

A Test Method for Certification of Cord Wood-Fired Hydronic Heating Appliances with Partial Thermal Storage: Measurement of Particulate Matter (PM) and Carbon Monoxide (CO) Emissions and Heating Efficiency of Wood-Fired Hydronic Heating Appliances with Partial Thermal Storage

1.0 Scope and Application

1.1 This test method applies to wood-fired hydronic heating appliances with heat storage external to the appliance. The units typically transfer heat through circulation of a liquid heat exchange media such as water or a water-antifreeze mixture. Throughout this document, the term “water” will be used to denote any of the heat transfer liquids approved for use by the manufacturer.

1.2 The test method measures PM and CO emissions and delivered heating efficiency at specified heat output rates referenced against the appliance’s rated heating capacity as specified by the manufacturer and verified under this test method.

1.3 PM emissions are measured by the dilution tunnel method as specified in EPA Method 28 WHH and the standards referenced therein with the exceptions noted in Section 12.5.9. Delivered Efficiency is measured by determining the fuel energy input and appliance output. Heat output is determined through measurement of the flow rate and temperature change of water circulated through a heat exchanger external to the appliance and the increase in energy of the external storage. Heat input is determined from the mass of dry wood fuel and its higher heating value (HHV). Delivered efficiency does not attempt to account for pipeline loss.

1.4 Products covered by this test method include both pressurized and non-pressurized hydronic heating appliances intended to be fired with wood and for which the manufacturer specifies for indoor or outdoor installation. The system, which includes the heating appliance and external storage, is commonly connected to a heat exchanger by insulated pipes and normally includes a pump to circulate heated liquid. These systems are used to heat structures such as homes, barns and greenhouses. They also provide heat for domestic hot water, spas and swimming pools.

1.5 Distinguishing features of products covered by this standard include:

1.5.1 The manufacturer specifies the application for either indoor or outdoor installation.

1.5.2 A firebox with an access door for hand loading of fuel.

1.5.3 Typically an aquastat mounted as part of the appliance that controls combustion air supply to maintain the liquid in the appliance within a predetermined temperature range provided sufficient fuel is available in the firebox. The appliance may be equipped with other devices to control combustion.

1.5.4 A chimney or vent that exhausts combustion products from the appliance.

1.5.5 A liquid storage system, typically water, which is not large enough to accept all of the heat produced when a full load of wood is burned and the storage system starts a burn cycle at 125 °F.

1.5.6 The heating appliances require external thermal storage and these units will only be installed as part of a system which includes thermal storage. The manufacturer specifies the minimum amount of thermal storage required. However, the storage system shall be large enough to ensure that the boiler does not cycle, slumber, or go into an off-mode when operated in a Category III load condition (see Section 4.3).

1.6 The values stated are to be regarded as the standard whether in I-P or SI units. The values given in parentheses are for information only.

2.0 Summary of Method and References

2.1 PM and CO emissions are measured from a wood-fired hydronic heating appliance burning a prepared test fuel charge in a test facility maintained at a set of prescribed conditions. Procedures for determining heat output rates, PM and CO emissions, and efficiency and for reducing data are provided.

2.2 Referenced Documents

2.2.1 EPA Standards

2.2.1.1 Method 28 Certification and Auditing of Wood Heaters

2.2.1.2 Method 28 WHH Measurement of Particulate Emissions and Heating Efficiency of Wood-Fired Hydronic Heating Appliances and the standards referenced therein. This test method is incorporated in the EPA Hydronic Heater Program Phase 2 Partnership Agreement, 10/12/2011, <http://www.epa.gov/burnwise/pdfs/owhphase2agreement.pdf> .

2.2.2 Other Standards

2.2.2.1 CAN/CSA-B415.1-2010 *Performance Testing of Solid-Fuel-Burning Heating Appliances*

3.0 Terminology

3.1 Definitions

- 3.1.1 Hydronic Heating – A heating system in which a heat source supplies energy to a liquid heat exchange media such as water that is circulated to a heating load and returned to the heat source through pipes.
- 3.1.2 Aquastat – A control device that opens or closes a circuit to control the rate of fuel consumption in response to the temperature of the heating media in the heating appliance.
- 3.1.3 Delivered Efficiency – The percentage of heat available in a test fuel charge that is delivered to a simulated heating load or the storage system as specified in this test method.
- 3.1.4 Emission factor – the emission of a pollutant expressed in mass per unit of energy (typically) output from the boiler
- 3.1.5 Emission index – the emission of a pollutant expressed in mass per unit mass of fuel used
- 3.1.6 Emission rate – the emission of a pollutant expressed in mass per unit time
- 3.1.7 Manufacturer’s Rated Heat Output Capacity –The value in Btu/hr (MJ/hr) that the manufacturer specifies that a particular model of hydronic heating appliance is capable of supplying at its design capacity as verified by testing, in accordance with Section 12.5.4.
- 3.1.8 Heat output rate – The average rate of energy output from the appliance during a specific test period in Btu/hr (MJ/hr)
- 3.1.9 Firebox – The chamber in the appliance in which the test fuel charge is placed and combusted.
- 3.1.10 NIST – National Institute of Standards and Technology
- 3.1.11 Test fuel charge – The collection of test fuel placed in the appliance at the start of the emission test run.
- 3.1.12 Test Run – An individual emission test which encompasses the time required to consume the mass of the test fuel charge. The time of the test run also considers the time for the energy to be drawn from the thermal storage.
- 3.1.13 Test Run Under “Cold-to-Cold” Condition – under this test condition the test fuel is added into an empty chamber along with kindling and ignition materials (paper). The boiler at the start of this test is typically 125 to 130 F.
- 3.1.14 Test Run Under “Hot-to-Hot” Condition – under this test condition the test fuel is added onto a still-burning bed of charcoals produced in a pre-burn period. The boiler water is near its operating control limit at the start of the test.

3.1.14 Overall Efficiency, also known as Stack Loss Efficiency – The efficiency for each test run as determined using the CSA B415.1-2010 Stack Loss Method (SLM).

3.1.15 Phases of a Burn Cycle. The “startup phase” is defined as the period from the start of the test until 15% of the test fuel charge is consumed. The “steady state phase” is defined as the period from the end of the startup phase to a point at which 80% of the test fuel charge is consumed. The “end phase” is defined as the time from the end of the steady state period to the end of the test.

3.1.16 Thermopile - A device consisting of a number of thermocouples connected in series, used for measuring differential temperature.

3.1.17 Slumber Mode – This is a mode in which the temperature of the water in the boiler has exceeded the operating control limit and the control has changed the boiler fan speed, dampers, and/or other operating parameters to minimize the heat output of the boiler.

4.0 Summary of Test Method

4.1 Dilution Tunnel. Emissions are determined using the “dilution tunnel” method specified in EPA Method 28 WHH and the standards referenced therein. The flow rate in the dilution tunnel is maintained at a constant level throughout the test cycle and accurately measured. Samples of the dilution tunnel flow stream are extracted at a constant flow rate and drawn through high efficiency filters. The filters are dried and weighed before and after the test to determine the emissions collected and this value is multiplied by the ratio of tunnel flow to filter flow to determine the total particulate emissions produced in the test cycle.

