

## Monthly Progress Report 2023 No. 6

Former NuHart West Site
10-14 Clay Street, 55-57 Dupont Street & 280 Franklin Street, Brooklyn, NY
NYSDEC Site No. 224136
Reporting Period: June 1, 2023 – July 1, 2023

#### 1. Introduction

In accordance with the reporting requirements for the Former NuHart West Site, located at 10-14 Clay Street, 55-57 Dupont Street & 280 Franklin Street, Brooklyn, NY (Site), Haley & Aldrich of New York (Haley & Aldrich), has prepared this monthly progress report, on behalf of Dupont Street Owner LLC, to summarize the work performed at the Site from June 1 through July 1, 2023.

The Former NuHart West Site is located in the Greenpoint neighborhood of Brooklyn, NY and is identified as Block 2487 Lots 1, 10, 12, 72, and 78 on the New York City tax map. The Site is listed in the New York State Department of Environmental Conservation (NYSDEC) Inactive Hazardous Waste Registry as a Class 2 Site (Site No. 224136). The Site is underlain by sub-grade footings, utility networks, closed underground storage tanks (USTs), and piping and trench systems. The USTs and trench systems were cleaned out and the USTs were closed in accordance with applicable regulations in 2006. Former industrial operations at the Site have impacted onsite and offsite soil and groundwater with phthalates and lubricating oil (Hecla oil), most likely released from the tank and piping/trench systems. Phthalates and a phthalate/oil mixture are present in soil and as a light non-aqueous-phase liquid (LNAPL) plume floating on the groundwater surface primarily beneath Lots 1, 10, and 78 of the Site and extending somewhat offsite to the southwest. Groundwater is encountered at approximately 8 to 10 feet below ground surface (ft bgs). Currently, the site is a vacant 49,000-square foot lot with a concrete slab on grade.

Resource Conservation and Recovery Act (RCRA) closure activities were completed at the Site in May 2022. Interim remedial measure (IRM) activities are no longer being conducted at the Site since the product recovery systems were decommissioned as part of the RCRA Closure. IRM activities concluded in February 2022. Eastern Environmental Solutions, Inc. (Eastern) previously conducted waste management activities for disposal of product from the IBC tanks at the Site. Prior to 2022, Eastern has transported and disposed an estimated 2,116 gallons of product at the CycleChem facility in Elizabeth, NJ as hazardous waste. In January 2022, ACV Environmental Services Inc. (ACV) transported and disposed a total of 2,529 gallons of product at the CycleChem facility in Elizabeth, NJ as hazardous waste.

## 2. Investigation or Remedial Actions Relative to the Site during this Reporting Period

- Installation of the off-site LNAPL recovery wells began on 5 June 2023 and was completed on 22 June 2023.
- Relocation of the negative pressure enclosure to the eastern portion of the Site began on
   12 June 2023 and will continue early into the coming reporting period.

### 3. Monthly On-Site and Off-Site Monitoring Well Gauging



Gauging of on-site and off-site monitoring wells associated with the Site was performed on 29 June 2023. Gauging results are included in the attached table. On-site wells are inaccessible due to construction activities. The wells that could not be accessed are identified in the attached figure.

Due to LNAPL identified in MW-24 in previous reporting periods, an absorbent sock (New Pig) remains installed in MW-24 and is inspected on a weekly basis and replaced periodically, as needed.

#### 4. Actions Relative to the Site Anticipated for the Next Reporting Period

- Begin remedy execution including removal of the slab and excavation and off-site disposal of soil on the eastern portion of the Site, under the negative pressure enclosure.
- Begin the full-scale LNAPL recovery demonstration test by recovering LNAPL from the offsite recovery wells.

## 5. Approved Activity Modifications (changes of work scope and/or schedule)

There have been no modifications to the work scope.

## 6. Results of Sampling, Testing and Other Relevant Data

Additional soil sampling for supplemental waste characterization was conducted at the Site on 16 June 2023 through 21 June 2023. Waste characterization analytical results have been presented in the Supplemental Contained-in Request 03 and in subsequent Contained-in requests.

#### 7. Deliverables Submitted During This Reporting Period

The OU-1 LNAPL Barrier Installation Summary Letter was resubmitted on 30 May 2023 and approved on 13 June 2023 addressing comments received from NYSDEC in the previous reporting period. A revised Request to Import was submitted to NYSDEC on 7 June 2023 to import 1,500 cubic yards of recycled concrete aggregate (RCA) from Clean Earth of Carteret and was approved by NYSDEC on 12 June 2023. The Supplemental Contained-in Request 03 was submitted to NYSDEC on 19 June 2023 and was approved on 21 June 2023. No other deliverables were submitted during this reporting period.

#### 8. Information Regarding Percentage of Completion

Installation of the OU-1 LNAPL barrier wall is complete.

# 9. <u>Unresolved Delays Encountered or Anticipated That May Affect the Schedule and</u> Mitigation Efforts

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None.

## 10. Community Participation (CP) Plan Activities during This Reporting Period

A Community Board Meeting to discuss the next steps in the remediation of the Site was held on 26 June 2023.

11. Activities Anticipated in Support of the CP Plan for the Next Reporting Period:

None.

12. Miscellaneous Information

None.

Table 1:

Attachment A: Apparent Thickness of LNAPL
Former NuHart Plastic Manufacturing Site, NYSDEC #224136

280 Franklin Street Brooklyn, NY

Readings taken 6/30/2023 between 7:45 am and 2:30 pm (high tide @ 7:20am and low tide @ 1:10pm) 1 of 2

