of certain alarm conditions. These alarm conditions include:

- High, High Level (indicating failure of both pumps) or Low, Low Level (indicating failure of a pump to shut off) at Pumping Manhole No. 1;
- High, High Level (indicating failure of both pumps) or Low, Low Level (indicating failure of a pump to shut off) at Pumping Manhole No. 2;
- High, High Level in the air stripper (indicating a blockage of the discharge line); and
- Loss of air flow to the air stripper (indicating blower failure).



Loss of air flow to the air stripper is a critical operating condition and will shut down all influent pumps to the air stripper. Should this condition occur, an operator will be required to investigate the problem and manually restart the blower and influent pumps. The remaining three alarm conditions will allow the treatment system to remain operational but provide notification of an abnormal operating condition. The Chicago Pneumatic security personnel will be trained to respond appropriately to each alarm condition.

#### 4.3.3 Additional Process Features

The total volume of water treated will be measured by flow meters providing instantaneous and totalizing flow readings. These flow meters will be located on air stripper influent pipeline from the oil skimmer pond, clay pipe, and the sump pump. Sample taps will be provided on all three influent lines and the effluent pipeline.

#### 4.3.4 Future Potential Process Upgrades

The IRM treatment system has been designed with additional treatment capacity which could be utilized for upgrading flow from the oil skimmer pond overflow or clay pipe discharge and/or other future remedial activities at the Site (if necessary). The following design features have been incorporated into the design to accommodate these future process upgrades:

- The air stripper has been designed to operate at a conservative inlet water temperature of 38°F and a conservative inlet air temperature of 50°F. Operating at temperatures greater than these will enhance air stripper performance.
- The maximum hydraulic capacity of the air stripper is 250 gallons per minute.



- An additional flow of 100 gpm at the high flow operating design concentrations of 1.9 mg/l for trichloroethylene, 0.34 mg/l for cis-1,2-dichloroethylene, 0.1 mg/l for trans-1,2-dichloroethylene, and 0.02 mg/l for vinyl chloride can be added to the treatment system influent and the target effluent concentrations of 0.01 mg/l would still be met for all four parameters.
- The flow from the two existing pumping manholes can be increased by 50% by merely upgrading the submersible pumps.
- A review of the available data on inorganic parameters has indicated that pretreatment is not required. However, the treatment system has been designed in such a manner that retrofitting for inorganic pretreatment, if necessary, can be easily accomplished.
- The air stripper effluent pipeline has been sized at 8-inch diameter to accommodate a discharge of 250 gpm.
- The transfer line inside of the manufacturing building from the clay pipe has been sized at 3-inch diameter to accommodate additional influent streams from the north side of the Chicago Pneumatic property (if necessary).

#### 4.4 Implementation of the Interim Remedial Measure

In parallel with this IRM Engineering Report, the following documents are being submitted to the NYSDEC:

- Contract Drawings;
- Air Permit Application to Construct; and
- SPDES Permit Modification Application.



Approval by NYSDEC of all four submittals will be necessary to implement the IRM.

The current schedule for the start up of the IRM is December 1994. In order to achieve this goal, preliminary approval by NYSDEC of the submittals by mid- to late-October 1994 is required. At that time, the air stripper will be placed on order and all exterior work will be completed prior to the onset of winter weather conditions. At the conclusion of construction, an Engineering Certification Report, certified by a professional engineer licensed to practice in New York State, will be prepared to certify that all facilities were constructed in accordance with this IRM Engineering Report and the Contract Drawings.

Respectfully submitted,

BLASLAND, BOUCK & LEE, INC.



Edward R. Lynch, P.E.

Executive Vice President

# CHICAGO PNEUMATIC TOOL COMPANY FRANKFORT, NEW YORK

# SURFACE WATER INTERIM REMEDIAL MEASURE DISCHARGE MONITORING DATA AT OUTFALL 003

Time	Flow (gpm)	Trichloroethene (mg/l)	cls-1,2- Dichloroethene (mg/l)	trans-1,2- Dichloroethene (mg/l)	Vinyl Chloride (mg/l)
1993					
January	15	0.44	0.15	<0.02	<0.02
	15	0.27	0.62	<0.02	<0.02
February	4 4	2.2 1.8	1 1.1	<0.05 <0.05	<0.05 <0.05
March	4	2	0.85	<0.05	<0.05
	10	1.7	0.44	<0.05	<0.05
April	100	0.2	0.064	<0.01	<0.01
	6	0.21	0.097	<0.01	<0.01
May	13	0.011	0.038	<0.005	<0.005
	55	0.005	0.01	<0.005	<0.005
June	0.6	0.008	0.016	<0.005	<0.005
	4	0.026	0.082	<0.001	0.007
July	0.2 No Flow	<0.005 	<0.005 	<0.005	<0.005 
August	No Flow No Flow	<del></del>	 		
September	0.3	0.011 <0.001	0.022 0.008	<0.001 <0.001	<0.001 <0.001
October	3	0.016	0.039	<0.001	<0.004
	12	0.026	0.065	<0.005	<0.005
November	300	0.29	0.16	<0.01	0.013
	5	0.99	0.34	<0.05	<0.05
December	8	0.031	0.02	<0.001	<0.001
	10	0.7	0.21	<0.02	<0.02
1994					
January	20	0.51	0.36	<0.02	<0.02
	5	0.22	0.71	<0.02	0.035
February	5	0.63	0.5	<0.02	<0.02
	5				
March	42	0.5	0.14	<0.02	<0.02
	2	0.67	0.18	<0.05	<0.05
April	10	0.01	0.026	<0.005	<0.005
	37	0.1	0.058	0.005	0.005

# TABLE 1 (Cont'd) CHICAGO PNEUMATIC TOOL COMPANY FRANKFORT, NEW YORK

# SURFACE WATER INTERIM REMEDIAL MEASURE DISCHARGE MONITORING DATA AT OUTFALL 003

Time	Flow (gpm)	Trichloroethene (mg/l)	cis-1,2- Dichloroethene (mg/l)	trans-1,2- Dichloroethene (mg/l)	Vinyl Chloride (mg/l)
Мау	19	0.11	0.15	<0.01	<0.01
	60	0.059	0.071	<0.01	<0.01
June	3.8	<0.001	0.012	<0.001	0.004
	0.3	<0.001	0.002	<0.001	<0.001

#### Notes:

1. Data provided by Chicago Pneumatic Tool Company.

2. gpm = gallons per minute.

3. mg/l = milligrams per liter.

#### CHICAGO PNEUMATIC TOOL COMPANY FRANKFORT, NEW YORK

#### SURFACE WATER INTERIM REMEDIAL MEASURE INVESTIGATION OF STREAMS THAT CONTRIBUTE FLOW TO OUTFALL 003

	Oll Skimmer Pond Overflow		Manufacturing Building Roof Leader		Warehouse Floor Drains		Warehouse Exterior Loading Dock Trench Drains	
Parameter	4/1/94	4/8/94	4/1/94	4/8/94	4/1/94	4/8/94	4/1/94	4/8/94
Flow (gpm)	2	2	2	10	No Flow	No Flow	12	No Flow
Trichloroethene (mg/l)	0.005	0.120	<0.001	<0.005			<0.001	
cis-1,2-Dichloroethene (mg/l)	0.031	0.068	<0.001	<0.005	_		<0.001	
trans-1,2-Dichloroethene (mg/l)	<0.001	<0.005	<0.001	<0.005			<0.001	
Vinyl chloride (mg/l)	0.003	<0.005	<0.001	<0.005		_	<0.001	

#### Notes:

- 1. Data provided by Chicago Pneumatic Tool Company.
- gpm = gallons per minute. mg/l = milligrams per liter. 2.
- 3.

#### CHICAGO PNEUMATIC TOOL COMPANY FRANKFORT, NEW YORK

#### SURFACE WATER INTERIM REMEDIAL MEASURE **BASIS OF DESIGN**

Parameter		Target Effluent Concentration		
. di alliotoi	Oil Skimmer Pond	Clay Pipe	Treatment System Influent	(mg/l)
High Flow Operating Conditions				
Flow (gpm)	130	20	150	
Trichloroethylene	1.0	7.6	1.9	<0.010
cis-1,2-Dichloroethylene	0.32	0.5	0.34	<0.010
trans-1,2-Dichloroethylene	<0.04	0.5	0.1	<0.010
Vinyl chloride	0.026	<0.01	0.02	<0.010
Normal Operating Conditions				
Flow (gpm)	65	10	75	
Trichloroethylene	4.4	15.2	5.8	<0.010
cis-1,2-Dichloroethylene	2.2	1.0	2.0	<0.010
trans-1,2-Dichloroethylene	<0.04	1.0	0.2	<0.010
Vinyl chloride	0.07	<0.01	0.06	<0.010
Long-Term Average Operations				
Flow (gpm)	23	2	25	
Trichloroethylene	0.28	7.6	0.87	<0.010
cis-1,2-Dichloroethylene	0.09	0.5	0.12	<0.010
trans-1,2-Dichloroethylene	0.01	0.5	0.05	<0.010
Vinyl chloride	0.01	<0.01	0.01	<0.010