4.2 Efficiency. The efficiency test procedure takes advantage of the fact that this type of system delivers heat through circulation of the heated liquid (water) from the system to a remote heat exchanger (e.g. baseboard radiators in a room) and back to the system. Measurements of the cooling water temperature difference as it enters and exits the test system heat exchanger along with the measured flow rate allow for an accurate determination of the useful heat output of the appliance. Also included in the heat output is the change in the energy content in the storage system during a test run. Energy input to the appliance during the test run is determined by weight of the test fuel charge, adjusted for moisture content, multiplied by the Higher Heating Value. Additional measurements of the appliance weight and temperature at the beginning and end of a test cycle are used to correct for heat stored in the appliance. Overall Efficiency (SLM) is determined using the CSA B415.1-2010 stack loss method for data quality assurance purposes.

4.3 Operation. Four test categories are defined for use in this method. These are:

4.3.1 Category I: A heat output of 15% or less of Manufacturer’s Rated Heat Output Capacity.

4.3.2 Category II: A heat output of 16% to 24% of Manufacturer's Rated Heat Output Capacity.

4.3.3 Category III: A heat output of 25% to 50% of Manufacturer's Rated Heat Output Capacity.

4.3.4 Category IV: Manufacturer's Rated Heat Output Capacity.

These heat output categories refer to the output from the system by way of the load heat exchanger installed for the test. The output from just the boiler part of the system may be higher for all or part of a test, as part of this boiler output goes to storage.

For the Category III and IV runs, appliance operation is conducted on a hot-to-hot test cycle meaning that the appliance is brought to operating temperature and a coal bed is established prior to the addition of the test fuel charge and measurements are made for each test fuel charge cycle. The measurements are made under constant heat draw conditions within pre-determined ranges. No attempt is made to modulate the heat demand to simulate an indoor thermostat cycling on and off in response to changes in the indoor environment.

For the Category I and II runs, the unit is tested with a "cold start".

At the manufacturer's option, the Category II and III runs may be waived and it may be assumed that the particulate emission values and efficiency values determined in the start-up, steady-state, and end phases of Category I are applicable in Categories II and III for the purpose of determining the annual averages in lb/MMBtu and g/MJ (see Section 13). For the annual average in g/hr, the length of time for stored heat to be drawn from thermal storage shall be determined for the test load requirements of the respective Category.

All test operations and measurements shall be conducted by personnel of the laboratory responsible for the submission of the test report.

5.0 Significance and Use

5.1 The measurement of particulate matter emission and CO rates is an important test method widely used in the practice of air pollution control.

5.1.1 These measurements, when approved by state or federal agencies, are often required for the purpose of determining compliance with regulations and statutes.

5.1.2 The measurements made before and after design modifications are necessary to demonstrate the effectiveness of design changes in reducing emissions and make this standard an important tool in manufacturer's research and development programs.

5.2 Measurement of heating efficiency provides a uniform basis for comparison of product performance that is useful to the consumer. It is also required to relate emissions produced to the useful heat production.

5.3 This is a laboratory method and is not intended to be fully representative of all actual field use. It is recognized that users of hand-fired wood burning equipment have a great deal of influence over the performance of any wood-burning appliance. Some compromises in realism have been made in the interest of providing a reliable and repeatable test method.

6.0 Test Equipment

6.1 Scale. A platform scale capable of weighing the boiler under test and associated parts and accessories when completely filled with water to an accuracy of ± 1.0 pound (± 0.5 kg) and a readout resolution of ± 0.2 pound (± 0.1 kg).

6.2 Heat Exchanger. A water-to-water heat exchanger capable of dissipating the expected heat output from the system under test.

6.3 Water Temperature Difference Measurement. A Type –T ‘special limits’ thermopile with a minimum of 5 pairs of junctions shall be used to measure the temperature difference in water entering and leaving the heat exchanger. The temperature difference measurement uncertainty of this type of thermopile is equal to or less than ± 0.50 °F (± 0.25 °C). Other temperature measurement methods may be used if the temperature difference measurement uncertainty is equal to or less than ± 0.50 °F (± 0.25 °C). This measurement uncertainty shall include the temperature sensor, sensor well arrangement, piping arrangements, lead wire, and measurement / recording system. The response time of the temperature measurement system shall be less than half of the time interval at which temperature measurements are recorded.

6.4 Water Flow Meter. A water flow meter shall be installed in the inlet to the load side of the heat exchanger. The flow meter shall have an accuracy of $\pm 1\%$ of measured flow.

6.4.1 Optional - Appliance side water flow meter. A water flow meter with an accuracy of $\pm 1\%$ of the flow rate is recommended to monitor supply side water flow rate.

6.5 Optional Recirculation Pump. Circulating pump used during test to prevent stratification, in the boiler, of liquid being heated.

6.6 Water Temperature Measurement – Thermocouples or other temperature sensors to measure the water temperature at the inlet and outlet of the load side of the heat exchanger must meet the calibration requirements specified in 10.1 of this method.

6.7 Lab Scale – For measuring the moisture content of wood slices as part of the overall wood moisture determination. Accuracy of ± 0.01 pounds.

6.8 Flue Gas Temperature Measurement – Must meet the requirements of CSA B415.1-2010, Clause 6.2.2.

6.9 Test Room Temperature Measurement – Must meet the requirements of CSA B415.1-2010, Clause 6.2.1.

6.10 Flue Gas Composition Measurement – Must meet the requirements of CSA B415.1-2010, Clauses 6.3.1 through 6.3.3.

6.11 Dilution Tunnel CO Measurement – In parallel with the flue gas composition measurements, the CO concentration in the dilution tunnel shall also be measured and reported at time intervals not to exceed one minute. This analyzer shall meet the zero and span drift requirements of CSA B415.1-2012. In addition the measurement repeatability shall be better than ± 15 ppm over the range of CO levels observed in the dilution tunnel.

7.0 Safety

7.1 These tests involve combustion of wood fuel and substantial release of heat and products of combustion. The heating system also produces large quantities of very hot water and the potential for steam production and system pressurization. Appropriate precautions must be taken to protect personnel from burn hazards and respiration of products of combustion.

8.0 Sampling, Test Specimens and Test Appliances

8.1 Test specimens shall be supplied as complete appliances, as described in marketing materials, including all controls and accessories necessary for installation in the test facility. A full set of specifications, installation and operating instructions, and design and assembly drawings shall be provided when the product is to be placed under certification of a third-party agency. The manufacturer's written installation and operating instructions are to be used as a guide in the set-up and testing of the appliance and shall be part of the test record.

8.2 The size, connection arrangement, and control arrangement for the thermal storage shall be as specified in the manufacturer's documentation. It is not necessary to use the specific storage system that the boiler will be marketed with. However, the capacity of the system used in the test cannot be greater than that specified as the minimum allowable for the boiler.

8.3 All system control settings shall be the as-shipped, default settings. These default settings shall be the same as those communicated in a document to the installer or end user. These control settings and the documentation of the control settings as to be provided to the installer or end user shall be part of the test record.

8.4 Where the manufacturer defines several alternatives for the connection and loading arrangement, one shall be defined in the appliance documentation as the default or standard installation. It is expected that this will be the configuration for use with a simple baseboard heating system. This is the configuration to be followed for these tests. The manufacturer's documentation shall define the other arrangements as optional or alternative arrangements.

9.0 Preparation of Test Equipment

9.1 The appliance is to be placed on a scale capable of weighing the appliance fully loaded with a resolution of ± 0.2 lb (0.1 kg).