|                     |                      | Donth   |         | Apparent Thickness of LNAI |           |            |          |        |        |        |        |         |        |        |        |        | NAPL (feet) |          |           |         |          |             |        |        | 7.20am and low tide @ 1.10pm) |           |             |           |        |          |            |             |        |               |          |             |           |        |        |          |          |               |           |              |          |              |                        |
|---------------------|----------------------|---------|---------|----------------------------|-----------|------------|----------|--------|--------|--------|--------|---------|--------|--------|--------|--------|-------------|----------|-----------|---------|----------|-------------|--------|--------|-------------------------------|-----------|-------------|-----------|--------|----------|------------|-------------|--------|---------------|----------|-------------|-----------|--------|--------|----------|----------|---------------|-----------|--------------|----------|--------------|------------------------|
| Well Number  MW – 4 | er Depth<br>Water (1 |         | t       |                            | 2023      |            |          | 1      |        |        |        |         |        | 2022   |        |        |             |          |           |         |          |             |        | 2021   | l                             |           |             |           |        |          |            | 2020        |        |               |          |             |           |        |        | 2019     |          |               |           |              |          |              | 2018                   |
|                     | water (              | (feet)  | Jun-23  | May-23                     | Apr-23 Ma | r-23 Feb-2 | 3 Jan-23 | Dec-22 | Nov-22 | Nov-22 | Oct-22 | Sept-22 | Aug-22 | Jul-22 | Jun-22 | May-22 | Apr-22 M    | Mar-22 I | eb-22 Jan | -22 Dec | c-21 Nov | v-21 Oct-21 | Sep-21 | Aug-21 | Jul-21                        | Jun-21 Ma | ay-21 Apr-2 | 21 Mar-21 | Nov-20 | Oct-20   | Jul-20 Jur | n-20 May-20 | Apr-20 | Mar-20 Feb-20 | 0 Jan-20 | Dec-19 Nov- | 19 Oct-19 | Sep-19 | Aug-19 | Jul-19 J | Jun-19 N | May-19 Apr-19 | Mar-19 Fe | eb-19 Jan-19 | Dec-18 O | ct-18 Jun-18 | May-18 Apr-18          |
| MW – 4              | ND*                  | * ND*   | ND*     | ND*                        | ND* N     | D* ND      | · ND*    | ND*    | ND*    | NA     | NA     | NA      | ND*    | ND*    | ND*    | ND*    | ND*         | ND*      | ND* N     | )* -    |          | - ND*       | ND*    | ND*    | ND*                           | ND* N     | ID* ND*     | * ND      | ND     | ND       | ND N       | ND ND       | ND     | ND ND*        | ND*      | ND* ND      | * ND*     | ND*    | ND     | ND*      | ND*      | ## ND*        | ND*       | ND* ND*      | ND*      | ND* 0.12     | 1.13 0.65              |
| MW – 5              | 12.24                | 4 9.82  | 2.42    | 2.80                       | 0.80 4    | 24 5.02    | 0.59     | 5.22   | 6.94   | NA     | NA     | NA      | 4.85   | 4.85   | 4.07   | 4.00   | 4.50        | 3.20     | 2.73 6.   | 38 3.   | 85 0.    | 71 4.27     | 2.17   | 3.52   | 0.78                          | 0.10 0    | 0.78        | 3 0.29    | 3.59   | 4.76     | 2.94 5.    | .43 3.71    | 4.18   | 4.46 4.21     | 3.44     | 4.47 4.6    | 1 5.65    | 5.18   | 1.30   | 3.73     | 5.15     | 2.89 2.46     | 2.26      | 3.28 2.62    | 2.83     | 4.12 1.66    | 1.83 2.77              |
| MW – 6              | 9.85                 | 9.37    | 0.48    | ND                         | ND N      | ID ND      | 0.74     | 0.99   | 1.55   | NA     | NA     | NA      | 2.63   | 3.20   | 3.36   | 3.01   | 3.05        | 1.65     | 2.55 2.   | 51 2.   | 71 2.    | 83 2.42     | 2.90   | 3.45   | 2.74                          | 3.17 0    | 0.28 3.03   | 3.18      | 3.00   | 2.78     | 2.48 0.    | .99 3.00    | 2.20   | 2.29 2.39     | 2.98     | 0.85 ##     | ##        | ##     | ##     | ##       | 0.50     | 2.35 ##       | ##        | ## ##        | ##       | ND 0.55      | 0.50 2.47              |
| MW – 7              | 13.58                | 8 9.36  | 4.22    | ND**                       | 3.7 4     | 40 4.85    | 3.17     | 1.42   | 3.17   | NA     | NA     | NA      | 0.40   | 1.10   | 3.35   | 2.13   | 2.82        | 1.00     | 1.00 2.   | )7 1.   | 59 0.    | .67 0.88    | 0.37   | 0.42   | 0.46                          | 2.26 0    | 0.54 1.76   | 5 1.28    | 1.15   | 1.56     | 2.10 3.    | .89 2.81    | 3.85   | 3.53 1.59     | 0.99     | 1.67 1.5    | 9 1.63    | 1.96   | 0.84   | 0.45     | 1.30     | 0.14 0.35     | 0.26      | 1.54 1.14    | 0.93     | J.54 1.89    | 1.99 1.80              |
| MW – 8              | 9.34                 | ND      | ND      | ND                         | ND N      | ID ND      | ND       | ND     | ND     | NA     | NA     | NA      | ND     | ND     | ND     | ND     | ND          | ND       | ND N      | D N     | ID N     | ID ND       | ND     | ND     | ND                            | ND 1      | ND ND       | ND        | ND     | ND       | ND N       | ND ND       | ND     | ND ND         | ND       | ND NI       | ND        | ND     | ND     | ND       | ND       | ND ND         | _         | ND ND        | ND ,     | ND ND        | ND ND                  |
| MW – 12             | 7.60                 | ) ND    | ND      | ND                         | ND N      | ID ND      | ND       | ND     | ND     | ND     | ND     | ND      | ND     | ND     | ND     | ND     | ND          | ND       | ND N      | D N     | ID N     | ID ND       | ND     | ND     | ND                            | ND 1      | ND ND       | ND        | ND     | ND       | ND N       | ND ND       | ND     | ND ND         | ND       | ND NI       | ND        | ND     | ND     | ND       | ND       | ND ND         | ND        | ND ND        | ND ,     | ND ND        | ND ND                  |
| MW – 13             | 7.99                 | ) ND    | ND      | ND                         | ND N      | ID ND      | ND       | ND     | ND     | ND     | ND     | ND      | ND     | ND     | ND     | ND     | ND          | ND       | ND N      | D N     | ID N     | ID ND       | ND     | ND     | ND                            | ND 1      | ND ND       | ND        | ND     | ND       | ND N       | ND ND       | ND     | ND ND         | ND       | ND NI       | ND ND     | ND     | ND     | ND       | ND       | ND ND         | ND        | ND ND        | ND ,     | ND ND        | ND ND                  |
| MW – 14             | 9.25                 | 5 ND    | ND      | ND                         | ND N      | ID ND      | ND       | ND     | ND     | ND     | ND     | ND      | ND     | ND     | ND     | ND     | ND          | ND       | ND N      | D N     | ID N     | ID ND       | ND     | ND     | ND                            | ND 1      | ND ND       | ND        | ND     | ND       | ND N       | ND ND       | ND     | ND ND         | ND       | ND NI       | ND        | ND     | ND     | ND       | ND       | ND ND         | ND        | ND ND        | ND ,     | ND ND        | ND ND                  |
| MW – 15             | 12.3                 | 5 10.88 | 1.47    | NA                         | NA 0      | .26 0.53   | 1.27     | 1.76   | 2.36   | NA     | NA     | NA      | 0.85   | 1.30   | 0.85   | 1.30   | 3.05        | 4.43     | 0.38 1.   | )4 1.   | 05 0.    | .10 0.48    | 0.38   | 0.83   | 0.46                          | 0.57 0    | 0.61 2.44   | 4.46      | 0.29   | 1.30     | 1.00 3.    | .13 2.36    | 2.75   | 3.29 2.66     | 0.83     | 0.85 1.0    | 3 1.99    | 0.18   | 0.03   | 0.11     | 0.87     | 0.08 0.08     | 1.08      | 1.00 0.84    | 0.26     | J.12 0.04    | 0.04 0.07              |
| MW – 16             | 16.2                 | 7 11.44 | 4.83    | 3.90                       | 2.70 0    | .11 2.71   | 3.47     | 0.47   | 0.15   | NA     | NA     | NA      | 0.1    | ND     | 0.02   | 0.40   | 0.58        | 0.03     | 0.20 0.   | 56 0.   | 12 0.    | .14 0.17    | 0.29   | 0.63   | 0.10                          | 1.59 1    | .17 1.80    | 0.04      | 0.35   | 0.85     | 0.85 0.    | .41 0.22    | 0.84   | 0.36 ND       | ND       | ND 1.9      | 5 0.56    | 0.81   | 0.01   | 0.04     | 1.17     | 0.45 0.73     | 0.07      | 0.39 0.17    | 0.19     | J.20 0.06    | 0.10 0.13              |
| MW – 20             | 11.14                | 4 ND    | ND      | 0.70                       | 2.50 2    | 05 2.25    | 1.41     | 3.66   | 2.69   | 2.36   | 2.80   | 2.73    | 3.1    | 3.05   | 2.61   | 2.60   | 2.61        | 2.02     | 3.22 2.   | 29 1.   | 78 2.    | 78 2.36     | 3.03   | 3.05   | 2.95                          | 3.08 2    | 2.06 2.71   | 1.09      | 2.66   | 3.71     | 1.23 2.    | .92 2.91    | 1.01   | 3.12 2.18     | 2.75     | 2.82 3.7    | 3.37      | 3.25   | 2.29   | 2.09     | 3.66     | 1.45 1.47     | 2.17      | 2.43 2.77    | 3.49     | 2.51 1.4     | 1.55 2.52              |
| MW – 21             | NA                   | . NA    | NA      | NA                         | NA 1      | IA NA      | NA       | NA     | NA     | NA     | NA     | NA      | 0.95   | 1.90   | 1.54   | 1.40   | 2.09        | 2.68     | 0.75 0.   | 36 1.   | 60 1.    | .15 2.45    | 0.05   | 0.35   | 1.39                          | 1.33 1    | .06 1.91    | 2.61      | 1.33   | 3.13     | 2.98 5.    | .44 4.29    | 4.29   | 4.57 3.63     | 1.11     | 2.88 3.0    | 7 3.13    | 1.99   | 1.51   | 1.41     | 1.84     | 0.52 1.25     | 1.01      | 1.57 1.48    | 2.81     | 1.73 1.43    | 1.42 1.62              |
| MW – 22             | NA                   | . NA    | NA      | NA                         | NA 1      | NA NA      | 1.23     | 1.15   | ND*    | NA     | NA     | NA      | 0.78   | 1.20   | 5.13   | 1.30   | 1.55        | ND*      | ND* 0.    | 58 -    |          | - 0.93      | 0.11   | 0.86   | 1.13                          | 1.62 0    | 0.99        | 0.45      | 0.37   | 1.95     | 0.76 2.    | .56 2.13    | 1.54   | 1.55 1.59     | 1.44     | 1.22 1.0    | 5 1.94    | 2.95   | 0.69   | 0.51     | 2.28     | 2.98 1.03     | 1.05      | 1.83 1.68    | 0.83     | J.69 0.97    | 0.89 0.76              |
| MW – 23             | 11.73                | 3 ND    | ND      | ND                         | ND N      | ID ND      | ND       | ND     | ND     | ND     | ND     | ND      | ND     | ND     | ND     | ND     | ND          | ND       | ND N      | D N     | ID N     | ID ND       | ND     | ND     | ND                            | ND 1      | ND ND       | ND        | ND     | ND       | ND N       | ND ND       | ND     | ND ND         | ND       | ND NI       | ND        | ND     | ND     | ND       | ND       | ND ND         | ND        | ND ND        | ND ,     | ND ND        | ND ND                  |
| MW – 24             | 10.9                 | 4 ND**  | * ND*** | ND***                      | ND*** 0   | 0.08       | NA       | NA     | ND     | ND     | ND     | ND      | ND     | ND     | ND     | ND     | ND          | ND       | ND N      | D N     | ID N     | ID ND       | ND     | ND     | ND                            | ND 1      | ND ND       | ND        | ND     | ND       | ND N       | ND ND       | ND     | ND ND         | ND       | ND NI       | ND ND     | ND     | ND     | ND       | ND       | ND ND         | ND        | ND ND        | ND ,     | ND ND        | ND ND                  |