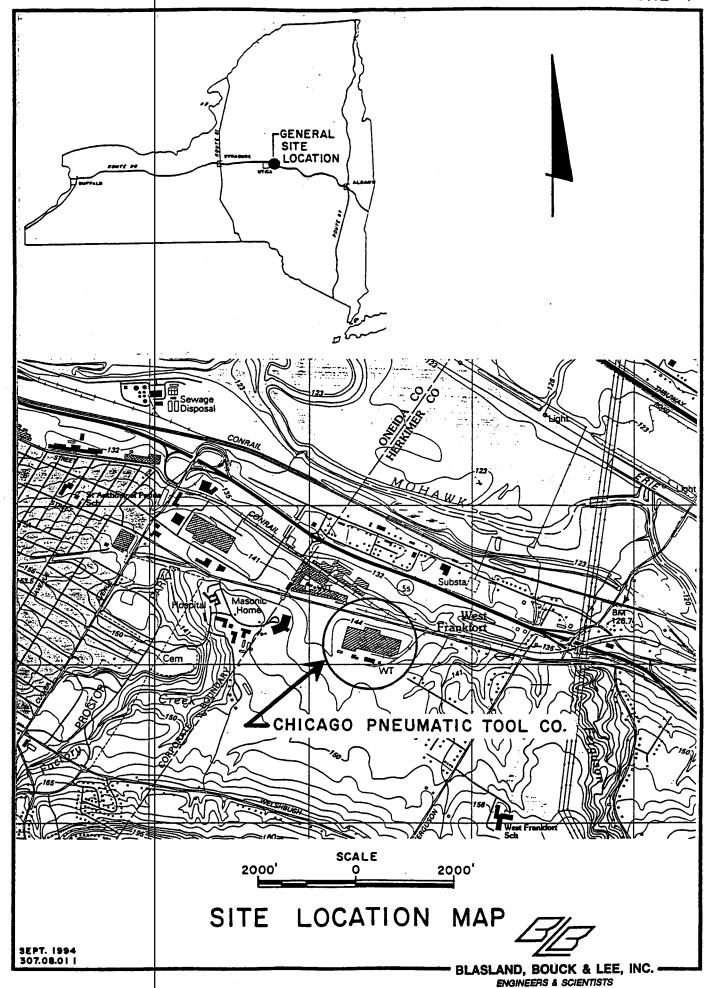
#### Notes:

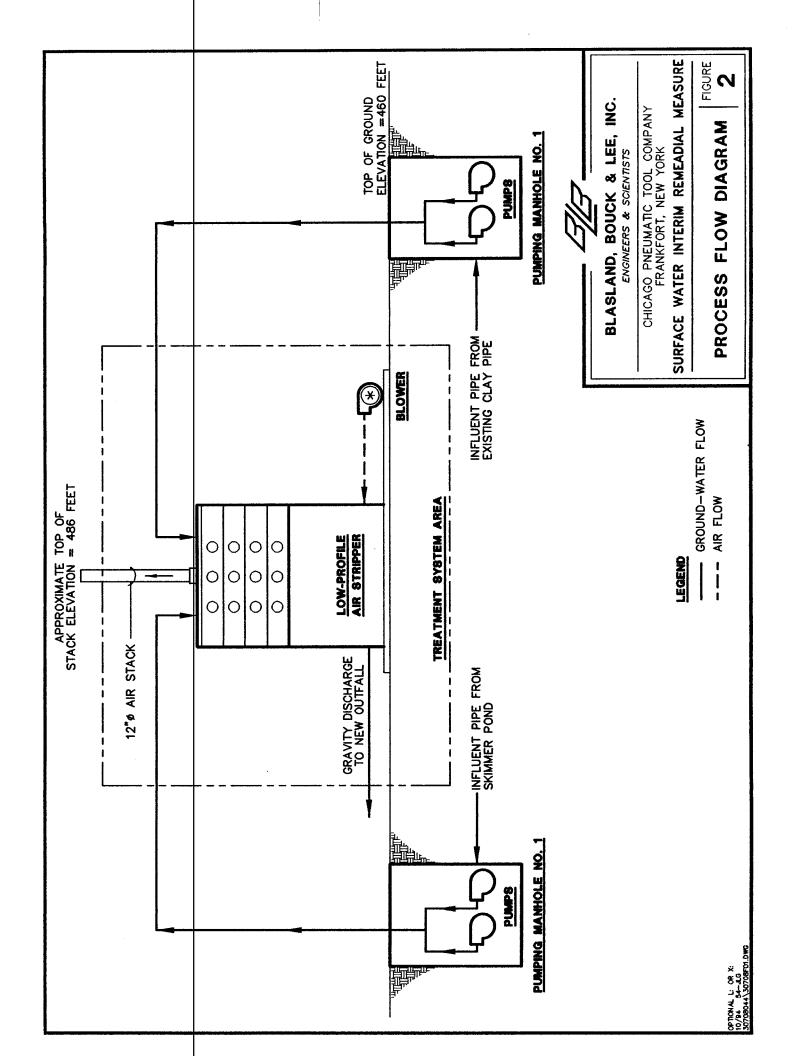
gpm = gallons per minule. mg/l = milligrams per liter. 1.

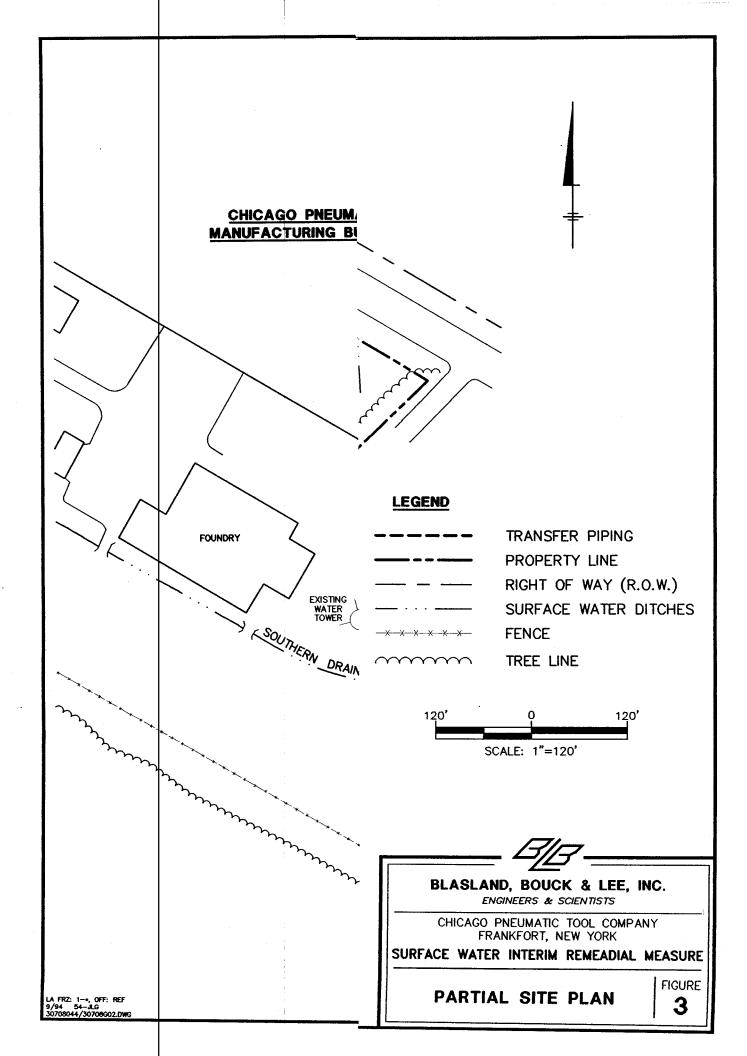
# CHICAGO PNEUMATIC TOOL COMPANY FRANKFORT, NEW YORK

# SURFACE WATER INTERIM REMEDIAL MEASURE TREATMENT SYSTEM EQUIPMENT SUMMARY

Quantity	Description	Specifications
1	Low-Profle Air Stripper	ShallowTray Model 31241 with one 20 HP blower capable of providing 1,800 cubic feet per minute of air at 32 inches of water column and 4 stainless steel trays. Air to water ratio at design water flow rate of 150 gallons per minute (gpm) is 90:1.
2	Pumping Manhole No. 1 Pumps	Myers Model ME75 capable of 65 gpm at 28 feet of head.
2	Pumping Manhole No. 2 Pumps	Myers Model ME50 capable of 10 gpm at 43 feet of head.
3	Flow Meters	Signet analog flow meter which displays flow rate and totalized flow volume.