9.2 The appliance shall be fitted with the type of chimney recommended or provided by the manufacturer and extending to 15 ± 0.5 feet (4.6 ± 0.15 m) from the upper surface of the scale. If no flue or chimney system is recommended or provided by the manufacturer, connect the appliance to a flue of a diameter equal to the flue outlet of the appliance. The flue section from the appliance flue collar to 8 ± 0.5 feet above the scale shall be single wall stove pipe and the remainder of the flue shall be double wall insulated class A chimney.

9.3 Optional Equipment Use

9.3.1 A recirculation pump may be installed between connections at the top and bottom of the appliance to minimize thermal stratification if specified by the manufacturer. The pump shall not be installed in such a way as to change or affect the flow rate between the appliance and the heat exchanger.

9.3.2 If the manufacturer specifies that a thermal control valve or other device be installed and set to control the return water temperature to a specific set point, the valve or other device shall be installed and set per the manufacturer's written instructions.

9.4 Prior to filling the boiler with water, weigh and record the appliance mass.

9.5 Heat Exchanger

9.5.1 Plumb the unit to a water-to-water heat exchanger with sufficient capacity to draw off heat at the maximum rate anticipated. Route hoses and electrical cables and instrument wires in a manner that does not influence the weighing accuracy of the scale as indicated by placing dead weights on the platform and verifying the scale's accuracy.

9.5.2 Locate thermocouples to measure the water temperature at the inlet and outlet of the load side of the heat exchanger.

9.5.3 Install a thermopile (or equivalent instrumentation) meeting the requirements of Section 6.3 to measure the water temperature difference between the inlet and outlet of the load side of the heat exchanger.

9.5.4 Install a calibrated water flow meter in the heat exchanger load side supply line. The water flow meter is to be installed on the cooling water inlet side of the heat exchanger so that it will operate at the temperature at which it is calibrated.

9.5.5 Place the heat exchanger in a box with 2 in. (50 mm) of expanded polystyrene (EPS) foam insulation surrounding it to minimize heat losses from the heat exchanger.

9.5.6 The reported efficiency and heat output rate shall be based on measurements made on the load side of the heat exchanger.

9.5.7 Temperature instrumentation per Section 6.6 shall be installed in the appliance outlet and return lines. The average of the outlet and return water temperature on the supply side of the system shall be considered the average appliance temperature for calculation of heat storage in the appliance (TF_{avg} and TI_{avg}). Installation of a water flow meter in the supply side of the system is optional.

9.6 Storage Tank. The storage tank shall include a destratification pump as illustrated in Figure 1. The pump will draw from the bottom of the tank and return to the top as illustrated. Temperature sensors (TS1 and TS2 in Figure 1) shall be included to measure the temperature in the recirculation loop. The valve plan in Figure 1 allows the tank recirculation loop to operate and the boiler-to-heat exchanger loop to operate at the same time but in isolation. This would typically be done before the start of a test or following completion of a test to determine the end of test average tank temperature. The nominal flow rate in the storage tank recirculation loop can be estimated based on pump manufacturer's performance curves and any significant restriction in the recirculation loop.

9.7 Fill the system with water. Determine the total weight of the water in the appliance when the water is circulating. Verify that the scale indicates a stable weight under operating conditions. Make sure air is purged properly.

10.0 Calibration and Standardization

10.1 Water Temperature Sensors. Temperature measuring equipment shall be calibrated before initial use and at least semi-annually thereafter. Calibrations shall be in compliance with National Institute of Standards and Technology (NIST) Monograph 175, Standard Limits of Error.

10.2 Heat Exchanger Load Side Water Flow Meter.

10.2.1 The heat exchanger load side water flow meter shall be calibrated within the flow range used for the test run using NIST-traceable methods. Verify the calibration of the water flow meter before and after each test run and at least once during each test run by comparing the water flow rate indicated by the flow meter to the mass of water collected from the outlet of the heat exchanger over a

timed interval. Volume of the collected water shall be determined based on the water density calculated from Section 13, Eq. 12, using the water temperature measured at the flow meter. The uncertainty in the verification procedure used shall be 1% or less. The water flow rate determined by the collection and weighing method shall be within 1% of the flow rate indicated by the water flow meter.

10.3 Scales. The scales used to weigh the appliance and test fuel charge shall be calibrated using NIST-traceable methods at least once every 6 months.

10.4 Flue Gas Analyzers – In accordance with CSA B415.1-2010, Clause 6.8.

11.0 Conditioning

11.1 Prior to testing, a non-catalytic appliance is to be operated for a minimum of 10 hours using a medium heat draw rate. Catalytic units shall be operated for a minimum of 50 hours using a medium heat draw rate. The pre-burn for the first test can be included as part of the conditioning requirement. If conditioning is included in pre-burn, then the appliance shall be aged with fuel meeting the specifications outlined in Sections 12.2 with a moisture content between 19 and 25 percent on a dry basis. Operate the appliance at a medium heat output rate (Category II or III) for at least 10 hours for non-catalytic appliances and 50 hours for catalytic appliances. Record and report hourly flue gas exit temperature data and the hours of operation. The aging procedure shall be conducted and documented by a testing laboratory.

12.0 Procedure

12.1 Appliance Installation. Assemble the appliance and parts in conformance with the manufacturer's written installation instructions. Clean the flue with an appropriately sized, wire chimney brush before each certification test series.

12.2 Fuel. Test fuel charge fuel shall be red (*Quercus ruba L.*) or white (*Quercus Alba*) oak 19 to 25% moisture content on a dry basis. Piece length shall be 80% of the firebox depth rounded down to the nearest 1 inch (25mm) increment. For example, if the firebox depth is 46 inches (1168mm) the piece length would be 36 inches (46 inches x 0.8 = 36.8 inches round down to 36 inches). Pieces are to be placed in the firebox parallel to the longest firebox dimension. For fireboxes with sloped surfaces that create a non-uniform firebox length, the piece length shall be adjusted for each layer based on 80% of the length at the level where the layer is placed. The test fuel shall be cord wood with cross section dimensions and weight limits as defined in CSA B415.1-2010, Section 8.3, Table 4. The use of dimensional lumber is not allowed.

12.2.1 Select three pieces of cord wood from the same batch of wood as the test fuel and the same weight as the average weight of the pieces in the test load \pm 1.0 lb. From each of these three pieces, cut three slices. Each slice shall be $\frac{1}{2}$ " to $\frac{3}{4}$ " thick. One slice shall be cut across the center of the length of the piece. The other two slices shall be cut half way between the center and the end. Immediately measure the mass of each piece in pounds. Dry each slice in an

oven at 220 °F for 24 hours or until no further weight change occurs. The slices shall be arranged in the oven so as to provide separation between faces. Remove from the oven and measure the mass of each piece again as soon as practical in pounds.

The moisture content of each slice, on a dry basis shall be calculated as:

$$MC_{slice} = \frac{100 \cdot (W_{SliceWet} - W_{SliceDry})}{W_{SliceDry}}$$

Where:

$W_{SliceWet}$ = weight of the slice before drying in pounds

$W_{SliceDry}$ = weight of the slice after drying in pounds

MC_{Slice} = moisture content of the slice in % dry basis

The average moisture content of the entire test load (MC) shall be determined using Eq. 6. Each individual slice shall have a moisture content in the range of 18 to 28 % on a dry basis. The average moisture content for the test fuel load shall be in the range of 19 to 25%. Moisture shall not be added to previously dried fuel pieces except by storage under high humidity conditions and temperature up to 100°F. Fuel moisture measurement shall begin within four hours of using the fuel batch for a test. Use of a pin-type meter to estimate the moisture content prior to a test is recommended.