| MW – 25             | 11.9                 | 1 10.81 | 1.10    | 1.30                       | 3.60 4    | 02 3.72    | 3.23     | 3.06   | 2.86   | 3.83   | 4.71   | 4.51    | 4.5    | 4.55   | 5.87   | 4.20   | 4.44        | 3.87     | 3.29 3.   | 78 3.   | 52 4.    | 49 3.78     | 3.81   | 3.90   | 3.08                          | 4.37 3    | 3.63 3.81   | 3.24      | 3.28   | 4.35     | 4.23 3.    | .68 0.98    | 3.79   | 6.72 4.57     | 4.89     | 4.66 4.9    | 3 4.31    | 3.18   | 3.38   | 3.83     | 4.61     | 3.76 3.81     | 4.19      | 4.77 3.86    | 3.89     | 3.44 2.85    | 2.89 4.03              |
| MW – 26             | 11.6                 | 5 10.84 | 0.81    | 1.45                       | 0.61 4    | 00 4.93    | 0.61     | 4.09   | 4.01   | 3.76   | 4.84   | 3.78    | 3.4    | 3.50   | 4.02   | 3.40   | 4.39        | 3.02     | 1.90 4.   | 15 3.   | 24 3.    | 44 2.89     | 7.14   | 3.58   | 3.07                          | 4.01 3    | 3.02 3.32   | 3.32      | 2.97   | 3.56     | 3.79 3.    | .78 3.71    | 3.47   | 4.13 4.14     | 4.11     | 4.65 4.0    | 2 4.62    | 5.21   | 3.43   | 3.19     | 4.90     | 0.69 2.46     | 2.94      | 3.37 3.14    | 3.84     | 3.45 0.75    | 2.35 3.14              |
| MW – 27             | 11.13                | 8 ND    | ND      | ND                         | ND N      | ID ND      | ND       | ND     | ND*    | ND     | ND     | ND      | ND     | ND     | ND     | ND     | ND          | ND       | ND N      | D N     | ID N     | ID ND       | ND     | ND     | ND                            | ND 1      | ND ND       | ND        | ND     | ND       | ND N       | ND ND       | ND     | ND ND         | ND       | ND NI       | ND ND     | ND     | ND     | ND       | ND       | ND ND         | ND        | ND ND        | ND 7     | ND ND        | ND ND                  |
| MW – 28             | 11.5                 | 1 ND    | ND      | ND                         | ND N      | ID ND      | ND       | ND     | ND     | ND     | ND     | ND      | ND     | ND     | ND     | ND     | ND          | ND       | ND N      | D N     | ID N     | ID ND       | ND     | ND     | ND                            | ND 1      | ND ND       | ND        | ND     | ND       | ND N       | ND ND       | ND     | ND ND         | ND       | ND NI       | ND ND     | ND     | ND     | ND       | ND       | ND ND         | ND        | ND ND        | ND 7     | ND ND        | ND ND                  |
| MW – 29             | 11.4                 | 6 ND    | ND      | ND                         | ND N      | ID ND      | ND       | ND     | ND     | ND     | ND     | ND      | ND     | ND     | ND     | ND     | ND          | ND       | ND N      | D N     | ID N     | ID ND       | ND     | ND     | ND                            | ND 1      | ND ND       | ND        | ND     | ND       | ND N       | ND ND       | ND     | ND ND         | ND       | ND NI       | ND ND     | ND     | ND     | ND       | ND       | ND ND         | ND        | ND ND        | ND 7     | ND ND        | ND ND                  |
| MW – 30             | 10.43                | 2 ND    | ND      | ND                         | ND N      | ID ND      | ND       | ND     | ND     | ND     | ND     | ND      | ND     | ND     | ND     | ND     | ND          | ND       | ND N      | D N     | ID N     | ID ND       | ND     | ND     | ND                            | ND 1      | ND ND       | ND        | ND     | ND       | ND N       | ND ND       | ND     | ND ND         | ND       | ND NI       | ND ND     | ND     | ND     | ND       | ND       | ND ND         | ND        | ND ND        | ND 7     | ND ND        | ND ND                  |
| MW – 31             | 9.73                 | ND ND   | ND      | ND                         | ND N      | ID ND      | ND       | ND     | ND     | ND     | ND     | ND      | ND     | ND     | ND     | ND     | ND          | ND       | ND N      | D N     | ID N     | ID ND       | ND     | ND     | ND                            | ND 1      | ND ND       | ND        | ND     | ND       | ND N       | ND ND       | ND     | ND ND         | ND       | ND NI       | ND ND     | ND     | ND     | ND       | ND       | ND ND         | ND        | ND ND        | ND 7     | ND ND        | ND ND                  |
| MW – 32             | 10.4                 | 1 ND    | ND      | ND                         | ND N      | ID ND      | ND       | ND     | ND     | ND     | ND     | ND      | ND     | ND     | ND     | ND     | ND          | ND       | ND N      | D N     | ID N     | ID ND       | ND     | ND     | ND                            | ND 1      | ND ND       | ND        | ND     | ND       | ND N       | ND ND       | ND     | ND ND         | ND       | ND NI       | ND ND     | ND     | ND     | ND       | ND       | ND ND         | ND        | ND ND        | ND 7     | ND ND        | ND ND                  |
| MW – 34             | NA                   | NA NA   | NA      | NA                         | ND 1      | NA NA      | ND       | NA     | NA     | NA     | NA     | NA      | ND     | ND     | ND     | ND     | ND          | ND       | ND N      | D -     |          | - ND        | ND     | ND     | ND                            | ND 1      | ND ND       | ND        | ND     | ND       | ND N       | ND ND       | ND     | ND ND         | ND       | ND NI       | ND ND     | ND     | ND     | ND       | ND       | ND ND         | ND        | ND ND        | ND 7     | ND ND        | ND ND                  |
| MW – 35             | NA                   | NA NA   | NA      | NA                         | ND N      | ID ND      | ND       | ND     | ND     | NA     | NA     | NA      | ND     | ND     | ND     | ND     | ND          | ND       | ND N      | D -     |          | - ND        | ND     | ND     | ND                            | ND 1      | ND ND       | ND        | ND     | ND       | ND N       | ND ND       | ND     | ND ND         | ND       | ND NI       | ND ND     | ND     | ND     | ND       | ND       | ND ND         | ND        | ND ND        | ND '     | ND ND        | ND ND                  |
| MW – 36             | 11.2                 | 1 ND    | ND      | ND                         | ND N      | ID ND      | ND       | ND     | ND     | ND     | ND     | ND      | ND     | ND     | ND     | ND     | ND          | ND       | ND N      | D N     | ID N     | ID ND       | ND     | ND     | ND                            | ND 1      | ND ND       | ND        | ND     | ND       | ND N       | ND ND       | ND     | ND ND         | ND       | ND NI       | ND ND     | ND     | ND     | ND       | ND       | ND ND         | ND        | ND ND        | ND 7     | ND ND        | ND ND                  |
| MW – 37             | 11.6                 | 4 ND    | ND      | ND                         | ND N      | ID ND      | ND*      | ND*    | ND*    | ND*    | ND     | ND      | ND     | ND     | ND     | ND     | ND          | ND       | ND N      | D N     | ID N     | ID ND       | ND     | ND     | ND                            | ND 1      | ND ND       | ND        | ND     | ND       | ND N       | D* ND       | ND     | ND ND         | ND       | ND NI       | ND        | ND     | ND     | ND       | ND       | ND ND         | ND        | ND ND        | ND N     | ID* ND       | ND ND                  |
| MW – 38             | 10.23                | 2 ND    | ND      | ND                         | ND N      | ID ND      | ND       | ND     | ND     | ND     | ND     | ND      | ND     | ND     | ND     | ND     | ND          | ND       | ND N      | D N     | ID N     | ID ND       | ND     | ND     | ND                            | ND 1      | ND ND       | ND        | ND     | ND       | ND N       | ND ND       | ND     | ND ND         | ND       | ND NI       | ND ND     | ND     | ND     | ND       | ND       | ND ND         | ND        | ND ND        | ND !     | ND ND        | ND ND                  |
| MW – 39             | 8.38                 | ND ND   | ND      | ND                         | ND N      | ID ND      | ND       | ND     | ND     | ND     | ND     | ND      | ND     | ND     | ND     | ND     | ND          | ND       | ND N      | D N     | ID N     | ID ND       | ND     | ND     | ND                            | ND 1      | ND ND       | ND        | ND     | ND       | ND N       | ND ND       | ND     | ND ND         | ND       | ND NI       | ND ND     | ND     | ND     | ND       | ND       | ND ND         | ND        | ND ND        | ND !     | ND ND        | ND ND                  |
| MW – 40             | NA                   | . NA    | NA      | NA                         | NA N      | IA ND      | ND       | ND     | ND     | NA     | NA     | NA      | ND     | ND     | _      | -      | ND          | ND       | ND -      | - N     | ID N     | ID ND       | ND     | ND     | ND                            | ND 1      | ND ND       | ND        | ND     | ND       | ND N       | ND ND       | ND     | ND ND         | ND       | ND NI       | ND ND     | ND     | ND     | ND       | ND       | ND ND         | ND        | ND ND        | ND !     | ND ND        | ND ND                  |
| MW – 41             | 10.3                 | 5 ND    | ND      | ND                         | ND N      | ID ND      | ND       | ND     | ND     | ND     | ND     | ND      | ND     | ND     | ND     | ND     | ND          | ND       | ND N      | D N     | ID N     | ID ND       | ND     | ND     | ND                            | ND 1      | ND ND       | _         | _      | _        |            | _   _       | _      | -   -         | _        |             | _         | _      | _      | -        | -        |               |           |              |          | — ND         | ND ND                  |
| MW – 42             | 9.64                 | ND ND   | ND      | ND                         | ND N      | ID ND      | ND       | ND     | ND     | ND     | ND     | ND      | ND     | ND     | ND     | ND     | ND          | ND       | ND N      | D N     | ID N     | ID ND       | ND     | ND     | ND                            | ND 1      | ND ND       | ND        | ND     | ND       | ND N       | ND ND       | ND     | ND ND         | ND       | ND NI       | ND ND     | ND     | ND     | ND       | ND       | ND ND         | ND        | ND ND        | ND* N    | ND* ND       | ND ND                  |
| MW - 45             | 11.13                | 2 ND    | ND      | ND                         | ND N      | ID -       | -        | -      | -      | -      | -      | -       | -      | -      | -      | -      | -           | -        | -   -     | .   .   | -   .    | -   -       | -      | -      | -                             | -         | -   -       | -         | -      | -        | -          | -   -       | -      | -   -         | -        | -   -       | -         | -      | -      | -        | -        | -   - '       | -         | -   -        |          | -   -        | 1 -   -                |
| MW - 46             | 11.5                 | 5 ND    | ND      | ND                         | ND N      | ID -       | -        | -      | -      | -      | -      | -       | -      | -      | -      | -      | -           | -        | -         |         | -   '    | -   -       | -      | -      | -                             | -         |             | -         | -      | -        | -          |             | -      |               | -        |             | -         | -      | -      | -        | -        | - '           | -         |              | · -      |              |                        |