14-16-4 (2/87) — Text 12	
PROJECT I.D. NUMBER	 

#### 617.21

**SEQR** 

#### Appendix C

#### State Environmental Quality Review SHORT ENVIRONMENTAL ASSESSMENT FORM For UNLISTED ACTIONS Only

PART I—PROJECT INFORM	ATION (To be completed by App	olicant or Project sponsor)	
1. APPLICANT/SPONSOR Chicago Pneumatic To	ol Company	2. PROJECT NAME Surface Water Interim Reme	dial Measure
3. PROJECT LOCATION:			
Municipality Frankfo	rt Township	County Herkimer	
4. PRECISE LOCATION (Street a	ddress and road intersections, prominent	landmarks, etc., or provide map)	
2200 Bleecker Street Utica, New York 1350			
5. IS PROPOSED ACTION:			· · · · · · · · · · · · · · · · · · ·
XX New Expans	on Modification/alteration		
6. DESCRIBE PROJECT BRIEFL	Ÿ:		
Surface water treatm	ent system consisting of a low	-profile air stripper.	
•			
		•	
7. AMOUNT OF LAND AFFECTE	D:		
Initially <u> </u>	acres Ultimately < 1	acres	
	MPLY WITH EXISTING ZONING OR OTHE	ER EXISTING LAND USE RESTRICTIONS?	
X Yes No If N	o, describe briefly		,
			• *
9. WHAT IS PRESENT LAND US	E IN VICINITY OF PROJECT?		
	ustrial Commercial Ag	griculture Park/Forest/Open space	Other
Describe:			
	ERMIT APPROVAL, OR FUNDING, NOW (	OR ULTIMATELY FROM ANY OTHER GOVE	RNMENTAL AGENCY (FEDERAL,
STATE OR LOCAL)?  ☑ Yes ☐ No	If you list appear(s) and parmittenesses	<b>1</b> ~	
⊠ tes □ No	If yes, list agency(s) and permit/approva	ıs	
	truct and Operate		The second secon
SPDES Permit Modi			
	E ACTION HAVE A CURRENTLY VALID F es, list agency name and permit/approval		•
Existing SPDES Permi	t No. NY 0108537 - NYSDEC		· · · · · · · · · · · · · · · · · · ·
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12. AS A RESULT OF PROPOSE  Yes No	D ACTION WILL EXISTING PERMIT/APPRO	OVAL REQUIRE MODIFICATION?	eg Demografia Berlinder og det i statister
I CERTIF	Y THAT THE INFORMATION PROVIDED	ABOVE IS TRUE TO THE BEST OF MY KNO	WLEDGE
Applicant/sponsor name:	avid L. Rosbrook, Senior Vice	President	Date: 12 Oct 94
Signature:	Il = Rockrook	A Company of the Comp	

If the action is in the Coastal Area, and you are a state agency, complete the Coastal Assessment Form before proceeding with this assessment

#### Chicago Pneumatic Tool Company Frankfort, New York Surface Water Interim Remedial Measure

#### Attachment 1

#### **Assumptions**

1. The surface water Interim Remedial Measure consists of two influent surface water sources, the oil skimmer pond and the clay pipe, that collect into two manholes and are pumped via level control to a low-profile air stripper. The flow into the manholes will vary widely so the following two short-term (hourly) and one long-term (annual) design conditions were developed:

#### Short-Term Design Condition

- High flow; and
- Normal flow.

#### Long-Term Design Condition

Average flow.

The high flow design condition is 150 gallons per minute (gpm) which represents the maximum capacity of the pumps used to transfer water from the manholes to the low-profile air stripper. Under the normal flow design condition, water accumulates into the two pumping manholes at a flow rate of up to 75 gpm until pumps are started to transfer water to the low-profile air stripper. The average flow design condition of 25 gpm represents the average condition anticipated over a full year of operation. The development of these flow rates and the associated chemical concentrations is described in detail in an Engineering Report for this project. The high flow and normal flow design conditions will be used to evaluate the long-term (annual) ambient air quality impacts while the average flow design condition will be used to evaluate the long-term (annual) ambient air quality impacts. These three design conditions and the resultant air emission mass load ngs are summarized below.

#### Short-Term Air Emissions

High Flow Design Conditions

	Concentration	Hourly Mass Loading		
Parameter	Oil Skimmer Pond	Clay Pipe	Treatment System Influent	[pounds per hour (lbs/hour)]
Flow [gallons per minute (gpm)]	130	20	150	•-
Trichloroethylene (TCE)	1.0	7.6	1.9	0.1427
cis-1,2-Dichloroethylene (cis-1,2-DCE)	0.32	0.5	0.34	0.0255
trans-1,2-Dichloroethylene (trans-1,2-DCE)	< 0.04	0.5	0.1	0.0075
Vinyl chloride (VC)	0.026	< 0.01	0.02	0.0015

#### Normal Flow Design Conditions

	Co	Hourly Mass		
Parameter	Oil Skimmer Pond	Clay Pipe	Treatment System Influent	Loading (Ibs/hour)
Flow (gpm)	65	10	75	
TCE	4.4	15.2	5.8	0.2178
cis-1,2-DCE	2.2	1.0	2.0	0.0751
trans-1,2-DCE	<0.04	1.0	0.2	0.0075
VC VC	0.07	< 0.01	0.06	0.0023

#### Long-Term Air Emissions

#### Average Flow Design Conditions

Parameter	Co	ncentration (m	Mass Loading		
	Oil Skimmer Pond	Clay Pipe	Treatment System Influent	Hourly (lbs/hour)	Annual (lbs/year)
Flow (gpm)	23	2	25	= +-	
TCE	0.28	7.6	0.87	0.0109	95.4
cis-1,2-DCE	0.09	0.5	0.12	0.0015	13.2
trans-1,2-DCE	0.01	0.5	0.05	0.0006	5.5
VC VC	0.01	< 0.01	0.01	0.0001	1.1

- 2. Ambient air quality input screening analysis conducted in accordance with the revised Appendix B of NYSDEC's Air Guide 1, dated April 12, 1994. Short-Term Guideline Concentrations (SGCs) and Annual Guideline Concentrations (AGCs) for each parameter were taken from the 1991 edition of NYSDEC's Draft Air Guide 1.
- 3. Air stripper removal efficiency is 100 percent for all parameters.
- 4. Operating period is 24 hours per day and 365 days per year.
- 5. Proposed stack height (h<sub>s</sub>) is 26 feet.
- 6. Building height  $(h_b)$  is 17 feet.
- 7. Shortest distance to the closest property line (D<sub>Pl</sub>) is 400 feet.
- 8. Exit temperature at stack is ambient (assume 72°F).

#### Calculations

- Since the horizontal extent of building cavity 3  $h_b = 51$  feet (where  $h_b = 17$  feet) is less than the shortest distance to the closest property line  $D_{Pl} = 400$  feet, then cavity impacts are confined to on-site receptors and the building cavity impacts do not need to be calculated.
- 2. Effective Stack Heigh

Since the stack exit temperature is at ambient conditions, a plume rise will not be calculated. Therefore, the effective stack height  $(h_e)$  is equal to the actual stack height  $(h_s)$  of 26 feet. However, since the ratio of the stack height to the building height  $(h_s/h_b)$  or 26/17 = 1.53 is greater than 1.5, but less than 2.5, all calculated impacts will be reduced by a factor of 0.75.

- 3. Maximum Actual Annual Impact (Ca)
  - $C_a$  [micrograms per cubic meter ( $\mu$ g/m³)] =  $\frac{(0.75)(6.0)(Q_a)}{h_a^{2.25}}$  [Equation III.A.2.]

 $Q_a$  (TCE) = 95.4 lbs/year

 $Q_a^*$  (cis-1,2-DCE) = 13.2 lbs/year

 $Q_a$  (trans-1,2-DCE) = 5.5 lbs/year

 $Q_a^a$  (VC) = 1.1 lbs/year

 $h_{e} = 26$  feet

 $C_a (TCE) = 0.28 \, \mu g/m^3$ 

 $C_a^{\mu}$  (cis-1,2-DCE) = 0.039  $\mu$ g/m<sup>3</sup>

 $C_a^a \text{ (trans-1,2-DCE)} = 0.016 \ \mu\text{g/m}^3$ 

 $C_a^{\circ} (VC) = 0.003 \, \mu g/m^3$ 

- 4. Maximum Short-Term Impacts (C<sub>st</sub>)
  - $C_{ST}$  ( $\mu g/m^3$ ) =  $\underline{(0.75)(65)(52,500)(Q)}$  [Equations III A.3 and III.A.5]  $h_e^{2.25}$