12.2.2 Firebox Volume. Determine the firebox volume in cubic feet. Firebox volume shall include all areas accessible through the fuel loading door where firewood could reasonably be placed up to the horizontal plane defined by the top of the loading door. A drawing of the firebox showing front, side and plan views or an isometric view with interior dimensions shall be provided by the manufacturer and verified by the laboratory. Calculations for firebox volume from computer aided design (CAD) software programs are acceptable and shall be included in the test report if used. If the firebox volume is calculated by the laboratory the firebox drawings and calculations shall be included in the test report.

12.2.3 Test Fuel charge. Test fuel charges shall be determined by multiplying the firebox volume by 10 pounds (4.54 kg) per ft³ (28L), or a higher load density as recommended by the manufacturer's printed operating instructions, of wood (as used wet weight). Select the number of pieces of cordwood that most nearly match this target weight. However, the test fuel charge cannot be less than the target of 10 pounds (4.54 kg) per ft³ (28L).

12.3 Sampling Equipment. Prepare the particulate emission sampling equipment as defined by EPA Method 28 WHH and the standards referenced therein.

12.4 Appliance Start-Up. The appliance shall be fired with wood fuel of any species, size and moisture content at the laboratories discretion to bring it up to operating temperature. Operate the appliance until the water is heated to the upper operating control limit and has cycled at least two times. Then remove all unburned fuel, zero the scale and verify the scales accuracy using dead weights.

12.4.1 Start-up Procedure for Category III and IV test runs, “hot-to-hot”

12.4.1.1 Pre-Test Burn Cycle. Following appliance start-up (Section 12.4), reload appliance with oak cord wood and allow it to burn down to the specified coal bed weight. The pre-test burn cycle fuel charge weight shall be within $\pm 10\%$ of the test fuel charge weight. Piece size and length shall be selected such that charcoalization is achieved by the time the fuel charge has burned down to the required coal bed weight. Pieces with a maximum thickness of approximately 2 inches have been found to be suitable. Charcoalization is a general condition of the test fuel bed evidenced by an absence of large pieces of burning wood in the coal bed and the remaining fuel pieces being brittle enough to be broken into smaller charcoal pieces with a metal poker. Manipulations to the fuel bed prior to the start of the test run are to be done to achieve charcoalization while maintaining the desired heat output rate. During the pre-test burn cycle and at least one hour prior to starting the test run, adjust water flow to the heat exchanger to establish the target heat draw for the test. For the first test run the heat draw rate shall be equal to the manufacturer’s rated heat output capacity.

12.4.1.2 Allowable Adjustments. Fuel addition or subtractions, and coal bed raking shall be kept to a minimum but are allowed up to 15 minutes prior to the start of the test run. For the purposes of this method, coal bed raking is the use of a metal tool (poker) to stir coals, break burning fuel into smaller pieces, dislodge fuel pieces from positions of poor combustion, and check for the condition of charcoalization. Record all adjustments to and additions or subtractions of fuel, and any other changes to the appliance operations that occur during pretest ignition period. During the 15-minute period prior to the start of the test run, the wood heater loading door shall not be open more than a total of 1 minute. Coal bed raking is the only adjustment allowed during this period.

12.4.1.3 Coal Bed Weight. The appliance is to be loaded with the test fuel charge when the coal bed weight is between 10% and 20% of the test fuel charge weight. Coals may be raked as necessary to level the coal bed but may only be raked and stirred once between 15 to 20 minutes prior to the addition of the test fuel charge.

12.4.1.4 Storage. The Category III and IV test runs may be done either with or without the thermal storage. If thermal storage is used the initial temperature of the storage must be 125 °F or greater at the start of the test. The storage may be heated during the pre-test burn cycle or it may be heated by external means. If thermal storage is used, prior to the start of the test run, the storage tank destratification pump, shown in Figure 1, shall be operated until the total volume pumped exceeds 1.5 times the tank volume and the difference between the temperature at the top and bottom of the storage tank (TS_1 and TS_2) is less than 1°F. These two temperatures shall then be recorded to determine the starting average tank temperature. The total volume pumped may be based on the nominal flow rate of the destratification pump (see Section 9.6).

If the Category III and IV runs are done with storage, it is recognized that during the last hour of the pre-burn cycle the storage tank must be mixed to achieve a uniform starting temperature and cannot receive heat from the boiler during this

time. During this time period the boiler might cycle or go into a steady reduced output mode. (Note – this would happen, for example, in a Category IV run if the actual maximum output of the boiler exceed the manufacturer’s rated output.) A second storage tank may be used temporarily to enable the boiler to operate during this last hour of the pre-burn period as it will during the test period. The temperature of this second storage tank is not used in the calculations but the return water to the boiler (after mixing device if used) must be 125 °F or greater.

12.4.2 Start-Up Procedure for Category I and II test runs, “cold-to-cold”.

12.4.2.1 Initial Temperatures. This test shall be started with both the boiler and the storage at a minimum temperature of 125°F. The boiler maximum temperature at the start of this test shall be 135°F. The boiler and storage may be heated through a pre-burn or it may be heated by external means.

12.4.2.2 Firebox Condition at Test Start. Prior to the start of this test remove all ash and charcoal from the combustion chamber(s). The loading of the test fuel and kindling should follow the manufacturer’s recommendations, subject to the following constraints: Up to 10 % kindling and paper may be used which is in addition to the fuel load. Further, up to 10 % of the fuel load (i.e. included in the 10 lb/ft³) may be smaller than the main fuel. This startup fuel shall still be larger than 2”.

12.4.2.3 Storage. The Category I and II test runs shall be done with thermal storage. The initial temperature of the storage must be 125 °F or greater at the start of the test. The storage may be heated during the pre-test burn cycle or it may be heated by external means. Prior to the start of the test run, the storage tank destratification pump, shown in Figure 1, shall be operated until the total volume pumped exceeds 1.5 times the tank volume and the difference between the temperature at the top and bottom of the storage tank (TS_1 and TS_2) is less than 1°F. These two temperatures shall then be recorded to determine the starting average tank temperature. The total volume pumped may be based on the nominal flow rate of the destratification pump (see Section 9.6).

12.5 Test Runs. For all test runs, the return water temperature to the hydronic heater must be equal to or greater than 120°F (this is lower than the initial tank temperature to allow for any pipeline losses). Where the storage system is used, flow of water from the boiler shall be divided between the storage tank and the heat exchanger such that the temperature change of the circulating water across the heat exchanger shall be 30 ± 5 °F, averaged over the entire test run. This is typically adjusted using the system valves.

Complete a test run in each heat output rate category, as follows:

12.5.1 Test Run Start. For Category III and IV runs: once the appliance is operating normally and the pretest coal bed weight has reached the target value per 12.4.1, tare the scale and load the full test charge into the appliance. Time for loading shall not exceed 5 minutes. The actual weight of the test fuel charge shall be measured and recorded within 30 minutes prior to loading. Start all sampling systems.

For Category I and II runs: once the appliance has reached the starting temperature, tare the scale and load the full test charge, including kindling into the appliance. The actual weight of the test fuel charge shall be measured and recorded within 30 minutes prior to loading. Light the fire following the manufacturer's written normal startup procedure. Start all sampling systems.

12.5.1.1 Record all water temperatures, differential water temperatures and water flow rates at time intervals of one minute or less.

12.5.1.2 Record particulate emissions data per the requirements of EPA Method 28 WHH and the standards referenced therein.