| MW - 47             | 11.10                | 0 ND    | ND      | ND                         | ND N      | ID -       | -        | -      | -      | -      | -      | -       | -      | -      | -      | -      | -           | -        | -         |         | -   .    |             | -      | -      | -                             | -         |             | -         | -      | -        | -          |             | -      |               | -        |             | -         | -      | -      | -        | -        | -   - '       | -         |              | · -      |              |                        |
| MW-A                | NA                   | . NA    | NA      | NA                         | 0.05 0    | 0.05       | 4.45     | -      | -      | -      | -      | -       | -      | -      | -      | -      | -           | -        | -         |         | -        |             | -      | -      | -                             | -         |             | -         | -      | -        | -          |             | -      |               | -        |             | -         | -      | -      | -        | -        |               | -         |              |          |              |                        |
| RW – 1              | NA                   | . NA    | NA      | NA                         | NA N      | NA NA      | NA       | NA     | NA     | NA     | NA     | NA      | ND     | ND     | ND     | ND     | ND          | ND       | ND N      | D N     | ID N     | ID ND       | ND     | ND     | ND                            | ND 1      | ND ND       | ND        | ND     | ND       | ND N       | ND ND       | ND     | ND ND         | ND       | ND NI       | ND ND     | ND     | ND     | ND       | ND       | ND ND         | ND        | ND ND        | ND !     | ND ND        | ND ND                  |
| RW-2                | NA                   | . NA    | NA      | NA                         | NA N      | NA NA      | NA       | 3.16   | 4.55   | NA     | NA     | NA      | 3.45   | 3.10   | 5.67   | 3.39   | 5.78        | 5.25     | 3.15 5.   | 19 3.   | 03 2.    | .11 2.00    | 2.16   | 2.12   | 2.92                          | 02.15 1   | .74 3.28    | 3 2.44    | 3.81   | 2.90     | 3.95 4.    | .56 3.25    | 4.93   | 4.78 4.59     | 3.31     | 4.49 2.4    | 5.03      | 2.19   | 1.41   | 0.66     | 4.08     | 1.64 1.47     | 1.27      | 4.73 5.12    | 1.63     | 0.06         | 0.08 1.65              |
| RW – 3              | NA                   | . NA    |         | NA                         |           | NA NA      |          |        | 2.51   | NA     | NA     |         |        | 3.40   |        |        |             |          |           | 20 0.   |          |             | 2.60   |        |                               | 05.02 1   |             |           |        |          |            |             |        |               |          | 2.62 4.3    | 4.03      | 4.09   | 3.50   | 3.25     | 3.96     | 1.61 2.11     | 2.26 4    | 4.71 2.22    | 2.63     | 3.77 2.08    | 2.03 2.52              |
| RW – 4              | NA                   | . NA    | NA      | NA                         | NA N      | NA NA      | 0.40     | 2.18   | 1.53   | NA     | NA     | NA      | 3.23   | 4.40   | 4.97   | 4.01   | 4.40        | 2.97     | 3.13 1.   | 92 2.   | 89 3.    | 50 3.17     | 0.86   | 4.35   | 4.52                          | 03.87 2   | 2.64 4.35   | 3.69      | 3.23   | 2.99     | 3.94 3.    | .35 2.92    | 3.55   | 2.46 3.78     | 2.64     | 3.02 4.1    | 5 ##      | 4.21   | 3.56   | 3.07     | 4.72     | 1.13 0.53     | 2.85      | ## ##        | 03.37 7  | 2.85 2.96    | 2.97 3.80<br>0.33 0.65 |
| RW – 5              | NA                   | . NA    |         |                            | NA N      |            |          | 3.47   |        | NA     |        |         |        |        | 5.02   |        |             |          |           |         |          | 81 3.80     |        |        |                               |           |             |           |        |          |            |             |        | 4.91 5.18     |          | ## ##       | ##        | 5.74   | ##     | ##       | ##       | 0.71 ##       | ##        | ## ##        | ## N     | √D* 0.44     | 0.33 0.65              |
| RW – 6              | NA                   | . NA    | NA      | NA                         | NA 1      | NA NA      | NA       | 0.40   | ND*    | NA     |        |         |        |        | 0.48   |        |             |          | 1.05 1.   | - 10    | - 0.     | 90 1.12     | 0.53   | 0.21   | 1.14                          | 1.33 0    | 0.58 2.49   | ##        | ##     | 2.82     | 1.85 2.    | .17 0.44    | 1.21   | 0.98 1.05     | 1.67     | 1.51 1.6    | 2.19      | 1.49   | 0.7    | 0.46     | 1.57     | 0.28 0.55     | 0.49 (    | 0.91         | 00.73    | .91 0.83     | 0.88 0.96<br>0.02 0.03 |
| RW – 8 **           | * NA                 | . NA    | NA      | NA                         | NA N      | NA NA      | 0.36     | 0.88   | 1.52   | NA     | NA     | NA      | 3.77   | 3.80   | 4.06   | 4.06   | 3.55        | 2.35     |           |         | -   -    | -   -       | _      | _      |                               |           |             |           |        | _        |            |             |        |               |          |             |           |        | _      |          |          |               |           |              |          |              | 0.02 0.03              |
| RW – 9              | NA                   | . NA    | NA      | NA                         | NA N      | NA NA      | 3.55     | 3.92   |        | NA     | NA     | NA      | 4.07   | 6.65   | 4.02   |        |             |          | 3.70 5.   | 97 4.   |          |             | 0.78   |        | 2.95                          | 3.65 3    | 3.42 4.39   | 5.42      | 6.45   |          |            | .90 4.65    |        | 5.01 5.36     |          |             | 7 5.59    |        |        | 3.55     | 4.57     | 2.32 1.73     |           |              |          | .52 0.11     | 2.38 2.28<br>1.60 3.70 |
| RW – 10             |                      | . NA    |         | NA                         | NA N      |            |          |        | 2.13   | NA     |        |         | 3      | 4.2    | 5.31   |        |             |          |           | 51 1.   |          | 95 3.04     |        |        |                               |           | 3.1 4.32    |           |        | 3.88     |            | .31 2.93    |        |               | 4.58     |             |           |        |        | 3.04     |          |               |           | 4.53 3.80    |          |              | 1.60 3.70              |
| RW – 11             |                      | . NA    |         |                            | NA N      |            |          | 2.48   |        | NA     |        |         | 4.1    | 4.9    | 3.48   |        |             |          | 2.85 0.   | 58 4.   | 78 4.    | 13 3.64     | 1.11   | 4.48   | 2.67                          | 6.11 2    | 2.00 4.20   | 1.43      | 3.25   | 4.24     | 3.45 3.    | .89 4.32    | 4.31   | 5.77 5.13     | 3.80     | 5.58 4.5    | 6.30      | 4.85   | 4.12   | 3.78     | 4.65     | 3.32 1.92     |           |              |          |              | 2.52 4.34              |
| RW- 12 **           | * NA                 | . NA    | NA      | NA                         | NA 1      | NA NA      | NA       | 5.42   | 6.10   | NA     | NA     | NA      | 4.17   |        | 7.02   | 3.86   | 3.30        | 3.50     |           | -   -   | _        | -   -       | _      | _      |                               |           |             | _         | _      | <u> </u> |            |             | _      | _   _         | _        |             | _         | _      |        | _        |          |               |           |              |          | - 0.11       |                        |
| MW - 1              |                      | NG      |         |                            | NG N      |            |          | NG     | _      | NG     | _      |         | NG     | NG     |        | NG     |             |          | NG N      | G N     |          | – NG        | _      |        |                               |           |             | _         | _      |          |            |             |        | NG NG         |          |             | _         |        |        |          |          | NG NG         |           |              |          |              | NG NG                  |
| MW - 9              | NG                   | NG      |         | NG                         | NG N      | IG NG      | NG       | NG     | NG     | NG     | NG     | NG      | NG     | NG     | NG     | NG     | NG          | NG       | NG N      | G N     | IG N     | ID NG       | NG     | NG     | NG                            | NG 1      | NG NG       | NG NG     | NG     | NG       | NG N       | NG NG       | NG     | NG NG         | NG       | NG NO       | G NG      | NG     | NG     | NG       |          |               |           | NG —         | NG N     | NG NG        | NG NG                  |
| MW - 10             | _                    | NG      |         | NG                         | NG N      |            |          |        |        | NG     | _      | _       | _      | NG     |        |        |             |          | NG N      |         |          | ID NG       |        |        | _                             |           |             |           | _      | NG       |            | NG NG       |        | NG NG         |          | NG NO       |           |        | NG     |          |          | NG NG         |           | NG ND        |          | NG NG        |                        |
| MW - 17             |                      | NG      |         | NG                         | NG N      |            |          |        |        | NG     | NG     | NG      | NG     | NG     | NG     |        | NG          | NG       | NG N      | G N     | IG N     | ID NG       | NG     | NG     |                               | NG 1      |             | NG NG     | NG     | NG       |            | NG NG       |        | NG NG         |          | NG NO       |           |        | NG     | NG       | NG       | NG NG         |           | NG ND        |          | NG NG        | NG NG                  |
| MW - 18             |                      | NG      |         |                            | NG N      |            |          |        | NG     | NG     |        |         | _      | NG     |        |        |             | NG       | N         | G N     | iG -     | – NG        | NG     | NG     |                               | NG 1      |             | NG NG     | NG     |          |            |             |        | NG NG         | _        |             |           |        |        |          |          | NG NG         |           |              |          |              |                        |
| RW - 7              | NG                   | NG      | NG      | NG                         | NG N      | IG NG      | NG       | NG     | NG     | NG     | NG     | NG      | NG     | NG     | NG     | NG     | NG          | NG       | NG N      | G N     | IG -     | – NG        | NG     | NG     | NG                            | NG 1      | NG NG       | NG        | NG     | NG       | NG N       | NG NG       | NG     | NG NG         | NG       | NG NO       | i NG      | NG     | NG     | NG       | NG       | NG NG         | NG        | NG —         | NG 1     | NG NG        | NG NG                  |