#### High Flow Design Conditions

Q (TCE) = 0.1427 lbs/hour

Q (cis-1,2-DCE) = 0.0255 lbs/hour

Q (trans-1,2-DCE) = 0.0075 lbs/hour

Q (VC) = 0.0015 lbs/hour

 $h_{\rm e} = 26 \, {\rm ft}$ 

 $C_{ST}$  (TCE) = 239  $\mu g/m^3$ 

 $C_{ST}$  (cis-1,2-DCE) = 43  $\mu$ g/m<sup>3</sup>

 $C_{ST}^{(3)}$  (trans-1,2-DCE) = 13  $\mu$ g/m<sup>3</sup>

 $C_{sr}$  (VC) = 3  $\mu$ g/m<sup>3</sup>

#### Normal Flow Design Conditions

Q (TCE) = 0.2178 lbs/hour

Q (cis-1,2-DCE) = 0.0751 lbs/hour

Q (trans-1,2-DCE) = 0.0075 lbs/hour

Q(VC) = 0.0023 lbs/hour

 $h_{a} = 26 \text{ ft}$ 

 $C_{ST}$  (TCE) = 365  $\mu$ g/m<sup>3</sup>

 $C_{ST}$  (cis-1,2-DCE) = 126  $\mu$ g/m<sup>3</sup>

 $C_{SI}$  (trans-1,2-DCE) = 13  $\mu$ g/m<sup>3</sup>

 $C_{ST}^{\circ}$  (VC) = 4  $\mu$ g/m<sup>3</sup>

5. Comparison of Annual and Short-Term Impacts

#### **Annual Impacts**

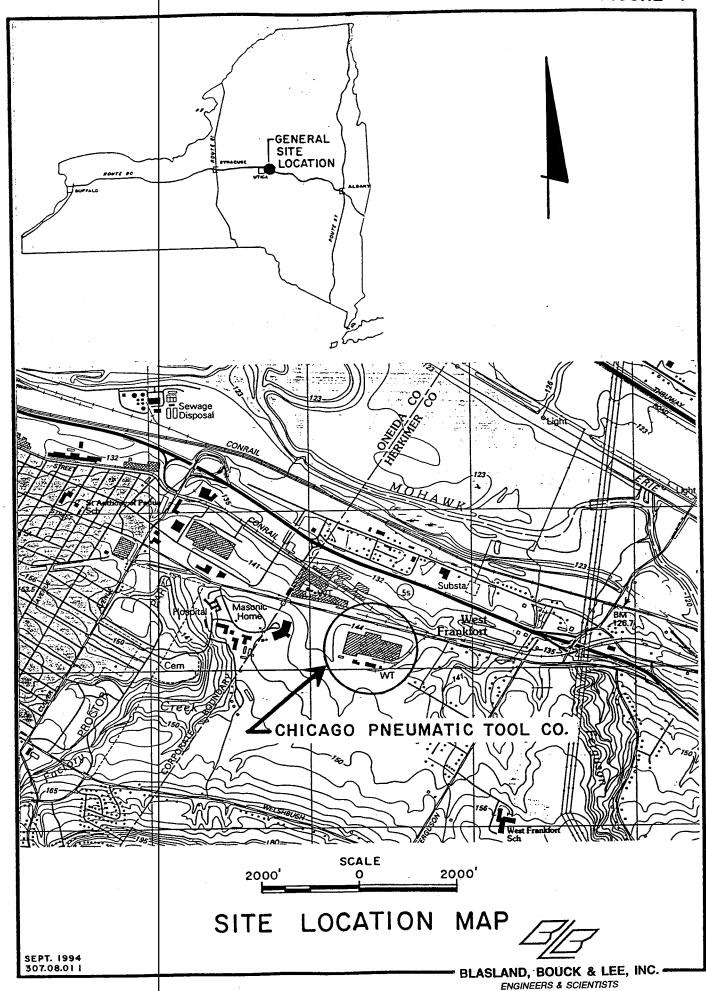
Parameter	AGC (μg/m³)	C <sub>a</sub> (μg/m³)
TCE	0.45	0.28
cis-1,2-DCE	1,900	0.039
trans-1,2-DCE	360	0.016
VC	0.02	0.003

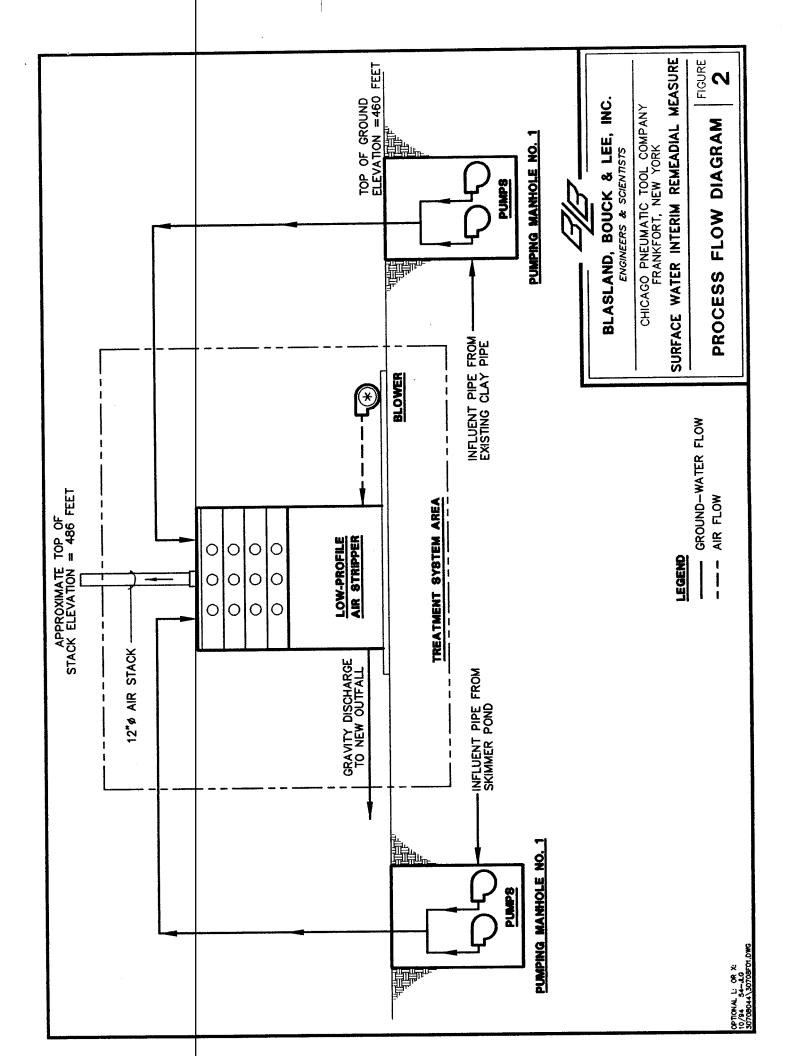
#### **Short-Term Impacts**

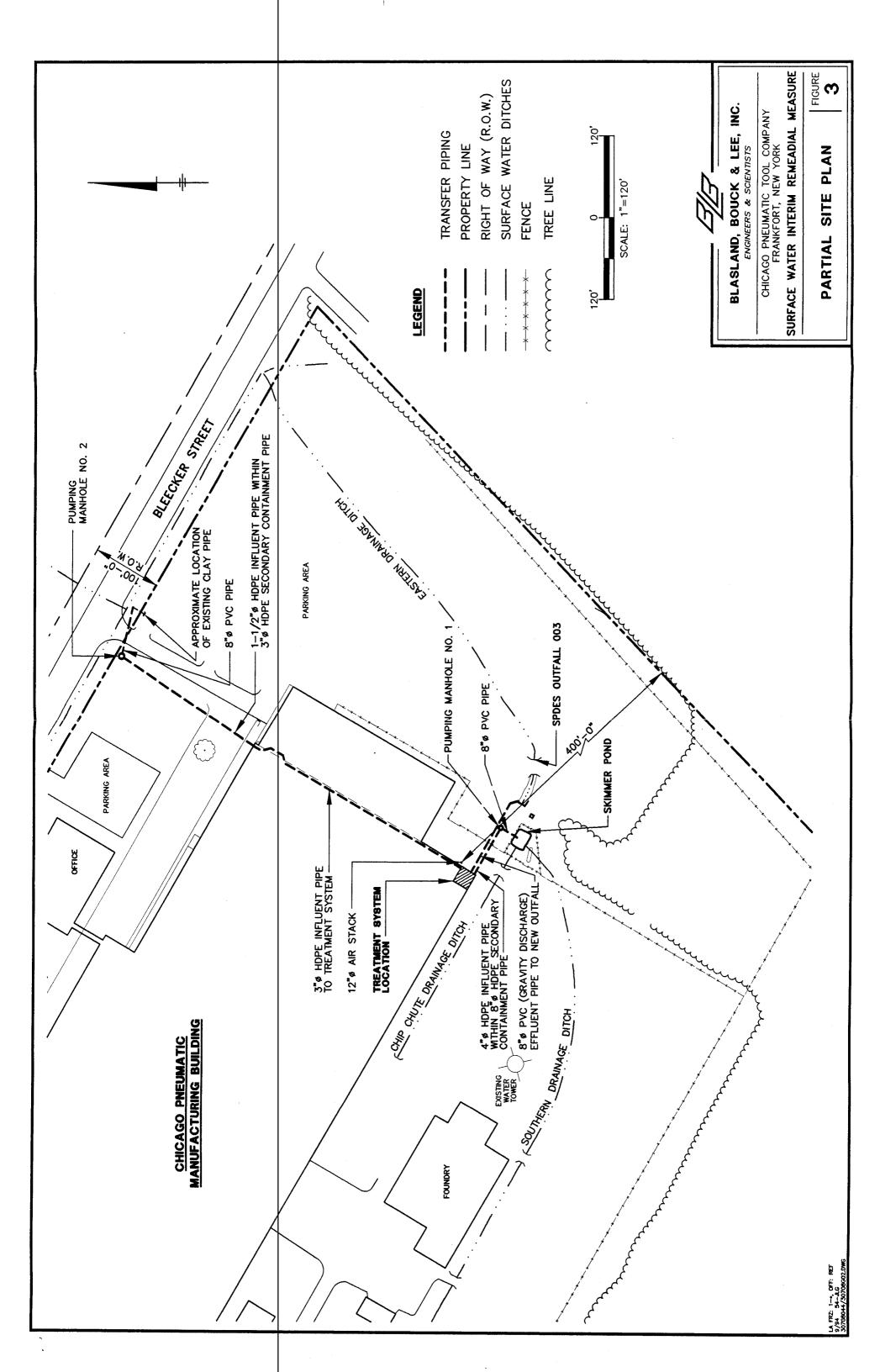
		High Flow Design Conditions	Normal Flow Design Conditions		
Paramete	r SGC (μg/m³)	C <sub>sτ</sub> (μg/m³)	C <sub>sτ</sub> (μg/m³)		
TCE	33,000	239	365		
cis-1,2-DCE	190,000	43	126		
trans-1,2-DCE	190,000	13	13		
VC	1,300	3	4		