12.5.1.3 Record data needed to determine Overall Efficiency (SLM) per the requirements of CSA B415.1-2010 Clauses 6.2.1, 6.2.2, 6.3, 8.5.7, 10.4.3 (a), 10.4.3(f), and 13.7.9.3

12.5.1.3.1 Measure and record the test room air temperature in accordance with the requirements of Clauses 6.2.1, 8.5.7 and 10.4.3 (g).

12.5.1.3.2 Measure and record the flue gas temperature in accordance with the requirements of Clauses 6.2.2, 8.5.7 and 10.4.3 (f).

12.5.1.3.3 Determine and record the Carbon Monoxide (CO) and Carbon Dioxide (CO₂) concentrations in the flue gas in accordance with Clauses 6.3, 8.5.7 and 10.4.3 (i) and (j).

12.5.1.3.4 Measure and record the test fuel weight per the requirements of Clauses 8.5.7 and 10.4.3 (h).

12.5.1.3.5 Record the test run time per the requirements of Clause 10.4.3 (a).

12.5.1.3.6 Record and document all settings and adjustments, if any, made to the boiler as recommended/required by manufacturer's instruction manual for different combustion conditions or heat loads. These may include temperature setpoints, under and over-fire air adjustment, or other adjustments that could be made by an operator to optimize or alter combustion. All such settings shall be included in the report for each test run.

12.5.1.4 Monitor the average heat output rate on the load side of the heat exchanger based on water temperatures and flow. If the heat output rate over a 10 minute averaging period gets close to the upper or lower limit of the target range ($\pm 5\%$), adjust the water flow through the heat exchanger to compensate. Make changes as infrequently as possible while maintaining the target heat output rate. The first test run shall be conducted at the category IV heat output rate to validate that the appliance is capable of producing the manufacturer's rated heat output capacity.

12.5.2 Test Fuel Charge Adjustment. It is acceptable to adjust the test fuel charge (i.e. reposition) once during a test run if more than 60 percent of the initial test

fuel charge weight has been consumed and more than 10 minutes have elapsed without a measurable (1 lb or 0.5 kg) weight change while the operating control is in the demand mode. The time used to make this adjustment shall be less than 60 seconds.

12.5.3 Test Run Completion. For the Category III and IV, “hot-to-hot” test runs, the test run is completed when the remaining weight of the test fuel charge is 0.0 lb (0.0 kg). ($W_{FuelBurned} = W_{fuel}$) End the test run when the scale has indicated a test fuel charge weight of 0.0 lb (0.0 kg) or less for 30 seconds.

For the Category I and II “cold-to-cold” test runs, the test run is completed when one of the following occurs:

1. The remaining weight of the test fuel charge is less than 1% of the total test fuel weight ($W_{FuelBurned} > 0.99 \bullet W_{fuel}$);
2. The automatic control system on the boiler switches to an off mode. In this case the boiler fan (if used) is typically stopped, and all air flow dampers are closed by the control system. Note that this off mode cannot be an “overheat” or emergency shutdown which typically requires a manual reset;
3. If the boiler does not have an automatic off mode: After 90% of the fuel load has been consumed and the scale has indicated a rate of change of the test fuel charge of less than 1.0 lb/hr for a period of 10 minutes or longer. Note- this is not considered “stopped fuel combustion”, see Section 12.5.6.1.

The end of a test is defined at the first occurrence of any one of these conditions.

12.5.3.1 At the end of the test run, stop the particulate sampling train and Overall Efficiency (SLM) measurements, and record the run time, and all final measurement values.

12.5.3.2 At the end of the test run, continue to operate the storage tank destratification pump until the total volume pumped exceeds 1.5 times the tank volume. The maximum average of the top and bottom temperatures measured after this time may be taken as the average tank temperature at the end of the tests (TFSavg, see Section 13.1). The total volume pumped may be based on the nominal flow rate of the destratification pump (see Section 9.6).

12.5.3.3 For the Category I and II test runs, there is a need to determine the energy content of the unburned fuel remaining in the chamber if the remaining mass in the chamber is greater than 1% of the test fuel weight. Following the completion of the test, as soon as safely practical, this remaining fuel is removed from the chamber, separated from the remaining ash and weighed. This separation could be implemented with a slotted “scoop” or similar tool. A ¼ inch opening size in the separation tool shall be used to separate the ash and charcoal. This separated char is assigned a heating value of 12,500 Btu/lb.

12.5.4 Heat Output Capacity Validation. The first test run must produce a heat output rate that is within 10% of the manufacturer’s rated heat output capacity

(Category IV) throughout the test run and an average heat output rate within 5% of the manufacturer's rated heat output capacity. If the appliance is not capable of producing a heat output within these limits, the manufacturer's rated heat output capacity is considered not validated and testing is to be terminated. In such cases, the tests may be restarted using a lower heat output capacity if requested by the manufacturer. Alternatively, during the Category IV run, if the rated output cannot be maintained for a 15 minute interval, the manufacturer may elect to reduce the rated output to match the test and complete the Category IV run on this basis. The target outputs for Cat I, II, and III shall then be recalculated based on this change in rated output capacity.

12.5.5 Additional Test Runs. Using the Manufacturer's Rated Heat Output Capacity as a basis, conduct a test for additional heat output categories as specified in 4.3. It is not required to run these tests in any particular order.

12.5.6 Alternative Heat Output Rate for Category I. If an appliance cannot be operated in the Category I heat output range due to stopped combustion, two test runs shall be conducted at heat output rates within Category II. When this is the case, the weightings for the weighted averages indicated in Section 15.1.14 shall be the average of the Category I and II weighting's and shall be applied to both Category II results. Appliances that are not capable of operation within Category II (<25% of maximum) cannot be evaluated by this test method.

12.5.6.1 Stopped Fuel Combustion. Evidence that an appliance cannot be operated at a Category I heat output rate due to stopped fuel combustion shall include documentation of two or more attempts to operate the appliance in heat output rate Category I and fuel combustion has stopped prior to complete consumption of the test fuel charge. Stopped fuel combustion is evidenced when an elapsed time of 60 minutes or more has occurred without a measurable (1 lb or 0.5 kg) weight change in the test fuel charge while the appliance operating control is in the demand mode. Report the evidence and the reasoning used to determine that a test in heat output rate Category I cannot be achieved. For example, two unsuccessful attempts to operate at an output rate of 10% of the rated output capacity are not sufficient evidence that heat output rate Category I cannot be achieved.

12.5.7 Appliance Overheating. Appliances with their associated thermal storage shall be capable of operating in all heat output categories without overheating to be rated by this test method. Appliance overheating occurs when the rate of heat withdrawal from the appliance is lower than the rate of heat production when the unit control is in the idle mode. This condition results in the water in the appliance continuing to increase in temperature well above the upper limit setting of the operating control. Evidence of overheating includes: 1 hour or more of appliance water temperature increase above the upper temperature set-point of the operating control, exceeding the temperature limit of a safety control device (independent from the operating control – typically requires manual reset), boiling water in a non-pressurized system or activation of a pressure or temperature relief valve in a pressurized system.