Notes:

Data recorded using an oil/water interface probe, measurements from the tops of well casings

NI = Not Installed ND = Not Detected NA= No Access

Wells MW-1, MW-2, MW-9, MW-10, MW-17, MW-18, MW-19, and RW-7 are associated with NYSDEC Spill 06-01852 and are under a separate investigation est= Estimated Value \*\* = Water not detected; well filled with sediment, value is the total depth of the well

\* = Well was dry

Wells MW-45, MW-46, and MW-47 installed on 13 March 2023

Wells were gauged on 30 June 2023

\*\*\*MW-24 absorbent sock installed

Haley Aldrich, Inc.

Attachment A: Apparent Thickness of LNAPL
Former NuHart Plastic Manufacturing Site, NYSDEC #224136
280 Franklin Street

Brooklyn, NY

|             | Dox            | th to       |          |            |          |        |        |          |           |          |           |         |            |          |        |          |          |         |                  |         |          |        |        |          |        |           |               |          |        |             |           |            |                  |           |              |                  |          |            |            |        |        |        |        |        |           |             |          |        |            |             |                |        |
|-------------|----------------|-------------|----------|------------|----------|--------|--------|----------|-----------|----------|-----------|---------|------------|----------|--------|----------|----------|---------|------------------|---------|----------|--------|--------|----------|--------|-----------|---------------|----------|--------|-------------|-----------|------------|------------------|-----------|--------------|------------------|----------|------------|------------|--------|--------|--------|--------|--------|-----------|-------------|----------|--------|------------|-------------|----------------|--------|
| Well Number | Depth to Pro   | duct        |          |            |          | 201    | 7      |          |           |          | 2017      | 7       |            |          |        |          |          |         | 016              |         |          |        |        |          |        |           |               | 2015     |        |             |           |            |                  |           |              | 2014             |          |            |            |        |        |        |        | 2013   |           |             |          |        |            | 2012        |                |        |
| l "         | ater (feet) (f | eet) Mar-18 | Feb-18 J | an-18 Nov- | 17 Oct-1 | Sep-17 | Aug-17 | Jul-17 J | Jun-17 Ma | ay-17 Ap | r-17 Mar- | 17 Feb- | -17 Jan-17 | 7 Dec-16 | Nov-16 | Oct-16 S | Sep-16 A | ug-16 J | ıl-16 Jun-1      | 6 May-1 | 6 Apr-16 | Mar-16 | Feb-16 | Jan-16   | Dec-15 | Nov-15 Oc | oct-15 Sep-15 | 5 Aug-15 | Jul-15 | 5 Jun-15 Ma | ay-15 Apr | r-15 Mar-1 | 15 Jan-15 S      | Sep-14 Au | ug-14 Jul-14 | Jun-14           | May-14 A | pr-14 Mar- | -14 Feb-14 | Jan-14 | Dec-13 | Nov-13 | Oct-13 | Sep-13 | Aug-13 Ju | ul-13 Apr-1 | 3 Mar-13 | Feb-13 | Jan-13 Dec | c-12 Nov-12 | 2 Oct-12       | Sep-12 |
| MW – 4      | ND* N          | D* 0.73     | ND*      | 0.92 2.1   | 2 0.81   | 1.76   | 1.73   | 1.23     | 1.77 N    | ND* 1.   | .32 1.6   | 1 1.13  | 13 1.31    | 1.30     | 1.00   | 1.18     | 1.35     | 1.71    | .73 1.80         | 1.53    | 1.73     | 1.43   | 1.85   | 1.77     | 1.96   | 2.04 1    | 1.99 1.77     | 2.22     | 4.27   | 0.35        | 0.44 -    | 0.56       | , –              | 1.75 1    | 1.90 1.24    | Trace            | _        | 0.01 Trac  | ce 0.23    | 0.22   | 0.30   | 0.66   | 0.78   | ##     | 3.49 2    | 2.22 0.59   | 0.67     | 0.44   | 0.44 0.    | 0.80 0.31   | 0.33           | 3.13   |
| MW – 5      | 12.24 9        | .82 2.19    | 2.21     | 4.65 5.8   | 3 2.19   | 4.44   | 4.4    | 3.71     | 3.54 2    | 2.81 2.  | 2.80 3.13 | 3 4.03  | 05 3.00    | 3.55     | 4.43   | 3.64     | 3.22     | 4.31    | 1.03 4.29        | 3.07    | 3.18     | 3.14   | 1.85   | 3.24     | 4.83   | 5.41 4    | 4.16 4.26     | 4.45     | 4.22   | 2.30 2      | 2.41 2.   | .55 3.10   | 4.40             | 4.79 5    | 5.03 1.97    | 3.39             | _        | 3.14 2.80  | 0 2.98     | _      | 6.46   | 7.17   | 5.54   | ##     | 5.08 3    | 3.92 3.00   | 2.39     | 4.32   | 3.00 4.    | .11 3.50    | 3.41           | 5.58   |
| MW – 6      | 9.85 9         | .37 0.74    | ##       | ## ##      | 1.22     | 3.19   | 3.15   | ##       | ##        | ## #     | ## ##     | ##      | # ##       | ##       | ##     | ##       | ##       | ##      | ## ##            | ##      | ##       | ##     | ##     | ##       | ##     | ##        | ## ##         | ##       | ##     | 2.30        | ## #      | ## ##      | ##               | ##        | ## ##        | ##               | -        | - 2.8      | 4 3.43     | _      | 2.89   | 2.76   | 2.00   | ##     | 2.42 2    | 2.82 —      | _        | - 1    |            |             | 3.49           | 2.14   |
| MW – 7      | 13.58 9        | .36 2.03    | 2.55     | 3.32 4.9   | 1 1.48   | 1.45   | 1.41   | 0.9      | 0.00      | 1.50 1.  | .92 2.53  | 3 3.7   | 71 1.28    | 0.78     | 1.73   | 0.91     | 0.04     | 1.89    | .58 2.22         | 2.11    | 1.90     | 1.66   | 2.31   | 2.47     | 3.44   | 3.31 2    | 2.58 1.46     | 1.28     | 0.99   | 1.58        | ND 1.     | .94 1.79   | ##               | 2.01 2    | 2.16 0.60    | 0.01             | -        | 0.17 0.1   | 7 —        | _      | 4.78   | 4.70   | 4.00   | ##     | 2.77 1    | 1.06 1.92   | 4.92     | 5.45   | 1.30 1.    | .36 2.00    | 1.84           | 1.83   |
| MW – 8      | 9.34 N         | ND ND       | ND       | ND NI      | ND ND    | ND     | ND     | ND       | ND 1      | ND N     | ND ND     | ) NE    | D ND       | ND       | ND     | ND       | ND       | ND      | ND ND            | ND      | ND       | ND     | ND     | ND       | ND     | ND 1      | ND ND         | ND       | ND     | ND 1        | ND N      | ND ND      | T - T            | ND N      | ND ND        | ND               | -        | ND NE      | ) –        | _      | ND     | ND     | ND     | ND     | ND 1      | ND ND       | ND       | ND     | ND N       | ND ND       | ND             | ND     |
| MW – 12     | 7.60 N         | ND ND       | ND       | ND NI      | ND ND    | ND     | ND     | ND       | ND I      | ND N     | ND ND     | ) NE    | D ND       | ND       | ND     | ND       | ND       | ND      | ND ND            | ND      | ND       | _      | _      | <u> </u> | ND     | ND        |               | _        | _      | ND 1        | ND N      | ND ND      | <u> </u>         | ND ·      | - ND         | ND               | _        | ND NE      | ) –        | _      | ND     | ND     | ND     | ND     | ND 1      | ND ND       | ND       | ND     | ND N       | ND ND       | ND             | ND     |
| MW – 13     | 7.99 N         | ND ND       | ND       | ND NI      | ) ND     | ND     | ND     | ND       | ND 1      | ND N     | ND ND     | ) NE    | D ND       | ND       | ND     | ND       | ND       | ND      | ND ND            | ND      | ND       | ND     | _      | _        | ND     | ND        |               | _        | _      | ND 1        | ND N      | ND ND      | <u> </u>         | ND ·      | - ND         | ND               | -        | ND NE      | ) –        | _      | ND     | ND     | ND     | ND     | ND 1      | ND ND       | ND       | ND     | ND N       | ND ND       | ND             | ND     |
| MW – 14     | 9.25 N         | ID ND       | ND       | ND NI      | ND ND    | ND     | ND     | ND       | ND 1      | ND N     | ND ND     | ) NE    | D ND       | ND       | ND     | ND       | ND       | ND      | ND ND            | ND      | ND       | ND     | ND     | ND       | ND     | ND 1      | ND ND         | ND       | ND     | ND 1        | ND N      | ND ND      | ND               | ND N      | ND ND        | ND               | _        | ND NE      | ) –        | _      | ND     | ND     | ND     | ND     | ND 1      | ND ND       | ND       | ND     | ND N       | ND ND       | ND             | ND     |
| MW – 15     | 12.35          | 0.88 0.07   | 0.08     | 3.16 1.7   | 3 0.31   | 0.29   | 0.26   | 0.26     | 0.24      | 0.12 0.  | 0.22 0.28 | 8 0.40  | 40 0.31    | 0.20     | 0.80   | 0.20     | 0.17     | 0.81    | 0.07 0.48        | 0.22    | 0.71     | 0.03   | 0.04   | 0.60     | 3.08   | 3.07 1    | 1.97 1.05     | 1.05     | ND     | 1.24        | 1.21 1.   | .56 1.67   | 1.71             | 2.19 2    | 2.32 ##      | 0.45             | _        | 0.61 0.3   | 0.38       | _      | 3.11   | 3.19   | 3.34   | ##     | 2.14      | 0.70 –      | 0.32     | 1.07   | - 1.       | .56 0.99    | 0.76           | 2.67   |
| MW – 16     | 16.27          | 1.44 —      | 0.1      | 0.34 0.2   | 5 0.35   | 0.37   | 0.35   | 0.08     | 0.28      | 0.03 0.  | 0.10 0.23 | 3 0.20  | 20 0.31    | ND       | ND     | ND       | ND       | ND      | 0.01 0.25        | 0.02    | 0.01     | 0.02   | 0.16   | 0.02     | 0.11   | 0.02      | 0.12 0.05     | 0.05     | 0.14   | 0.13        | 0.15 0.   | .03 0.08   | 0.02             | - 0       | 0.03 0.99    | Trace            | -        | 0.01 0.0   | 0.10       | _      | 0.23   | 0.22   | 0.19   | ##     | 0.05      | 0.07 0.02   | 0.01     | 0.10   | 0.25 0.    | .20 ND      | 0.24           | 0.20   |