#### 6. Assessment of Comparison

The  $C_a$  and  $C_{ST}$  for all parameters are less than the respective AGCs and SGCs, therefore, no emissions controls are required.







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				K .X.			YES	MAR	FORM
SPECIFIC QUI	STIONS	YES	NO	FORM ATTACHED		SPECIFIC QUESTIONS	YES	40	ATTACHED
A. Is this facility a publicly	owned treatment works				В.	Does or will this facility (either existing or proposed)	1		
which results in a dischar	ge to waters of the U.S.?		Х			include a concentrated animal feeding operation or aquatic animal production facility which results in a		X	
(FORM 2A)						discharge to waters of the U.S.? (FORM 2B)	19	20	21
C. Is this a facility which cur	rently regults in discharge	16	17	18	D	le this a proposed facility (other than those described		1	
to waters of the U.S. other	er than those described in	Х			J -:	in A or B above) which will result in a discharge to	X		X :
A or B above? (FORM 2C)		22	23	24	<u> </u>	waters of the U.S.? (FORM 2D)	25	26	27
E. Does or will this facility	tract store or dispose of			ļ	F.	Do you or will you inject at this facility industrial or municipal effluent below the lowermost stratum con-		X	
hazardous wastes? (FORM)	R)		X		ĺ	existing within one quarter mile of the Well bore.		^	
Hazardous Wastes: (1 C11111	ľ			ļ	Į	underground sources of drinking water? (FORM 4)	31	32	33
G. Do you or will you inject a	t this facility any produced	28	29	30	<del> </del>				
water or other fluids which	are brought to the surface				H.	. Do you or will you inject at this facility fluids for spe- cial processes such as mining of sulfur by the Frasch		X	
in connection with convent	lional oil or natural gas pro-		Х		l	process solution mining of minerals, in situ combus-		``	
duction, inject fluids used	for enhanced recovery of fluids for storage of liquid		^		1	tion of fossil fuel, or recovery of geothermal energy?	1		
hydrocarbons2 (EORM 4)		34	38	36	1	(FORM 4)	37	38	39
I is this facility a proposed	stationary source which is				J.	Is this facility a proposed stationary source which is		1	
one of the 28 industrial	categories listed in the in-	1			}	NOT one of the 28 industrial categories listed in the instructions and which will potentially emit 250 tons		X	
structions and which will	potentially emit 100 tons utant regulated under the		Χ		l	nor year of any air poliutant regulated under the Clean		"	
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Form		<del></del>	w Sources and Ne	ew Dischargers
2D S	<b>EPA</b>	Application for	or Permit to Disch	narge Process Wastewater
. Outfall Location				
For each outfa	<del></del>	tude and longitude, and the na	ame of the receiving water. eceiving Water (name)	
Outfall Number (list)	Deg Min		eceiving water (name)	
03A			nnamed tributary of Mohawk R	River.
	1			
		d expect to begin discharging?	December 1, 1994	
II. Flows. Source	s of Pollution	and Treatment Technologie		wastewater to the effluent including
process w	vastewater, each operati	Isanitary wastewater, co	cooling water, and stormwate	wastewater to the effluent, including ter runoff; (2) The average flow contributes water. Continue on additional sheets
Outfall Number	1. 0	perations Contributing Flow (list)	2. Average Flow (include units)	3. Treatment (Description or List Codes from Table 2D-1)
03A		ter from "clay pipe" at e of property	2,880 gpd	Low-profile air stripper
03A	Oil skimme	er pond overflow	33,120 gpd	Low-profile air stripper
		TOTAL	36,000 gpd	
			<u> </u>	

CONTINUED FROM THE FRONT	EPA ID Number (copy from Item 1 of Form 1)	Outfall Number
COMMINGED PROMITHE PROMI	NYD 002230977	03A

#### V. Effluent Characteristics

A, and B: These items require you to report estimated amounts (both concentration and mass) of the pollutants to be discharged from each of your outfalls. Each part of this item addresses a different set of pollutants and should be completed in accordance with the specific instructions for that part. Data for each outfall should be on a separate page. Attach additional sheets of paper if necessary.

#### General Instructions (See table 2D-2 for Pollutants)

Each part of this item requests you to provide an estimated daily maximum and average for certain pollutants and the source of information. Data for all pollutants in Group A, for all outfalls, must be submitted unless waived by the permitting authority

For all outfalls, data for pollutants in Group B should be reported only for pollutants which you believe will be present or are limited directly by an effluent limitations guideline or NSPS or indirectly through limitations on an indicator pollutant.

1. Pollutant	2. Maximum Daily Value (include units)	3. Average Daily Value (include units)	4. Source (see instructions)
Flow	216,000 apd	36,000 gpd	1 (Engineering Study)
[rich]orethylene	1.9 mg/1	0.87 mg/l	1 (Engineering Study)
	3.4 #/d	0.26 #/d	1 (Engineering Study)
Cis-1,2-dichloroethylene	0.34 mg/l	0.12 mg/l	1 (Engineering Study)
	0.61 #/d	0.036 #/d	1 (Engineering Study)
trans-1,2-dichloroethylere	0.1 mg/1	0.05 mg/1	1 (Engineering Study)
	0.18 #/d	0.015 #/d	1 (Engineering Study)
Vinyl Chloride	0.02 mg/1	0.01 mg/1	1 (Engineering Study)
VIIIyi diriorida	0.036 #/d	0.003 #/d	1 (Engineering Study)
A waiver is requested for all			
additional parameters since the	ne.		
two sources currently dischar	ge		
to surface water and the prop	osed		
treatment system is not desig	ned		
to treat any other parameter	beyond		
those listed above.			
			CONTINUE ON REVE