12.5.8 Option to Eliminate Tests in Category II and III. Following successful completion of a test run in Category I, the manufacturer may eliminate the Cat II and III tests. For the purpose of calculating the annual averages for particulates and efficiency, the values obtained in the Category I run shall be assumed to apply also to Category II and Category III. It is envisioned that this option would be applicable to systems which have sufficient thermal storage such that the fuel load in the Cat I test can be completely consumed without the system reaching its upper operating temperature limit. In this case the boiler would likely be operating at maximum thermal output during the entire test and this output rate may be higher than the Manufacturer's Rated Heat Output Capacity. The Category II and III runs would then be the same as the Category I run. It may be assumed that the particulate emission values and efficiency values determined in the start-up, steady-state, and end phases of Category I are applicable in Categories II and III, for the purpose of determining the annual averages in lb/MMBtu and g/MJ (see Section 13). For the annual average in g/hr, the length of time for stored heat to be drawn from thermal storage shall be determined for the test load requirements of the respective Category.

12.5.9 Modification to Measurement Procedure in EPA Method 28 WHH to Determine Emissions Separately During the Startup, Steady-State and End Phases. With one of the two particulate sampling trains used, filter changes shall be made at the end of the startup phase and the steady state phase (see Section 3.0). This shall be done to determine the particulate emission rate and particulate emission index for the startup, steady state, and end phases individually. For this one train, the particulates measured during each of these three phases shall be added together to also determine the particulate emissions for the whole run.

12.5.10 Modification to Measurement Procedure in EPA Method 28 WHH and the standards referenced therein on Averaging Period for Determination of Efficiency by the Stack Loss Method. The methods currently defined in Method 28 WHH allow averaging over 10 minute time periods for flue gas temperature, flue gas CO₂, and flue gas CO for the determination of the efficiency with the Stack Loss Method. However, under some cycling conditions the "on" period may be short relative to this 10 minute period. For this reason, during cycling operation the averaging period for these parameters may not be longer than the burner on period divided by 10. The averaging period need not be shorter than one minute. During the off period, under cycling operation, averaging periods as specified in EPA Method 28 WHH and the standards referenced therein may be used. Where short averaging times are used, however, the averaging period for fuel consumption may still be at 10 minutes. This average wood consumption rate shall be applied to all of the smaller time intervals included.

12.6 Additional Test Runs. The testing laboratory may conduct more than one test run in each of the heat output categories specified in Section 4.3. If more than one test run is conducted at a specified heat output rate, the results from at least two-thirds of the test runs in that heat output rate category shall be used in calculating the weighted average emission rate. The measurement data and results of all test runs shall be reported regardless of which values are used in calculating the weighted average emission rate.

13.0 Calculation of Results

13.1 Nomenclature.

CO_s – Carbon monoxide measured in the dilution tunnel at arbitrary time in ppm dry basis.

$CO_{g/min}$ – Carbon monoxide emission rate in g/min.

CO_T – Total carbon monoxide emission for the full test run in grams.

$CO_{_1}$ – Startup period carbon monoxide emissions in grams.

$CO_{_2}$ – Steady-state period carbon monoxide emission in grams.

$CO_{_3}$ – End period carbon monoxide emission in grams.

E_T – Total particulate emissions for the full test run as determined per EPA Method 28 WHH and the standards referenced therein in grams.

E_1 = Startup period particulate emissions in grams.

E_2 = Steady-state period particulate emissions in grams.

E_3 = End period particulate emissions in grams.

$E_{1_g/kg}$ = Startup period particulate emission index in grams per kg fuel.

$E_{2_g/kg}$ = Steady-state period particulate emission index in grams per kg fuel.

$E_{3_g/kg}$ = End period particulate emission index in grams per kg fuel.

$E_{1_g/hr}$ = Startup period particulate emission rate in grams per hour.

$E_{2_g/hr}$ = Steady-state period particulate emission rate in grams per hour.

$E_{3_g/hr}$ = End period particulate emission rate in grams per hour.

$E_{g/MJ}$ – Emission rate in grams per MJ of heat output.

$E_{lb/mmBtu\ output}$ – Emissions rate in pounds per million Btu's of heat output.

$E_{g/kg}$ – Emissions factor in grams per kilogram of dry fuel burned.

$E_{g/hr}$ – Emission factor in grams per hour.

HHV – Higher Heating Value of fuel = 8600 Btu/lb (19.990 MJ/kg).

LHV – Lower Heating Value of fuel = 7988 Btu/lb (18.567 MJ/kg).

ΔT – Temperature difference between cooling water entering and exiting the heat exchanger.

Q_{out} – Total heat output in Btu's (MJ).

Q_{in} – Total heat input available in test fuel charge in Btu's (MJ).

Q_{std} – Volumetric flow rate in dilution tunnel in dscfm.

M – Mass flow rate of water in lb/min (kg/min).

V_i – Volume of water indicated by a totalizing flow meter at the i^{th} reading in gallons (liters).

V_f – Volumetric flow rate of water in heat exchange system in gallons per minute (liters/min).

Θ – Total length of burn period in hours ($\Theta_1 + \Theta_2 + \Theta_3$).

Θ_1 – Length of time of the startup period in hours.

Θ_2 – Length of time of the steady state period in hours.

Θ_3 – Length of time of the end period in hours.

Θ_4 – Length of time for stored heat to be used following a burn period in hours.

t_i – Data sampling interval in minutes.

η_{del} – Delivered heating efficiency in percent.

F_i – Weighting factor for heat output category i . See Table 2.

$T1$ – Temperature of water at the inlet on the supply side of the heat exchanger, °F.

$T2$ – Temperature of the water at the outlet on the supply side of the heat exchanger, °F.

$T3$ – Temperature of cooling water at the inlet to the load side of the heat exchanger, °F.

$T4$ – Temperature of cooling water at the outlet of the load side of the heat exchanger, °F.

$T5$ – Temperature of the hot water supply as it leaves the boiler, °F.

$T6$ – Temperature of return water as it enters the boiler, °F.

$T7$ – Temperature in the boiler optional destratification loop at the top of the boiler, °F.

T_8 – Temperature in the boiler optional destratification loop at the bottom of the boiler, °F.

$T_{I_{avg}}$ – Average temperature of the appliance and water at start of the test.

$$T_{I_{avg}} = (T_5 + T_6)/2 \text{ at the start of the test, } ^\circ\text{F.} \quad \text{Eq. 1}$$

$T_{F_{avg}}$ – Average temperature of the appliance and water at the end of the test.

$$T_{F_{avg}} = (T_5 + T_6)/2 \text{ at the end of the test, } ^\circ\text{F.} \quad \text{Eq. 2}$$

TIS_1 – Temperature at the inlet to the storage system at the start of the test.

TIS_2 – Temperature at the outlet from the storage system at the start of the test.

TFS_1 – Temperature at the inlet to the storage system at the end of the test.

TFS_2 – Temperature at the outlet from the storage system at the end of the test.

TIS_{avg} – Average temperature of the storage system at the start of the test.

$$TIS_{avg} = (TIS_1 + TIS_2)/2 \text{ at the end of the test.} \quad \text{Eq. 3}$$

TFS_{avg} – Average temperature of the storage system at the end of the test.

$$TFS_{avg} = (TFS_1 + TFS_2) / 2. \quad \text{Eq. 4}$$

MC – Fuel moisture content in percent dry basis.

σ – Density of water in pounds per gallon.

$\sigma_{Initial}$ – Density of water in the boiler system at the start of the test in pounds per gallons.

σ_{boiler} – Density of water in the boiler system at arbitrary time during the test in pounds per gallon.

C_p – Specific heat of water in Btu /lb °-F.

C_{steel} – Specific heat of steel (0.1 Btu/ lb °-F).