| MW - 20     | 11.14 N        | ND 1.77     | 1.02     | 3.15 3.9   | 9 2.52   | 2.58   | 2.63   | 2.9      | 2.83 2    | 2.61 2.  | .94 2.33  | 3 3.00  | 02 3.02    | 2.88     | 3.28   | 2.90     | 3.16     | 2.89    | 2.88 2.85        | 2.22    | 2.49     | 2.43   | 1.99   | 2.46     | 3.52   | 3.02 3    | 3.33 3.25     | 3.12     | 2.88   | 2.58 2      | 2.79 3.   | .84 4.38   | 5.13             | 1.87 1    | 1.71 2.92    | 2.06             | -        | 1.47 2.9   | 0 2.58     | 4.19   | 5.07   | 4.90   | 4.11   | ##     | 3.33 1    | 1.37 3.32   | 1.20     | 1.10   | 1.35 1.    | .38 3.39    | 3.15           | 3.80   |
| MW – 21     | NA 1           | NA 1.38     | 2.29     | 3.83 4.7   | 9 3.26   | 3.35   | 2.13   | 1.45     | 2.75      | 3.31 3.  | 3.04      | 4 3.62  | 52 7.59    | 3.27     | 3.32   | 1.25     | 2.39     | 3.61    | 2.96 2.95        | 2.63    | 4.18     | 2.68   | 2.42   | 2.97     | 4.46   | 3.85 4    | 4.51 3.63     | 3.32     | 2.97   | 2.53 2      | 2.77 2.   | .98 3.46   | 3.23             | 3.62 4    | 4.64 4.90    | 1.99             | -        | 2.69 2.4   | 7 2.48     | 3.37   | 3.13   | 3.72   | 4.66   | ##     | 4.37 3    | 3.66 3.38   | 3.43     | 3.75   | 4.10 4.    | .23 2.89    | 2.04           | 4.15   |
| MW – 22     | NA 1           | NA 1.11     | 0.28     | 0.37 1.7   | 7 1.25   | 1.24   | 1.21   | 0.75     | 0.66      | 0.66 0.  | 0.78      | 4 0.65  | 55 0.50    | 0.51     | 0.38   | 0.30     | 0.01     | 0.51    | 0.62             | 0.45    | 0.48     | 0.44   | 0.15   | 0.22     | 1.33   | 1.01      | 0.49 1.17     | 1.04     | 0.79   | 0.86        | 0.84 0.   | .74 1.33   | 1.27             | 1.03 1    | 1.02 0.54    | 0.85             | -        | 0.74 0.8   | 6 0.75     | 1.22   | 1.07   | 0.69   | 0.50   | ##     | 1.12      | 0.86 0.50   | 0.62     | 1.15   | 1.20 0.    | 0.18 0.21   | 0.18           | 1.80   |
| MW – 23     | 11.73 N        | ND ND       | ND       | ND NI      | ) ND     | ND     | ND     | ND       | ND 1      | ND N     | ND ND     | ) NE    | D ND       | ND       | ND     | ND       | ND       | ND      | ND ND            | ND      | ND       | ND     | ND     | ND       | ND     | ND 1      | ND ND         | ND       | ND     | ND 1        | ND N      | ND ND      | ND               | ND N      | ND ND        | ND               | -        | ND NE      | ) ND       | ND     | ND     | ND     | ND     | ND     | ND 1      | ND ND       | ND       | ND     | ND N       | ND ND       | ND             | ND     |
| MW – 24     | 10.94 NI       | )*** ND     | ND       | ND NI      | ND ND    | ND     | ND     | ND       | ND I      | ND N     | ND ND     | ) NE    | D ND       | ND       | ND     | ND       | ND       | ND      | ND ND            | ND      | ND       | ND     | ND     | ND       | ND     | ND 1      | ND ND         | ND       | ND     | ND 1        | ND N      | ND ND      | ND               | ND N      | ND ND        | ND               | -        | ND NE      | ) –        | _      | ND     | ND     | ND     | ND     | ND 1      | ND ND       | ND       | ND     | ND N       | ND ND       | ND             | ND     |
| MW – 25     | 11.91 10       | 0.81 3.45   | 3.44     | 3.66 4.5   | 4.03     | 4.05   | 4.02   | 3.73     | 4.09      | 3.85 3.  | 3.74      | 4 3.4   | 47 3.89    | 3.62     | 3.60   | 4.20     | 3.79     | 3.65    | 1.01 3.75        | 3.55    | 3.33     | 3.42   | 3.32   | 3.43     | 3.68   | 3.53      | 3.63 3.53     | 3.68     | 3.53   | 2.81 3      | 3.24 3.   | .36 1.07   | 1.03             | 3.16 4    | 4.02 3.65    | 3.48             | -        | 3.91 3.73  | '5 —       | _      | 5.66   | 5.56   | 4.01   | ##     | 4.41 3    | 3.58 3.96   | 3.96     | 4.34   | 3.70 2.    | 82 7.86     | 4.40           | 3.96   |
| MW – 26     | 11.65 10       | 0.84 2.48   | 3.19     | 3.95 5.5   | 3.81     | 3.82   | 3.79   | 3.65     | 3.42      | 3.29 3.  | 3.64      | 4 3.24  | 24 3.14    | 3.20     | 3.56   | 4.00     | 3.28     | 4.26    | 3.58 3.82        | 3.41    | 3.37     | 2.97   | 3.82   | 3.41     | 4.23   | 4.08      | 3.77 4.00     | 3.70     | 3.65   | 3.18        | 3.33 3.   | .64 4.14   | 4.11             | 3.84 3    | 3.70 4.50    | 3.02             | -        | 2.71 3.4   | 8 3.80     | 4.34   | 4.44   | 4.47   | 4.62   | ##     | 4.18      | 3.69 2.86   | 2.33     | 1.00   | 2.45 1.    | .62 –       | 2.61           | 4.02   |
| MW – 27     | 11.18 N        | ND ND       | ND       | ND NI      | ND ND    | ND     | ND     | ND       | ND 1      | ND N     | ND ND     | ) NE    | D ND       | ND       | ND     | ND       | ND       | ND      | ND ND            | ND      | ND       | ND     | ND     | ND       | ND     | ND 1      | ND ND         | ND       | ND     | ND 1        | ND N      | ND ND      | ND               | ND N      | ND ND        | ND               | -        | ND NE      | ) –        | _      | ND     | ND     | ND     | ND     | ND 1      | ND ND       | ND       | ND     | ND N       | ND 0.99     | ND             | ND     |
| MW – 28     | 11.51 N        | ND ND       | ND       | ND NI      | ND ND    | ND     | ND     | ND       | ND 1      | ND N     | ND ND     | ) NE    | D ND       | ND       | ND     | ND       | ND       | ND      | ND ND            | ND      | ND       | ND     | ND     | ND       | ND     | ND 1      | ND ND         | ND       | ND     | ND 1        | ND N      | ND ND      | ND               | ND N      | ND ND        | ND               | _        | ND NE      | O ND       | ND     | ND     | ND     | ND     | ND     | ND 1      | ND ND       | ND       | ND     | ND N       | NI NI       | NI             | NI     |
| MW – 29     | 11.46 N        | ND ND       | ND       | ND NI      | ND ND    | ND     | ND     | ND       | ND 1      | ND N     | ND ND     | ) NE    | D ND       | ND       | ND     | ND       | ND       | ND      | ND ND            | ND      | ND       | ND     | ND     | ND       | ND     | ND 1      | ND ND         | ND       | ND     | ND 1        | ND N      | ND ND      | ND               | ND N      | ND ND        | ND               | -        | ND NE      | O ND       | ND     | ND     | ND     | ND     | ND     | ND 1      | ND ND       | ND       | ND     | ND N       | NI NI       | NI             | NI     |
| MW - 30     | 10.42 N        | ND ND       | ND       | ND NI      | ND ND    | ND     | ND     | ND       | ND 1      | ND N     | ND ND     | ) NE    | D ND       | ND       | ND     | ND       | ND       | ND      | ND ND            | ND      | ND       | ND     | ND     | ND       | ND     | ND 1      | ND ND         | ND       | ND     | ND 1        | ND N      | ND ND      | ND               | ND N      | ND ND        | ND               | -        | ND NE      | ) –        | _      | ND     | ND     | ND     | ND     | ND        | NI NI       | NI       | NI     | NI N       | NI NI       | NI             | NI     |
| MW – 31     | 9.73 N         | ND ND       | ND       | ND NI      | ND ND    | ND     | ND     | ND       | ND 1      | ND N     | ND ND     | ) NE    | D ND       | _        | _      | _        | -        | -       | ND ND            | ND      | ND       | ND     | ND     | ND       | ND     | — l       | ND ND         | ND       | ND     | ND 1        | ND N      | ND ND      | ND               | ND N      | ND ND        | ND               | -        | ND NE      | ) –        | _      | ND     | ND     | ND     | ND     | ND        | NI NI       | NI       | NI     | NI N       | NI NI       | NI             | NI     |
| MW – 32     | 10.41 N        | ND ND       | ND       | ND NI      | ND ND    | ND     | ND     | ND       | ND 1      | ND N     | ND ND     | ) NE    | D ND       | ND       | ND     | ND       | ND       | ND      | ND ND            | ND      | ND       | ND     | ND     | ND       | ND     | ND 1      | ND ND         | ND       | ND     | ND 1        | ND N      | ND ND      | ND               | ND N      | ND ND        | ND               | -        | ND NE      | ) –        | _      | ND     | ND     | ND     | ND     | ND        | NI NI       | NI       | NI     | NI N       | NI NI       | NI             | NI     |
| MW – 34     | NA 1           | NA ND       | ND       | ND NI      | ND ND    | ND     | ND     | ND       | ND 1      | ND N     | ND ND     | ) NE    | D ND       | ND       | ND     | ND       | ND       | ND      | ND ND            | ND      | ND       | ND     | ND     | ND       | ND     | ND 1      | ND ND         | ND       | ND     | ND 1        | ND N      | ND ND      | ND               | ND N      | ND ND        | ND               | -        | ND NE      | ) ND       | ND     | ND     | ND     | ND     | ND     | ND        | NI NI       | NI       | NI     | NI N       | NI NI       | NI             | NI     |