EPA ID Number (copy from item one of Form 1)
NYD 002230977

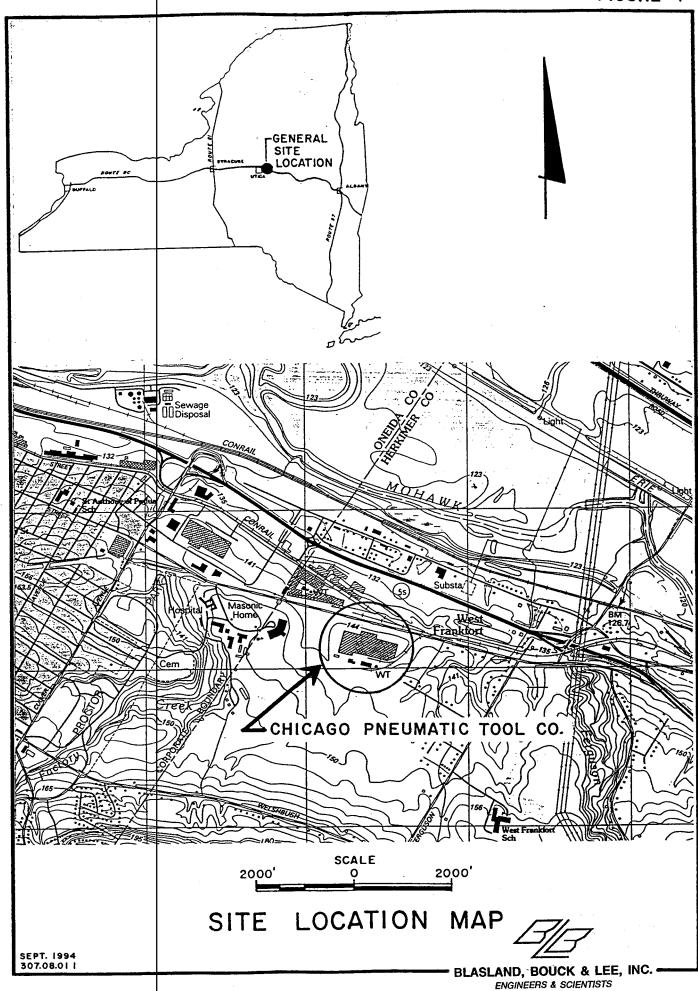
Vii	. Other Information (Option	al)		and the second of the control of the second of	
	the street balance	to expand upon any o u feel should be con	of the above questions nsidered in establishin	or to bring to the attenti g permit limitations for	on of the reviewer any the proposed facility.
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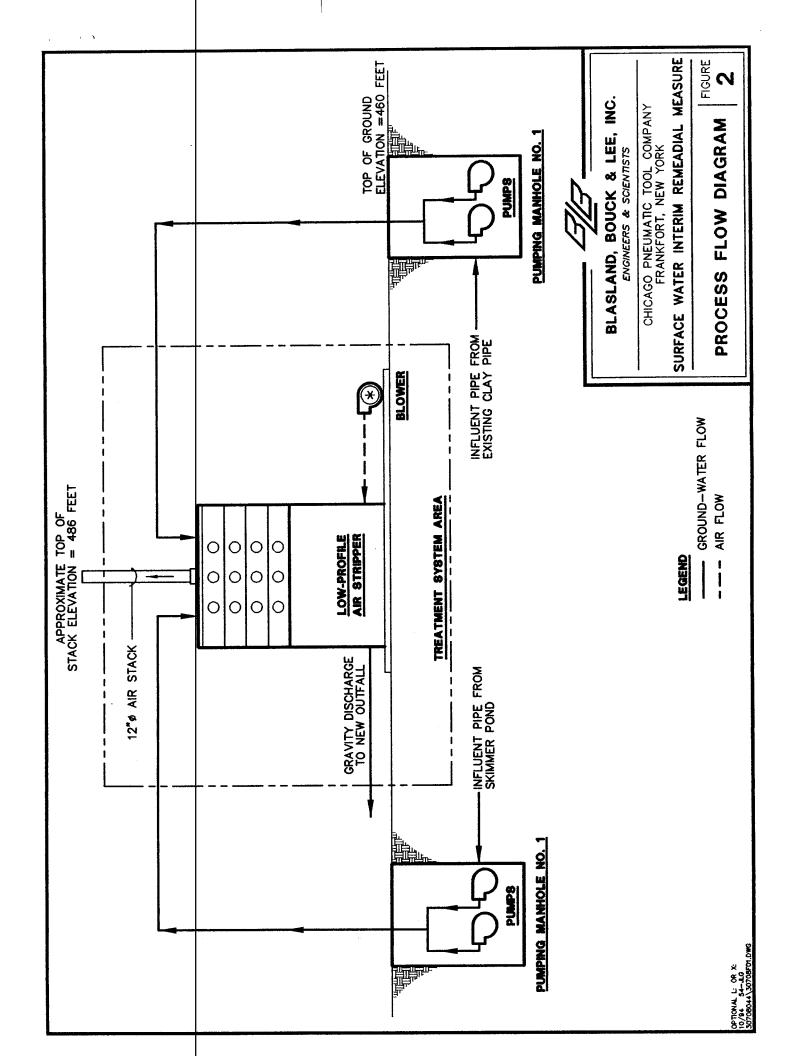
The permit limitations for Oufall O3A should be established based on the New York State Department of Environmental Conservation Division of Water Best Available Technology Economically Achievable (BAT) Guidance.

#### VIII. Certification

I certify under penalty of law that this document and all attachments were prepared under my direction or supervision in accordance with a system designed to assure that qualified personnel properly gather and evaluate the information submitted. Based on my inquiry of the person or persons who manage the system, or those persons directly responsible for gathering the information, the information submitted is, to the best of my knowledge and belief, true, accurate, and complete. I am aware that there are significant penalties for submitting false information, including the possibility of fine and imprisonment for knowing violations.

1	A. Name and Official Title (ty	pe or print)	B. Phone No.
	David L. Rosbrook,	Senior Vice President	(315) 792-2710
I	C. Signature		D. Date Signed
	l • • • • • • • • • • • • • • • • • • •	amil & Rorbrook	12 oct 94





FORM			NMENTAL PROTEC		I. EPA I.D. NUMBER		
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is exclude	ed from permit requ	irements; see Section C of the	instructions. See also	, Section D of the instructions	for definitions of bold-faced	terms.	
		ESTIONS	MARK 'X'				ARK 'X'
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F Does	or will this facility	y treat, store, or dispose of		F. Do you or will you inject			
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L			28 29 30	underground sources of di		31 3	2 33
		at this facility any produced		H. Do you or will you inject	at this facility fluids for spe-		
		dh are brought to the surface ritional oil or natural gas pro-		cial processes such as mi	ning of sulfur by the Frasch	;	X
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	natural gas, or injectorations? (FORM 4)	dt fluids for storage of liquid	34 35 36	(FORM 4)	<b>,</b> , , , , , , , , , , , , , , , , , ,	37 3	39
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VI. FACIL	ITY LOCATION						
	A. STREE	, ROUTE NO. OR OTHER S	PECIFIC IDENTIFIE	i R			
5 2 2 0		CVED STREET	<del>, , , , , , , , , , , , , , , , , , , </del>				
5 2 2 0	O BLEE	CKER STREE		45			
		B. COUNTY NAME	t				
1111			<del>er, raas</del> ,				
HER	KI M ER	<del> </del>	<del></del>	70			
		C. CITY OR TOWN		D.STATE E. ZIP COD	E F. COUNTY CODE		
9	<del> </del>	<del>                                     </del>	<del>, , , , , , , , , , , , , , , , , , , </del>	<del></del>	11 7.7760		
6 F.R.A	NKF ORI	T.O.W N SH .I P	<del></del>	N Y 1 3 5 0 1			1.00

CONTINUED FROM THE FRONT		
VII. SIC CODES (4-digit, in order of priority)		
A. FIRST		B. SECOND
7 3 5 4 6 Power driven hand tools	7 3 5 3 6 (specify)	la de la companya de
15 16 - 10	7 3,5,3,6	doists
C. THIRD		D. FOURTH
7 3, 3, 6,5 Aluminum foundry	7 3,3,6,6 (specify) Non-	ferrous foundry (brass-, bronze-, r-based alloys)
VIII. OPERATOR INFORMATION	1.9 1.6 and copper	bused arroys;
Α.	NAME	B. is the name listed in
		item VIII-A also the owner?
8 CHICAGO PNEUMATIC TOO	L COMPANY	X YES NO
15 10		56 facility, not site
C. STATUS OF OPERATOR (Enter the appropriate letter if		D. PHONE (area code & no.)
F = FEDERAL M = PUBLIC (other than federal or state S = STATE O = OTHER (specify) P = PRIVATE	, P (1950)	A 3 1 5 7 9 2 2 6 0 0
E. STREET OR P.O. BOX	14	15 16 18 19 21 22 - 29
2200 BLEECKER STRE	<u> </u>	
3	35	
F. CITY OR TOWN	G.STATE H. ZIP CODE	
BUTICA	NY 13 501	Is the facility located on Indian lands?  YES X NO
15 16	<del></del>	52
X. EXISTING ENVIRONMENTAL PERMITS	40 41 42 47 - 51	
A. NPDES (Discharges to Surface Water) D. PSD (	Air Emissions from Proposed Sources)	
	T T T T T T T T T T T T T T T T T T T	
9 N N, Y, O, 1 , O, 8 5 3 7, , 9 P	<del></del>	
8. UIC (Underground Injection of Fluids)	E. OTHER (specify)	
9 0	(spec	38 air emission operating
15 16 17 18 - 30 15 16 17 18	30	permits
C. RCRA (Hazardous Wastes)	E. OTHER (specify)	
9 R	(spec	rify)
XI. MAP	30	
Attach to this application a topographic map of the area	extending to at least one mile beyond pro	perty bounderies. The map must show
the outline of the facility, the location of each of its extreatment, storage, or disposal facilities, and each well was bediened to the contract had been seen as the contract had been s	STING and proposed intake and discharge	eterioturae anch of its hazardava wase
water bodies in the map area. See instructions for precise	requirements. (See Figures 1 a	nd 3)
XII. NATURE OF BUSINESS (provide a brief description)	The second of th	114 3)
provide a price description?		
The manufacturer, distribution, and sale of	portable pneumatic and electric-dr	riven hand tools.
- 1		
		· ·
YIII CERTIFICATION (and instrumed and		
XIII. CERTIFICATION (see instructions)		
I certify under penalty of law that I have personally exam	nined and am familiar with the information	on submitted in this application and all
attachments and that, based on my inquiry of those p application, I believe that the information is true, accura-	ersons immediately resoonsible for obtail	ning the information contained in the
false information, including the possibility of fine and imp	prisonment.	are significant penalties for submitting
A. NAME & OFFICIAL TITLE (type or print)	B. SIGNATURE	C. DATE SIGNED
		1
David L. Rosbrook Senior Vice President	Dan Koderook	12 oct 94
COMMENTS FOR OFFICIAL USE ONLY		
	<del></del>	