V_{boiler} – total volume of water in the boiler system on the weight scale in gallons.

W_{fuel} – Fuel charge weight, as-fired or “wet”, in pounds (kg).

W_{fuel_1} – Fuel consumed during the startup period in pounds (kg).

W_{fuel_2} – Fuel consumed during the steady state period in pounds (kg).

W_{fuel_3} – Fuel consumed during the end period in pounds (kg).

$W_{\text{FuelBurned}}$ – Weight of fuel which has been burned from the start of the test to an arbitrary time, including the needed correction for the change in density and weight of the water in the boiler system on the scale in pounds (kg).

$W_{\text{RemainingFuel}}$ – weight of unburned fuel separated from the ash at the end of a test. Useful only for Cat I and Cat II tests.

W_{app} – Weight of empty appliance in pounds (kg).

W_{wat} – Weight of water in supply side of the system in pounds (kg).

$W_{\text{ScaleInitial}}$ – weight reading on the scale at the start of the test, just after the test load has been added in pounds (kg).

W_{Scale} – Reading of the weight scale at arbitrary time during the test run in pounds (kg).

$W_{\text{StorageTank}}$ – Weight of the storage tank empty in pounds (kg).

$W_{\text{WaterStorage}}$ – Weight of the water in the storage tank at TIS_{avg} in pounds (kg).

13.2 After the test is completed, determine the particulate emissions E_T in accordance with EPA Method 28 WHH and the standards referenced therein.

13.3 Determination of the weight of fuel which has been burned at arbitrary time
For the purpose of tracking the consumption of the test fuel load during a test run the following may be used to calculate the weight of fuel which burned since the start of the test:

$$W_{\text{FuelBurned}} = (W_{\text{ScaleInitial}} - W_{\text{Scale}}) + V_{\text{Boiler}} \cdot (\sigma_{\text{Initial}} - \sigma_{\text{boiler}}) \quad \text{Eq. 5}$$

Water density, σ , is calculated using Equation 12.

13.4 Determine Average Fuel Load Moisture Content.

$$MC = \frac{\sum W_{\text{SliceWet}_i} \cdot MC_{\text{Slice}_i}}{\sum W_{\text{SliceWet}_i}} \quad \text{Eq. 6}$$

13.5 Determine heat input.

$$Q_{\text{in}} = (W_{\text{fuel}} / (1 + (MC/100))) \times \text{HHV}, \text{ Btu (MJ)}. \quad \text{Eq. 7}$$

$$Q_{\text{in LHV}} = (W_{\text{fuel}} / (1 + (MC/100))) \times \text{LHV}, \text{ Btu (MJ)}. \quad \text{Eq. 8}$$

13.5.1 Correction to Q_{in} for the Category I and II tests, where there is greater than 1% of the test fuel charge in the chamber at the end of the test period.

$$Q_{InCorrected} = Q_{in} - W_{RemainingFuel} \cdot 12,500 \frac{Btu}{lb} \quad \text{Eq. 9}$$

13.6 Determine heat output, efficiency, and emissions

13.6.1 Determine heat output as:

$Q_{out} = \Sigma$ [Heat output determined for each sampling time interval]+ Change in heat stored in the appliance + Change in heat in storage tank.

$$Q_{out} = \sum_i [C_{pi} \cdot \Delta T_i \cdot M_i \cdot t_i] + (W_{app} \cdot C_{steel} + W_{water} \cdot C_{pa}) \cdot (TF_{avg} - TI_{avg}) + (W_{StorageTank} \cdot C_{steel} + W_{WaterStorage} \cdot C_{pa}) \cdot (TFS_{avg} - TIS_{avg}) \text{ Btu (MJ)}. \quad \text{Eq. 10}$$

Note: The subscript (i) indicates the parameter value for sampling time interval t_i .

$M_i = \text{Mass flow rate} = \text{gal/min} \times \text{Density of Water (lb/gal)} = \text{lb/min.}$

$$M_i = V_{fi} \cdot \sigma_i, \text{ lb/min.} \quad \text{Eq. 11}$$

$$\sigma_i = (62.56 + (-.0003413 \times T_{3i}) + (-.00006225 \times T_{3i}^2)) 0.1337, \text{ lbs/gal.} \quad \text{Eq. 12}$$

$$C_p = 1.0014 + (-.000003485 \times T_{3i}) \text{ Btu/lb-}^\circ\text{F.} \quad \text{Eq. 13}$$

$$C_{steel} = 0.1 \text{ Btu/lb-}^\circ\text{F.}$$

$$C_{pa} = 1.0014 + (-.000003485 \times (TI_{avg} + TF_{avg})/2), \text{ Btu/lb-}^\circ\text{F.} \quad \text{Eq. 14}$$

$$V_{fi} = (V_i - V_{i-1}) / (t_i - t_{i-1}), \text{ gal/min.} \quad \text{Eq. 15}$$

Note: V_i is the total water volume at the end of interval i and V_{i-1} is the total water volume at the beginning of the time interval. This calculation is necessary when a totalizing type water meter is used.

13.6.2 Determine Heat Output Rate Over Burn Period ($\Theta_1 + \Theta_2 + \Theta_3$) as:

$$\text{Heat Output Rate} = Q_{out} / \Theta, \text{ Btu/hr (MJ/hr)}. \quad \text{Eq. 16}$$

13.6.3 Determine Emission Rates and Emission Factors as:

$$E_{g/MJ} = E_T / (Q_{out} \times 0.001055), \text{ g/MJ.} \quad \text{Eq. 17}$$

$$E_{lb/MM \text{ Btu output}} = (E_T / 453.59) / (Q_{out} \times 10^{-6}), \text{ lb/MMBtu Out.} \quad \text{Eq. 18}$$

$$E_{g/kg} = E_T / (W_{fuel} / (1 + MC/100)), \text{ g/dry kg.} \quad \text{Eq. 19}$$

$$E_{g/hr} = E_T / (\Theta_1 + \Theta_2 + \Theta_3 + \Theta_4), \text{ g/hr.} \quad \text{Eq. 20}$$

$$\Theta_4 = (W_{StorageTank} \cdot C_{steel} + W_{WaterStorage} \cdot C_{pa}) \cdot (TFS_{avg} - TIS_{avg}) / (Q_{out} / \Theta) \quad \text{Eq. 21}$$

If thermal storage is not used in a Category III or IV run, then $\Theta_4 = 0$

$$E_{1_g/kg} = E_1 / (W_{fuel_1} / (1 + MC/100)), \text{ g/dry kg}$$

$$E_{2_g/kg} = E_2 / (W_{fuel_2} / (1 + MC/100)), \text{ g/dry kg}$$

$$E_{3_g/kg} = E_3 / (W_{fuel_3} / (1 + MC/100)), \text{ g/dry kg}$$

$$E_{1_g/hr} = E_1 / \Theta_1, \text{ g/hr}$$

$$E_{2_g/hr} = E_2 / \Theta_2, \text{ g/hr}$$

$$E_{3_g/hr} = E_3 / \Theta_3, \text{ g/hr}$$

13.6.4 Determine delivered efficiency as:

$$\eta_{del} = (Q_{out} / Q_{inCorrected}) \times 100, \% \quad \text{Eq. 22}$$

Eq. 17

$$\eta_{del\ LHV} = (Q_{out} / Q_{in\ LHV}) \times 100, \% \quad \text{Eq. 23}$$

13.6.5 Determine η_{SLM} - Overall Efficiency, also known as Stack Loss Efficiency, using Stack Loss Method (SLM).

For determination of the average overall thermal efficiency (η_{SLM}) for the test run, use the data collected over the full test run and the calculations in accordance with CSA B415.1-2010, Clause 13.7 except for 13.7.2 (e), (f), (g), and (h), use the following average fuel properties for oak: %C = 50.0, %H = 6.6, %O = 43.2, %Ash = 0.2.