| MW – 35     | NA I           | NA ND       | ND       | ND NE      | ND ND    | ND     | ND     | ND       | ND I      | ND N     | ND ND     | ) NE    | D ND       | ND       | ND     | ND       | ND       | ND      | ND ND            | ND      | ND       | ND     | ND     | ND       | ND     | ND 1      | ND ND         | ND       | ND     | ND 1        | ND N      | ND ND      | ND               | ND N      | ND ND        | ND               | -        | ND NE      | ) ND       | ND     | ND     | ND     | ND     | ND     | ND        | NI NI       | NI       | NI     | NI N       | NI NI       | NI             | NI     |
| MW – 36     | 11.21 N        | ND ND       | ND       | ND NE      | ND       | ND     | ND     | ND       | ND I      | ND N     | ND ND     | ) NE    | D ND       | ND       | ND     | ND       | ND       | ND      | ND ND            | ND      | ND       | ND     | ND     | ND       | ND     | ND 1      | ND ND         | ND       | ND     | ND 1        | ND N      | ND ND      | ND               | ND N      | ND NI        | NI               | NI       | NI NI      | I NI       | NI     | NI     | NI     | NI     | NI     | NI        | NI NI       | NI       | NI     | NI N       | NI NI       | NI             | NI     |
| MW – 37     | 11.64 N        | ND ND       | ND       | ND NI      | ND ND    | ND     | ND     | ND       | ND 1      | ND N     | ND ND     | ) NE    | D ND       | ND       | ND     | ND       | ND       | ND      | ND ND            | ND      | ND       | ND     | ND     | ND       | ND     | ND 1      | ND ND         | ND       | ND     | ND 1        | ND N      | ND ND      | ND               | ND N      | ND NI        | NI               | NI       | NI NI      | I NI       | NI     | NI     | NI     | NI     | NI     | NI        | NI NI       | NI       | NI     | NI N       | NI NI       | NI             | NI     |
| MW – 38     | 10.22 N        | ND ND       | ND       | ND NI      | ND ND    | ND     | ND     | ND       | ND 1      | ND N     | ND ND     | ) NE    | D ND       |          | _      | _        | _        |         | ND ND            | ND      | ND       | ND     | ND     | ND       | ND     | ND 1      | ND ND         | ND       | ND     | ND 1        | ND N      | ND ND      |                  | ND I      | NI NI        | NI               | NI       | NI NI      | I NI       | NI     | NI     | NI     | NI     | NI     | NI        | NI NI       | NI       | NI     | NI N       | NI NI       | NI             | NI     |
| MW – 39     | 8.38 N         | ND ND       | ND       | ND NI      | ND ND    | ND     | ND     | ND       | ND 1      | ND N     | ND ND     | ) NE    | D ND       | ND       | ND     | ND       | ND       | ND      | ND ND            | ND      | ND       | ND     | ND     | ND       | ND     | ND 1      | ND ND         | ND       | ND     | ND 1        | ND N      | ND ND      | ND               | ND I      | NI NI        | NI               | NI       | NI NI      | I NI       | NI     | NI     | NI     | NI     | NI     | NI        | NI NI       | NI       | NI     | NI N       | NI NI       | NI             | NI     |
| MW – 40     | NA N           | NA ND       | ND       | ND NE      | ) ND     | ND     | ND     | ND       | ND I      | ND N     | ND ND     | ) NE    | D ND       | ND       | ND     | ND       | ND       | ND      | ND ND            | ND      | ND       | ND     | ND     | ND       | ND     | - 1       | ND ND         | ND       | ND     | ND 1        | ND N      | ND ND      | ND               | ND I      | NI NI        | NI               | NI       | NI NI      | I NI       | NI     | NI     | NI     | NI     | NI     | NI        | NI NI       | NI       | NI     | NI N       | NI NI       | NI             | NI     |
| MW – 41     | 10.35 N        | ND ND       | ND       | ND NI      | ND ND    | ND     | ND     | ND       | ND I      | ND N     | ND ND     | ) NE    | D ND       | ND       | ND     | ND       | ND       | ND      | ND ND            | ND      | ND       | ND     | ND     | ND       | ND     | ND 1      | ND ND         | ND       | ND     | ND 1        | ND N      | ND ND      | ND               | NI I      | NI NI        | NI               | NI       | NI NI      | I NI       | NI     | NI     | NI     | NI     | NI     | NI        | NI NI       | NI       | NI     | NI N       | NI NI       | NI             | NI     |
| MW – 42     | 9.64 N         | ND ND       | ND       | ND NI      | ) ND     | ND     | ND     | ND       | ND 1      | ND N     | ND ND     | ) NE    | D ND       | ND       | ND     | ND       | ND       | ND      | ND ND            | ND      | ND       | ND     | ND     | ND       | ND     | ND 1      | ND ND         | ND       | ND     | ND 1        | ND N      | ND ND      | ND               | NI I      | NI NI        | NI               | NI       | NI NI      | I NI       | NI     | NI     | NI     | NI     | NI     | NI        | NI NI       | NI       | NI     | NI N       | NI NI       | NI             | NI     |
| MW - 45     | 11.12 N        | ID -        | -        |            | -        | -      | -      | -        | -         | -        |           | -       |            | -        | -      | -        | -        | -       |                  | -       | -        | -      | -      | -        | -      | -         |               | -        | -      | -           | -         |            | -                | -         |              | -                | -        |            | -          | -      | -      | -      | -      | -      | -         |             | -        | -      | -          |             | -              | -      |
| MW - 46     | 11.55 N        | 1D -        | -        |            | -        | -      | -      | -        | -         | -        |           | -       | -          | -        | -      | -        | -        | -       |                  | -       | -        | -      | -      | -        | -      | -         |               | -        | -      | -           | -         |            | -                | -         |              | -                | -        |            | -          | -      | -      | -      | -      | -      | -         |             | -        | -      | -          |             | -              | -      |
| MW - 47     | 11.10 N        | 1D -        | -        |            | -        | -      | -      | -        | -         | -        |           | -       |            | -        | -      | -        | -        | -       |                  | -       | -        | -      | -      | -        | -      | -         |               | -        | -      | -           | -         |            | -                | -         |              | -                | -        |            | -          | -      | -      | -      | -      | -      | -         |             | -        | -      | -          |             | -              | -      |
| MW-A        | NA N           | NA -        | -        |            | -        | -      | -      | -        | -         | -        |           | -       | -   -      | -        | -      | -        | -        | -       |                  | -       | -        | -      | -      | -        | -      | -         |               | -        | -      | -           | -         |            | -                | -         |              | -                | -        |            | -          | -      | -      | -      | -      | -      | -         |             | -        | -      | -          |             | -              | -      |
| RW – 1      | NA 1           | NA ND       | ND       | ND NI      | ND ND    | ND     | ND     | ND       | ND I      | ND N     | ND ND     | ) NE    | D ND       | ND       | ND     | ND       | ND       | ND      | ND ND            | ND      | ND       | ND     | ND     | ND       | ND     | - 1       | ND ND         | ND       | ND     | ND 1        | ND N      | ND ND      | ND               | ND N      | ND ND        | ND               | -        | ND NE      | ) ND       | ND     | ND     | ND     | ND     | ND     | ND I      | ND –        | ND       | ND     | ND N       | ND ND       | ND             | ND     |
| RW – 2      | NA 1           | NA 0.08     | 5.52     | 4.01 5.1   | 0.56     | 0.58   | 0.53   | 6.09     | 6.25      | 0.42     | .13 2.90  | 0 3.09  | 09 3.53    | 1.65     | 1.18   | 1.26     | 1.35     | 1.88    | 2.05 2.41        | 3.02    | 2.12     | 3.34   | 2.70   | 2.83     | 4.28   | _ 2       | 2.64 2.97     | 3.41     | 5.54   | 5.28        | 5.44 2.   | .82 4.19   | 4.52             | 4.52 4    | 4.53 4.52    | 0.11             | -        | 1.30 3.0   | 5 2.31     | 2.80   | 3.19   | 5.09   | 3.86   | ##     | 4.07      | 2.96 2.92   | 3.48     | 3.75   | 4.20 2.    | 1.92        | 1.50           | 5.85   |
| RW – 3      |                | NA 2.12     |          |            | _        |        |        |          |           |          |           |         | 98 3.10    |          |        | 2.40     |          |         |                  | _       |          |        |        |          |        |           |               | _        | _      | 2.23 2      |           |            |                  |           |              |                  |          | 1.58 2.9   |            | _ ` `  |        |        |        |        | 2.96      |             |          | 3.34   |            | 5.58 2.84   |                |        |