•		,		
Please type or print	in the unshaded	1 11/0 000000	r (copy from Item 1 of Form 1, 1977	Form Approved OM8 No. 2040-0086 Approval exorces 7-31-88
2D	<u> </u>	New	Sources and N	lew Dischargers
NPOES	<b>PEPA</b>	Application for	Permit to Disc	harge Process Wastewate
I. Outfall Location	n file s		an esta de la compania del la compania de la compan	
For each out	· · · · · · · · · · · · · · · · · · ·	tude and longitude, and the name		A STATE OF THE STA
(list)	Deg Min		iving Water <i>(name)</i>	
03A	43 05	11 75 10 55 Unnam	ned tributary of Mohawk	River.
03/1	13 13			
	<u> </u>		· · · · · · · · · · · · · · · · · · ·	
	:			
	:			
	;			
II. Discharge Dat	e (When do yo	u expect to begin discharging?)	December 1, 1994	
		, and Treatment Technologies		
<ul> <li>A. For each orocess v</li> </ul>	outfall, pro vastewater	vide a description of (1) All	l operations contributing	g wastewater to the effluent, including ter runoff; (2) The average flow contrib-
uted by e if necess	each opera	tion; and (3) The treatment	t received by the waste	ewater. Continue on additional sheets
Outfall Number	1. C	perations Contributing Flow (list)	2. Average Flow (include units)	3. Treatment (Description or List Codes from Table 2D-1)
03A	Ground-wat	ter from "clay pipe" at e of property	2,880 gpd	Low-profile air stripper
03A	Oil skimme	er pond overflow	33,120 gpd	Low-profile air stripper
		TOTAL	36,000 gpd	

C. Except season			spills, will any of		s described in ite	m III-A be interr	mittent or
L	☐ Yes (complete	te the following ta		o (go to item IV) quency	1		
	Outfall Number		a. Days Per Week (specify average)	b. Months Per Year (specify average)	a. Maximum Daily Flow Rate (in mgd)	2. Flow b. Maximum Total Volume (specify with units)	c. Ouration
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•							. 900
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actual produ	applicable produ	desian), expressa	ed in the terms and	lunits used in the a	fall list the estimated applicable effluent g rnative estimates (at	ruideline or NSPS, f	for each of th
					-		

		ļ			
	i,				
CONTINUED FROM THE FRONT		EPA ID Number (co	opy from Item 1 of F	orm 1)	Outfall Number
		NYD 002230977			03A
V. Effluent Characteristics				17.5	
he discharged from each	of your out	tfalls. Each part o the specific insti	of this item addre ructions for that	esses a	ntration and mass) of the pollutants to different set of pollutants and should data for each outfall should be on a
the source of information	uests you t n. Data for y. For all ou e present o	o provide an esti all pollutants in ( itfalls, data for p r are limited dire	mated daily max Group A, for all o pollutants in Gro	utfalls, un B sh	and average for certain pollutants and must be submitted unless waived by nould be reported only for pollutants ations guideline or NSPS or indirectly
1. Pollutant		2. Maximum Daily Value (include units)	3. Average Daily Value (include units)		4. Source (see instructions)
Flow		216,000 gpd	36,000 gpd	1	(Engineering Study)
Trichlorethylene		1.9 mg/l	0.87 mg/1	1	(Engineering Study)
		<u> </u>			

1. Politiani	(include units)	(include units)	
Flow	216,000 gpd	36,000 gpd	1 (Engineering Study)
Trichlorethylene	1.9 mg/l	0.87 mg/1	1 (Engineering Study)
	3.4 #/d	0.26 #/d	1 (Engineering Study)
Cis-1,2-dichloroethylene	0.34 mg/l	0.12 mg/l	1 (Engineering Study)
	0.61 #/d	0.036 #/d	1 (Engineering Study)
trans-1,2-dichloroethylehe	0.1 mg/l	0.05 mg/1	1 (Engineering Study)
	0.18 #/d	0.015 #/d	1 (Engineering Study)
Vinyl Chloride	0.02 mg/1	0.01 mg/l	1 (Engineering Study)
	0.036 #/d	0.003 #/d	1 (Engineering Study)
A waiver is requested for all			
additional parameters since the			
two sources currently discharge			
to surface water and the proposed			
treatment system is not designed			
to treat any other parameter beyon	nd		
those listed above.			Ì

CON	TINUED FROM THE FRONT	EPA ID Number (copy from Item 1 of Form 1) NYD 002230977	
C.	Use the space below to list any of reason to believe will be discharge believe it will be present.	the pollutants listed in Table 2D-3 of the instrued from any outfall. For every pollutant you list, b	ctions which you know or have priefly describe the reasons you
1. Pc	ollutant	2. Reason for Discharge	
Non			
	The state of the s		
	the second secon		
	•	••• •••	e e e e e e e e e e e e e e e e e e e
		to the way of the second of th	er en
V	Engineering Report on Wastewater Treats	ment	
Δ.	If there is any technical evaluation concappropriate box below.	erning your wastewater treatment, including engineering	reports or pilot plant studies, check the
8.	Provide the name and location production facility with respect t	of any existing plant(s) which, to the best of y o production processes, wastewater constituent	our knowledge, resembles this ts, or wastewater treatments.
	Name	Location	
N	lone		en la companya de la La companya de la co
			e en la menta de la la la companya de la companya d
	e e e e e e e e e e e e e e e e e e e		
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	<ul> <li>A section of the sectio</li></ul>	The first term of the second o	бол бол от не передости от объекто от мене од от организация <b>ния на</b> със

EPA ID Number (copy from item one of Form 1)

NYD 002230977

	ormation	

Use the space below to expand upon any of the above questions or to bring to the attention of the reviewer any other information you feel should be considered in establishing permit limitations for the proposed facility. Attach additional sheets if necessary.

The permit limitations for Oufall O3A should be established based on the New York State Department of Environmental Conservation Division of Water Best Available Technology Economically Achievable (BAT) Guidance.

#### VIII. Certification

I certify under penalty of law that this document and all attachments were prepared under my direction or supervision in accordance with a system designed to assure that qualified personnel properly gather and evaluate the information submitted. Based on my inquiry of the person or persons who manage the system, or those persons directly responsible for gathering the information, the information submitted is, to the best of my knowledge and belief, true, accurate, and complete. I am aware that there are significant penalties for submitting false information, including the possibility of fine and imprisonment for knowing violations.

A. Name and Official Title (type or print)	B. Phone No.
David L. Rosbrook, Senior Vice President	(315) 792-2710
C. Signature	D. Date Signed
David & Rorbrook	12 oct 94