13.6.5.1 Whenever the CSA B415.1-2010 overall efficiency is found to be lower than the overall efficiency based on load side measurements, as determined by Eq. 22 of this method, Section 14.1.7 of the test report must include a discussion of the reasons for this result. For a test where the CSA B415.1-2010 overall efficiency SLM is less than 2 percentage points lower than the overall efficiency based on load side measurements, the efficiency based on load side measurements shall be considered invalid. *[Note on the rationale for the 2 percentage points limit. The SLM method does not include boiler jacket losses and, for this reason, should provide an efficiency which is actually higher than the efficiency based on the energy input and output measurements or “delivered efficiency”. A delivered efficiency that is higher than the efficiency based on the SLM could be considered suspect. A delivered efficiency greater than 2 percentage points higher than the efficiency based on the SLM, then, clearly indicates a measurement error.]*

13.6.6 Carbon Monoxide Emissions

For each minute of the test period, the carbon monoxide emission rate shall be calculated as:

$$CO_{g/min} = Q_{std} \cdot CO_S \cdot 3.298 \times 10^{-5} \quad \text{Eq.24}$$

Total CO emissions for each of the three test periods (CO₋₁, CO₋₂, CO₋₃) shall be calculated as the sum of the emission rates for each of the 1 minute intervals.

Total CO emission for the test run, CO_T, shall be calculated as the sum of CO₋₁, CO₋₂, and CO₋₃.

13.7 Weighted Average Emissions and Efficiency.

13.7.1 Determine the weighted average emission rate and delivered efficiency from the individual tests in the specified heat output categories. The weighting factors (F_i) are derived from an analysis of ASHRAE Bin Data which provides details of normal building heating requirements in terms of percent of design capacity and time in a particular capacity range – or “bin” - over the course of a heating season. The values used in this method represent an average of data from several cities located in the northern United States.

$$\text{Weighted average delivered efficiency: } \eta_{avg} = \sum \eta_i \times F_i, \% \quad \text{Eq. 25}$$

$$\text{Weighted average emissions: } E_{avg} = \sum E_i \times F_i, \% \quad \text{Eq. 26}$$

If, as discussed in Section 12.5.8, the option to eliminate tests in Category II and III is elected, the values of efficiency and particulate emission rate as measured in Category I, shall be assigned also to Category II and III for the purpose of determining the annual averages.

14.0 Report

14.1.1 The report shall include the following:

14.1.2 Name and location of the laboratory conducting the test.

14.1.3 A description of the appliance tested and its condition, date of receipt and dates of tests.

14.1.4 A description of the minimum amount of external thermal storage that is required for use with this system. This shall be specified both in terms of volume in gallons and stored energy content in Btu with a storage temperature ranging from 125 °F to the manufacturer’s specified setpoint temperature.

14.1.5. A statement that the test results apply only to the specific appliance tested.

14.1.6 A statement that the test report shall not be reproduced except in full, without the written approval of the laboratory.

14.1.7 A description of the test procedures and test equipment including a schematic or other drawing showing the location of all required test equipment. Also, a description of test fuel sourcing, handling and storage practices shall be included.

14.1.8 Details of deviations from, additions to or exclusions from the test method, and their data quality implications on the test results (if any), as well as information on specific test conditions, such as environmental conditions.

14.1.9 A list of participants and their roles and observers present for the tests.

14.1.10 Data and drawings indicating the fire box size and location of the fuel charge.

14.1.11 Drawings and calculations used to determine firebox volume.

14.1.12 Information for each test run fuel charge including piece size, moisture content and weight.

14.1.13 All required data and applicable blanks for each test run shall be provided in spreadsheet format both in the printed report and in a computer file such that the data can be easily analyzed and calculations easily verified. Formulas used for all calculations shall be accessible for review.

14.1.14 For each test run, $\Theta_1, \Theta_2, \Theta_3$, the total CO and particulate emission for each of these three periods, and Θ_4 .

14.1.15 Calculated results for delivered efficiency at each heat output rate and the weighted average emissions reported as total emissions in grams, pounds per million Btu of delivered heat, grams per MJ of delivered heat, grams per kilogram of dry fuel and grams per hour. Results shall be reported for each heat output category and the weighted average.

14.1.16 Tables 1A, 1B, 1C, 1D, 1E and 2 must be used for presentation of results in test reports.

14.1.17 A statement of the estimated uncertainty of measurement of the emissions and efficiency test results.

14.1.18 A plot of CO emission rate in grams/minute vs. time, based on 1 minute averages, for the entire test period, for each run.

14.1.19 A plot of estimated boiler energy release rate in Btu/hr based on 10 minute averages, for the entire test period, for each run. This will be calculated from the fuel used, the wood heating value and moisture content, and the SLM efficiency during each 10 minute period.

14.1.20 Raw data, calibration records, and other relevant documentation shall be retained by the laboratory for a minimum of 7 years.

15.0 Precision and Bias

15.1 Precision – It is not possible to specify the precision of the procedure in this test method because the appliance operation and fueling protocols and the appliances themselves produce variable amounts of emissions and cannot be used to determine reproducibility or repeatability of this test method.

15.2 Bias – No definitive information can be presented on the bias of the procedure in this test method for measuring solid fuel burning hydronic heater emissions because no material having an accepted reference value is available.

16.0 Keywords

16.1 Solid fuel, hydronic heating appliances, wood-burning hydronic heaters, partial thermal storage.

Table 1C. Data Summary Part C

			Θ_1	Θ_2	Θ_3	CO ₁	CO ₂	CO ₃	CO _T
Category	Run No	Load % Capacity	Startup Time.	Steady State Time	End Time	Startup CO emission	Steady State CO emission	End CO emission	Total CO emission
			min	min	min	g	g	g	g
I		< 15% of max							
II		16-24% of max							
III		25-50% of max							
IV		Max capacity							

Table 1D. Data Summary Part D

			E ₁	E ₂	E ₃	E _{1_g/kg}	E _{2_g/kg}	E _{3_g/kg}
Category	Run No	Load % Capacity	Startup PM	Steady State PM	End PM	Startup PM emission index	Steady State PM emission index	End PM emission index
			g	g	g	g/kg fuel	g/kg fuel	g/kg fuel
I		< 15% of max						
II		16-24% of max						
III		25-50% of max						
IV		Max capacity						

Table 1E: Hang Tag Information

MANUFACTURER:			
MODEL NUMBER:			
ANNUAL EFFICIENCY RATING:	η_{avg}		(Using higher heating value)
			(Using lower heating value)
PARTICLE EMISSIONS:	E_{avg}		GRAMS/HR (average)
			LBS/MILLION Btu/hr OUTPUT

Table 2. Annual Weighting

Category	Weighting Factor (F_i)	$\eta_{del,i} \times F_i$	$E_{g/MJ,i} \times F_i$	$E_{g/kg,i} \times F_i$	$E_{lb/MMBtu Out,i} \times F_i$	$E_{g/hr,i} \times F_i$
I	0.437					
II	0.238					
III	0.275					
IV	0.050					
Totals	1.000					