| RW – 4      |                | NA 3.01     |          | 3.06 4.3   |          |        | 4.18   |          |           | 3.69     |           | 9 3.6   |            | 3.80     |        | 2.77     |          |         |                  | 2.02    |          |        | 2.03   |          |        | 2.31 1    |               | 2.02     |        |             |           |            |                  |           | 2.88 ##      |                  |          | 1.81 3.2   |            | 2.45   |        | 2.30   |        |        |           |             |          | 3.00   |            | 95 —        | 3.45           |        |
|             |                |             |          |            |          |        |        |          |           |          |           |         |            |          |        |          |          |         |                  |         |          |        |        |          |        |           |               |          |        | 4.69 4      |           |            |                  |           |              |                  |          |            |            |        |        |        |        |        |           |             |          |        |            | 3.00        |                |        |
| RW – 6      |                |             |          |            |          |        |        |          |           |          |           | 2 0.90  | 90 0.90    | 0.85     | 0.68   | 0.87     | 0.92     | 1.46    | .29 0.81         | 0.67    | 0.73     | 0.74   | 0.76   | 0.74     | 0.77   | 0.65      | 0.66 0.65     | 0.61     | 0.78   | 1.96 2      |           |            |                  |           |              |                  |          |            |            |        |        |        |        |        |           |             | 0.50     | 0.21   | 0.40 0.    | 0.15 0.90   | 0.22           | 0.06   |
| RW – 8 ***  |                |             | 0.96     |            |          |        |        | 1.2      |           |          |           |         |            |          | _      | _        |          |         | _   _            |         |          |        |        |          | _      |           |               |          |        |             |           |            | 2.92             |           |              |                  |          | 0.65 1.4   |            |        |        |        |        |        |           |             |          |        |            |             |                |        |
| RW – 9      |                | NA 1.51     |          |            |          |        |        |          |           |          |           |         |            |          |        |          |          |         |                  |         |          |        |        |          |        |           |               |          |        |             |           |            |                  |           |              |                  |          |            |            |        |        |        |        |        |           |             | 2.62     | 3.11   | 3.50 3.    | 3.83        | 2.98           | 5.33   |
| RW – 10     |                | NA 0.66     |          | 4.64 4.2   |          |        |        |          |           |          | 3.79 4.2  |         |            | 3.86     |        |          |          |         |                  |         |          |        |        |          |        |           |               |          |        | 3.80        |           |            |                  |           | 3.74 3.57    |                  |          | 3.38 3.89  |            |        |        | 3.99   |        |        | 4.11 3    |             |          |        | _   -      |             | <del>  -</del> |        |
| RW – 11     |                |             |          |            |          |        |        |          |           |          |           |         |            | 1.90     |        | 2.43     |          |         | 2.98 3.43        | 3.08    | 2.94     | 3.05   |        | _        | 4.65   | 4.39 3    | 3.59 3.24     | 3.62     | 3.43   | 3.66        |           | .00 3.87   | 3.97             |           |              | 3.87             | -        | 2.03 2.5   |            | 3.66   | 4.27   | 5.48   |        | ##     | 3.91      | 3.49 3.15   | 2.67     | 3.11   | 3.50 2.    | .93 4.49    |                |        |
| RW- 12 ***  |                |             |          | 1.5 5.9    |          |        |        |          |           |          | 0.02 0.80 |         |            |          | _      | -        |          | _       | <del>-   -</del> |         |          | -      |        | -        | _      | -         |               |          |        |             | _   -     | -   -      | <del>  -  </del> |           |              | <del>  -  </del> | _        |            | ·   -      |        | -      | _      | _      | _      | -         |             |          |        | _   -      |             |                |        |
| MW - 1      |                |             |          |            |          |        |        |          |           |          |           |         |            |          |        |          |          |         |                  |         |          |        |        |          |        |           |               |          |        | NG 1        |           |            |                  |           |              |                  |          |            |            |        | _      |        |        |        |           |             |          |        |            | NG NG       |                |        |
| MW - 9      |                |             |          | NG NO      | _        |        |        |          |           |          |           |         |            | _        |        | NG       |          |         |                  | _       |          | _      | NG     | + +      |        |           |               |          | _      | NG 1        |           | _          |                  |           | NG NG        |                  |          | NG NO      |            |        | _      |        |        |        |           |             |          | NG     |            |             | NG             |        |
| MW - 10     |                | NG NG       | NG       |            |          |        | NG     |          |           | NG N     |           | G NO    |            | NG       |        |          |          |         |                  | NG      |          | _      | NG     |          |        |           | NG NG         |          |        |             | NG N      |            |                  |           | NG NG        |                  |          | NG NO      |            |        | _      | NG     |        |        |           |             |          | NG     |            |             | _              | _      |
| MW - 17     |                | NG NG       |          | NG NO      |          |        |        | NG       |           |          | NG NG     | _       |            | NG       |        |          | NG       |         | NG NG            |         |          | _      | NG     | _        |        |           |               |          |        | NG 1        |           |            | NG               | _         | NG NG        |                  |          | NG NO      |            |        | _      | _      |        |        |           | NG NG       |          | _      |            | NG NG       |                | NG     |
| MW - 18     |                | NG NG       | NG       |            |          |        | NG     |          |           | NG N     |           |         |            |          | NG     |          |          |         | NG NG            |         |          |        |        | _        |        |           | NG NG         |          |        |             | NG N      |            |                  |           | NG NG        |                  |          | NG NO      |            | _      |        | NG     |        |        |           | NG NG       |          |        |            | NG NG       |                | NG     |
| RW - 7      | NG N           | NG NG       | NG       | NG NO      | NG       | NG     | NG     | NG       | NG I      | NG N     | NG NG     | G NC    | G NG       | NG       | NG     | NG       | NG       | NG      | NG NG            | NG      | NG       | NG     | NG     | NG       | NG     | NG I      | NG NG         | NG       | NG     | NG 1        | NG N      | NG NG      | NG               | NG N      | NG NG        | NG               | NG       | NG NO      | G NG       | NG     | NG     | NG     | NG     | NG     | NG        | NG NG       | NG       | NG     | NG N       | NG NG       | NG             | NG     |

Notes:

Data recorded using an oil/water interface prol
## = NAPL observed, apparent thickness not c
NI = Not Installed ND = Not Del
Wells MW-1, MW-2, MW-9, MW-10, MW-1
est= Estimated Value \*\* = Water n

\* = Well was dry
Wells were gauged on 30 June 2023