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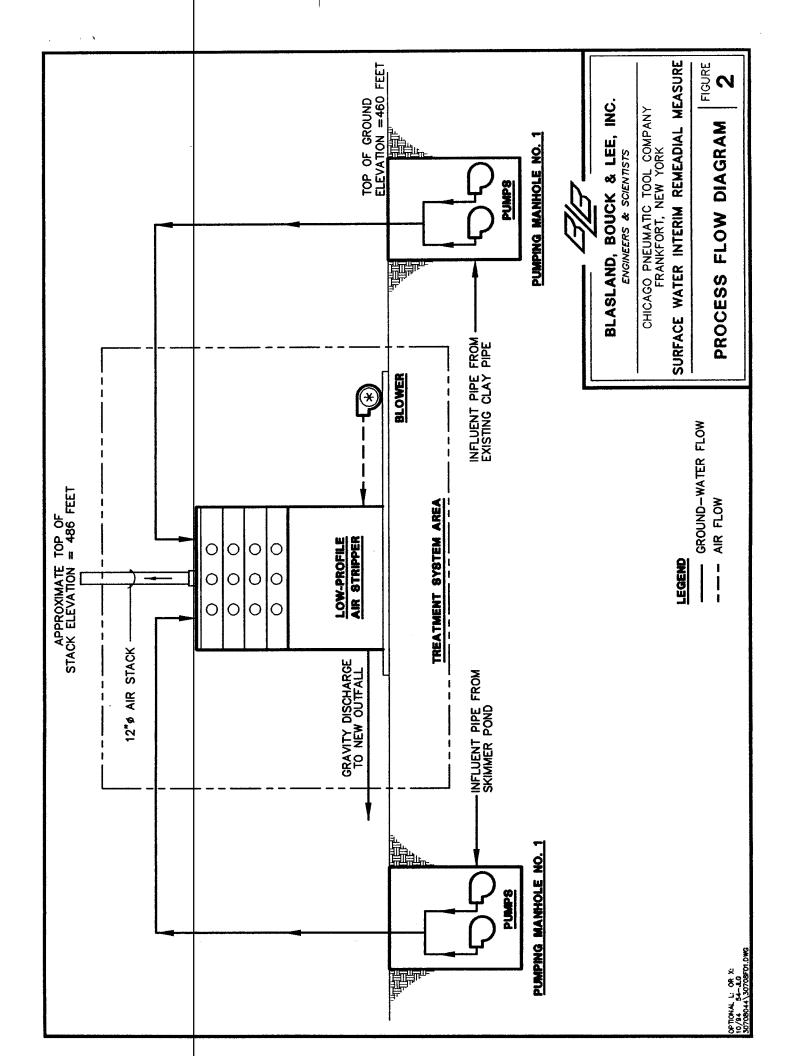
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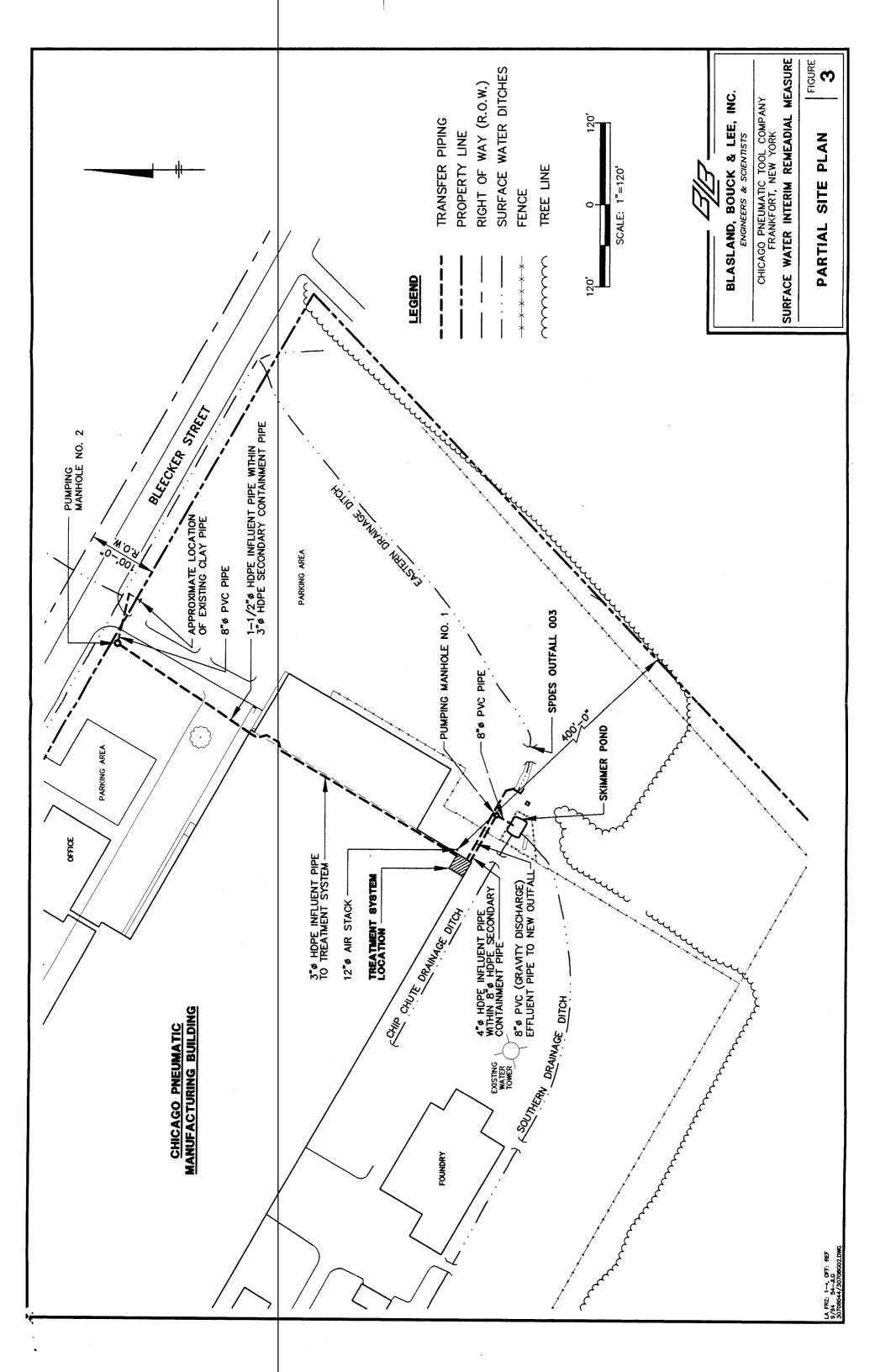
ENGINEERS & SCIENTISTS



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## 1.0 - Introduction



This Engineering Report presents the basis of design for a proposed surface water Interim Remedial Measure (IRM) to address volatile organic compounds (VOCs) in the surface water discharge from the Chicago Pneumatic Tool Company Site (the Site) in Frankfort, New York (see Figure 1 for a site location map). In a July 1994 Remedial Investigation (RI) Report, Blasland, Bouck & Lee, Inc. (BB&L) presented the results of RI activities performed at the Chicago Pneumatic Site from November 1993 to April 1994. The results of these RI activities and previous site investigations identified elevated concentrations of VOCs, principally trichlordethene and 1,2-dichloroethene, in selected areas at the Site. Additionally, elevated concentrations of VOCs, specifically trichloroethene, cis-1,2-dichloroethene, trans-1,2-dichloroethene, and vinyl chloride, have been detected in surface water from the oil skimmer pond overflow that discharges through State Pollutant Discharge Elimination System (SPDES)-permitted Outfall 003 and a clay pipe that discharges to a surface water ditch along Bleecker Street. A Feasibility Study (FS) is underway to select an overall site remediation program. The IRM covered by this Engineering Report will address the discharge of VOCs to surface water and consist of pumping water from the oil skimmer pond overflow and the clay pipe discharge to a low-profile air stripper located in the existing Chicago Pneumatic manufacturing building (see Figure 2 for process flow diagram). The locations of these proposed facilities are shown on the partial site plan on Figure 3.

The remainder of this Engineering Report presents an overview of site background information and a discussion of existing site data utilized to develop a basis of design for the surface water IRM. This document also presents a description of the surface water treatment system components and a discussion of the specific activities to be completed during implementation of the IRM.

# 2.0 - Background



#### 2.1 Site History

The Chicago Pneumatic Site is located in the town of Frankfort, Herkimer County, approximately one mile east of the City of Utica, New York, and 0.5 miles south of the Mohawk River. The Site is situated on a 77-acre lot in an industrial setting, which is bound to the north by Bleecker Street, to the south by wooded and agricultural land, to the west by an unnamed creek that drains a wooded area, and to the east by a property fence line bordering Industrial Park Drive. During the 1930s and early 1940s, the Site was occupied by an amusement park and baseball field. The amusement park was located in an area to the south of the current manufacturing building. The former baseball field is thought to be located near the southeast portion of the manufacturing building, and the flagpole for the former baseball field still stands at the Site.

The manufacturing building was constructed in 1948 and has since been used as a pneumatic tool manufacturing facility. A circa 1948-49 aerial photograph of the Site shows the manufacturing building, foundry, and power plant. In this time period, railroad tracks ran along the south and east side of the building, and a spur originated behind the power plant building and connected to another spur near the existing oil skimmer pond. Drainage ditches were evident along the entire southern edges of both spurs. During the early 1970s, a connecting warehouse was constructed to the east of the existing manufacturing building.

Waste oils were discharged into three unlined separation ponds located in the southern portion of the Site from 1966 through 1978. Waste oil from a metal chip handling facility was collected in an underground steel holding tank located within a pump house adjacent to the former chip handling area. Waste oil and water were then pumped to the first of the three separation ponds. The water and oil were allowed to discharge to the next pond in series, then ultimately to the drainage ditch located on the east side of the site. Each



pond provided a degree of oil/water separation. When the ponds became filled with oil, the oil was pumped off and either disposed of off-site or burned as fuel in the power plant.

In 1979, this practice was discontinued, and the New York State Department of Environmental Conservation (NYSDEC) granted Chicago Pneumatics permission to close the three separation ponds. The waste oils were removed from the ponds and disposed of off-site, and the ponds were backfilled. The steel holding tank and pump house were also dismantled. A new oil skimmer pond was constructed near the southeast corner of the manufacturing building to intercept any spillage from the metal chip handling area.

Metal chips from the manufacturing process were continued to be stored in a chip chute located along the south side of the manufacturing building until this system was eliminated in 1991. The spent chips were centrifuged prior to storage in the chip chute and removal off-site for recycling; however, some oil remained attached to the chips. Occasionally, this oil drained from the former chip chute and was discharged to the drainage ditch that drains to the oil skimmer pond. A similar drainage ditch receives surface water runoff from the area north of the former separation pond area. A rope-type oil skimmer removes oil from the surface of the oil skimmer pond. From the oil skimmer pond, water overflows through four overflow pipes to a diversion structure where it is discharged to a drainage ditch that runs along the east side of the Site. In addition to the oil skimmer pond overflow, this drainage ditch receives discharges from roof drains from a portion of the manufacturing building, floor drains inside of the warehouse to the east of the manufacturing building and a trench drain located east of the warehouse exterior loading docks. These four streams combine together and discharge through a SPDES-permitted discharge designated as Outfall 003 (SPDES Permit Number NY-0108537).

### 2.2 Investigation History

Over the last nine years, there have been a number of Site investigations that ultimately resulted in identification of the oil skimmer pond overflow and the clay pipe discharge as sources of VOCs in the